

*Pertti Ala-aho*

# GROUNDWATER-SURFACE WATER INTERACTIONS IN ESKER AQUIFERS

*FROM FIELD MEASUREMENTS TO FULLY  
INTEGRATED NUMERICAL MODELLING*

UNIVERSITY OF OULU GRADUATE SCHOOL;  
UNIVERSITY OF OULU,  
FACULTY OF TECHNOLOGY





ACTA UNIVERSITATIS OULUENSIS  
C Technica 510

*PERTTI ALA-AHO*

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INTERACTIONS IN ESKER AQUIFERS**

From field measurements to fully integrated numerical  
modelling

Academic dissertation to be presented with the assent of  
the Doctoral Training Committee of Technology and  
Natural Sciences of the University of Oulu for public  
defence in Auditorium GO101, Linnanmaa, on 9  
December 2014, at 12 noon

UNIVERSITY OF OULU, OULU 2014

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Acta Univ. Oul. C 510, 2014

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ISBN 978-952-62-0657-8 (Paperback)  
ISBN 978-952-62-0658-5 (PDF)

ISSN 0355-3213 (Printed)  
ISSN 1796-2226 (Online)

Cover Design  
Raimo Ahonen

JUVENES PRINT  
TAMPERE 2014

# **Ala-aho, Pertti, Groundwater-surface water interactions in esker aquifers. From field measurements to fully integrated numerical modelling**

University of Oulu Graduate School; University of Oulu, Faculty of Technology

*Acta Univ. Oul. C 510, 2014*

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## ***Abstract***

Water resources management calls for methods to simultaneously manage groundwater (GW) and surface water (SW) systems. These have traditionally been considered separate units of the hydrological cycle, which has led to oversimplification of exchange processes at the GW-SW interface. This thesis studied GW hydrology and the previously unrecognised connection of the Rokua esker aquifer with lakes and streams in the area, with the aim of identifying reasons for lake water level variability and eutrophication in the Rokua esker.

GW-SW interactions in the aquifer were first studied with field methods. Seepage meter measurements showed substantial spatial variability in GW-lake interaction, whereas transient variability was more modest, although present and related to the surrounding aquifer. Environmental tracers suggested that water exchange occurs in all lakes in the area, but is of varying magnitude in different lakes. Finally, GW-SW interaction was studied in peatland catchments, where drainage channels in the peat soil presumably increased groundwater outflow from the aquifer.

Amount and rate of GW recharge were then estimated with a simulation approach developed explicitly to account for the physical characteristics of the Rokua esker aquifer. This produced a spatially and temporally distributed recharge estimate, which was validated by independent field techniques. The results highlighted the impact of canopy characteristics, and thereby forestry management, on GW recharge.

The data collected and the new understanding of site hydrology obtained were refined into a fully integrated surface-subsurface flow model of the Rokua aquifer. Simulation results compared favourably to field observations of GW, lake levels and stream discharge. A major finding was of good agreement between simulated and observed GW inflow to lakes in terms of discharge locations and total influx.

This thesis demonstrates the importance of using multiple methods to gain a comprehensive understanding of esker aquifer hydrology with interconnected lakes and streams. Importantly, site-specific information on the reasons for water table variability and the trophic status of Rokua lakes, which is causing local concern, is provided. As the main outcome, various field and modelling methods were tested, refined and shown to be suitable for integrated GW and SW resource management in esker aquifers.

*Keywords:* environmental tracers, esker aquifers, groundwater, groundwater-surface water interaction, hydrological modelling



## **Ala-aho, Pertti, Pinta- ja pohjaveden vuorovaikutus harjuakvifereissa. Kenttämitauksista integroituun numeeriseen mallinnukseen**

Oulun yliopiston tutkijakoulu; Oulun yliopisto, Teknillinen tiedekunta

*Acta Univ. Oul. C 510, 2014*

Oulun yliopisto, PL 8000, 90014 Oulun yliopisto

### ***Tiivistelmä***

Vesivarojen hallinnassa tarvitaan menetelmiä pohja- ja pintaveden kokonaisvaltaiseen huomioimiseen. Pohja- ja pintavesiä tarkastellaan usein erillisinä osina hydrologista kiertoa, mikä on johtanut niiden välisten virtausprosessien yksinkertaistamiseen. Tässä työssä selvitettiin Rokuan pohjavesiesiintymän hydrologiaa ja hydraulista yhteyttä alueella oleviin järviin ja puroihin. Tutkimuksessa pyrittiin osaltaan selvittämään syitä harjualueen järvien pinnanvaihteluun ja veden laatuongelmiin.

Kenttätutkimuksissa todettiin voimakasta alueellista vaihtelua järven ja pohjaveden vuorovaikutuksessa. Pohjaveden suotautumisen ajallinen vaihtelu puolestaan oli vähäisempää, mutta havaittavissa, ja kytköksissä järveä ympäröivän pohjavesipinnan vaihteluihin. Merkkiaineet vesinäytteistä viittasivat vastaavan vuorovaikutuksen olevan läsnä myös muissa alueen järvissä, mutta suotautuvan pohjaveden määrän vaihtelevan järvirtäin. Turvemaiilla tehdyt mittaukset osoittivat pohjaveden purkautuvan ojaverkostoon ja ojituksen mahdollisesti lisäävän ulosvirtaamaa pohjavesiesiintymästä.

Pohjaveden muodostumismäärää ja -nopeutta tutkittiin numeerisella mallinnuksella, joka kehitettiin huomioimaan harjualueelle ominaiset fysikaaliset tekijät. Mallinnus tuotti arvion ajallisesti ja alueellisesti vaihtelevasta pohjaveden muodostumisesta, joka varmennettiin kenttämitauksilla. Tuloksissa korostui kasvillisuuden, ja sitä kautta metsähakkuiden, vaikutus pohjaveden muodostumismääriin.

Hydrologiasta kerätyn aineiston ja kehittyneen prosessiymmärryksen avulla Rokuan harjualueesta muodostettiin täysin integroitu numeerinen pohjavesi-pintavesi virtausmalli. Mallinnustulokset vastasivat mittauksia pohjaveden ja järvien pinnantasosta sekä purovirtaamista. Työn merkittävin tulos oli, että mallinnetut pohjaveden purkautumiskohdat ja purkautumismäärät alueen järviin vastasivat kenttähavaintoja.

Tämä työ havainnollisti, että ymmärtääkseen pohjaveden ja siitä riippuvaisten järvien ja purojen vuorovaikutusta harjualueella on käytettävä monipuolisia tutkimusmenetelmiä. Työ toi lisätietoa Rokuan harjualueen vesiongelmiin syihin selittäen järvien vedenpinnan vaihtelua ja vedenlaatua pohjavesihydrologialla. Väitöstyön tärkein anti oli erilaisten kenttä- ja mallinnusmenetelmien soveltaminen, kehittäminen ja hyödylliseksi havaitseminen harjualueiden kokonaisvaltaisessa pinta- ja pohjavesien hallinnassa.

*Asiasanat:* harjut, hydrologinen mallinnus, pinta- ja pohjaveden vuorovaikutus, pohjavesi, ympäristömerkkiaineet





*To my Mother*



## Acknowledgements

This thesis was made possible by funding from the EU Seventh Framework Programme GENESIS (no. 226536) and the Academy of Finland project AQVI (no. 128377). In addition, VALUE doctoral programme, Thule doctoral programme and University of Oulu Graduate School offered high level education, scientific workshops and travel grants, which gave me the knowhow required for the thesis. In addition, travel and personal grants from Maa- ja Vesitekniikan Tuki r.y., Renlund Foundation, Tauno Tönning Foundation and Sven Hallin Foundation were vital in completing the thesis and giving me the opportunity to attend several international scientific courses, conferences and an exchange visit.

My supervisor, Prof. Bjørn Kløve, gets my sincerest gratitude for guiding me through the PhD process and creating unique opportunities during that time. I especially appreciate the open-mindedness and encouraging attitude of Prof. Kløve, which gave me great support in becoming a scientist. Another person who single-handedly made a tremendous contribution to this thesis was my dear friend and colleague Pekka Rossi. Innumerable shared moments and experiences made these years what they were, cheers mate! I thank pre-examiners Dr. John Paul Jones and Prof. Peter Engesgaard for their valuable contribution in completing the thesis and Dr. Mary McAfee for her expertise and helpfulness in language revision of all the manuscripts.

My day-to-day work at the university was always coloured by the Water Resources and Environmental Engineering Research Group - thank you all for the shared laughs and help I could always rely on. I want to thank Anna-Kaisa, Elina, Hannu, Riku, Virve K., Tuomo R., and Tuomo P. for their important contributions to the thesis, and (going from south to north along our corridor) Virve M, Ali, Pirkko, Katharina, Jarmo, Anne, Kauko, Simo, Paavo, Shähram, Tuomas, Masoud, Tapio, Ehsan, Meseret, Justice, Elisangela, Heini, and all the trainees and students over the years for their smiles and kind words.

I had the privilege to spend fall semester 2012 at the University of Waterloo, Canada, which was crucial for the final outcome of this thesis. I sincerely thank all the inspiring professors, students and people at UW and Aquanty Inc. Special thanks to Prof. Ed Sudicky and his team at the time, Rob, Young-Jin, Hyuon-Tae and Jason, for their help with the HGS and hospitality in general. Several other institutions and collaborators have provided irreplaceable input to this thesis and sincere thanks go to all those individuals and institutions who took part in investigations at the Rokua site. In particular would like to thank Jarkko Okkonen for his advice and discussions along

the way, which gave me lots of perspective and new ideas. I want to acknowledge all the people in the GENESIS project for their great scientific advice and fun company in the memorable meetings around Europe. You are too many to list, sorry! As seen from the above, this four-year period acquainted me with numerous people around the world, for which I'm extremely grateful. Special thanks to Dmytro, Marc-André and Peter, my international friends, it has been a pleasure getting to know you guys.

An unconditional thank you goes to my family Tuija, Olavi, Irma, Laura, Saara, Vilma and extended family and friends, who have been my bedrock throughout my studies. Dear sisters, read the next hundred or so pages and you might finally figure out what it is I do at the University. Sweet thank you Essi-Maaria for your loving encouragement and support.

Even though my name appears on the book cover, it is just as much authored by all the people acknowledged above and the science preceding my studies. You gave small ideas like springs, which eventually combined into the stream flowing in the text. My humble thanks to you all.

Oulu, October 2014

Pertti Ala-aho

## List of symbols and abbreviations

GW-SW	Groundwater – surface water
SWE	Snow water equivalent
asl	Above sea level
K	Hydraulic conductivity of porous medium
MH	Finnish Forest Administration (Metsähallitus)
MK	Finnish Forest Centre (Metsäkeskus)
EC	Electrical conductivity, a water quality parameter
LAI	Leaf area index
UZD	Unsaturated zone depth
1-D	One-dimensional
DEM	Digital elevation model
TIR	Thermal infrared imaging
B&C	Brooks and Corey water retention function
WTF	Water table fluctuation method to estimate groundwater recharge
ELY Centre	Centre for Economic Development, Transport and the Environment
FMI	Finnish Meteorological Institute



## List of original publications

This thesis is based on the following publications, which are referred to throughout the text by their Roman numerals:

- I Ala-aho P, Rossi, PM & Kløve, B (2013) Interaction of esker groundwater with headwater lakes and streams. *Journal of Hydrology* 500(2013): 144-156.
- II Rossi PM, Ala-aho P, Ronkanen A-K & Kløve B (2012) Groundwater-surface water interaction between an esker aquifer and a drained fen. *Journal of Hydrology* 432-433 (2012): 52-60.
- III Ala-aho P, Rossi, PM & Kløve, B (2014) Estimation of temporal and spatial variations in groundwater recharge in unconfined sand aquifers using Scots pine inventories. *Hydrology and Earth System Sciences Discussions* 11: 7773-7826. (*Manuscript*)
- IV Ala-aho P, Rossi, PM, Isokangas E & Kløve, B (2014) Fully integrated surface-subsurface flow modelling of groundwater-lake interaction in an esker aquifer: Model verification with stable isotopes and airborne thermal imaging. (*Manuscript*)

The author's contribution to publications I-IV:

- I Designed the study with co-authors. Performed the field work and analysed the results with Pekka Rossi. Wrote the paper with the co-authors.
- II Designed the study with Pekka Rossi and Bjørn Kløve, conducted the field work with Pekka Rossi. Analysed the results and wrote the paper with the co-authors.
- III Designed the study with the co-authors. Conducted the field work with Pekka Rossi. Was responsible for the modelling work, data analysis and writing the paper. Received critical comments on model analysis and on the manuscript from the co-authors.
- IV Designed the study with Pekka Rossi and Bjørn Kløve. Conducted the field work with Pekka Rossi and Elina Isokangas. Took responsibility for the modelling work. Received critical comments on model analysis and wrote the manuscript with the co-authors.





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# 1 Introduction

## 1.1 Future trends in Finnish groundwater management

Groundwater resources are vital for the well-being of society by providing a clean and reliable freshwater source for human consumption and agriculture, while supporting ecosystem services. However, these resources are facing multiple stresses at present, which are likely to increase in the future. The main threats come from over-abstraction (Konikow & Kendy 2005, Wada *et al.* 2010), pollution (Gleick 1993, Spalding & Exner 1993) and climate change (Green *et al.* 2011, Holman 2006, Treidel *et al.* 2011), all acting together to make the use of global groundwater resources less reliable in a world with a growing population and increasing need for water. As a consequence, groundwater management agencies and legislation have to respond to these challenges worldwide. Even though global trends in stressors are evident, local water resource management has to address aquifer-specific problems. In Finland, water resources management is guided by the National Water Act (Ministry of the Environment 2004) and European Union Groundwater Directive (EC 2006), both aiming to ensure the qualitative and quantitative integrity of groundwater bodies and related ecosystems.

To date, the Finnish policy for providing water supply has preferred the use of groundwater over surface water as a more clean and reliable water source (Katko *et al.* 2006). Unconfined esker aquifers make up the majority of exploitable groundwater resources for large-scale water supply in Finland (Britschgi *et al.* 2009). The total volume of renewable groundwater in esker aquifers greatly exceeds Finnish requirements, but the resources are small in size and unevenly distributed (Isomäki *et al.* 2007). The small and unconfined aquifers are susceptible to contamination, and the number of aquifers at risk of contamination has markedly increased within recent years (Ministry of the Environment 2013). Eskers are commonly covered by peatlands in their groundwater discharge area. These peatlands are often drained for forestry, but groundwater exfiltration to peatlands is not well understood (Langhoff *et al.* 2006, Lowry *et al.* 2009), which brings about uncertainty in land use management around esker aquifers.

Management of conflicting interests around these complex aquifers has gained recent research attention (Bolduc *et al.* 2005, Karjalainen *et al.* 2013, Koundouri *et al.* 2012, Kurki *et al.* 2013). As growing communities in Finland demand more potable groundwater, increasing abstraction pressures along with threats from contamination

have generated plans to exploit aquifers in Natura 2000 natural conservation areas (Isomäki *et al.* 2007). In addition to water supply, esker aquifers support groundwater-dependent ecosystems and provide recreational services for local inhabitants (Kløve *et al.* 2011). Finnish water abstraction plans have brought about vibrant discussion and, in some cases, strong local opposition to abstraction that might endanger protected natural habitats dependent on groundwater. A major reason igniting the conflicts has been uncertainty about the impacts of water abstraction on surface water bodies and on ecological systems dependent on the groundwater outflow.

At the same time, there has been a clear shift in management focus: well-being of aquatic ecosystems is now at the centre of European Union (EU) water management (EC 2000). One particularly important and endangered ecosystem type is groundwater-dependent ecosystems (GDEs), and the EU Groundwater Directive requires such systems to be characterised in order to determine their quality status (EC 2006). GDEs can be found in water bodies such as springs, wetlands, rivers and lakes, where groundwater directly or indirectly sustains ecosystems by providing them with a favourable water flow, temperature or chemical environment (Kløve *et al.* 2011). However, in most cases there is very little information on the status or even existence of GDEs or the environmental conditions they require (Brown *et al.* 2010, Hinsby *et al.* 2008).

Knowledge about GDEs is particularly important in Finland due to plans to include GDEs as a part of the national classification of exploitable aquifers (Government of Finland 2014). This would mean that the protected status of aquifers would partly depend on the ecosystems they support, and thereby influence land use planning and abstraction regulation. Such proposed legislation generates an urgent need to develop new tools and to raise awareness about existing practical methods for distinguishing, monitoring and protecting GDEs (Bertrand *et al.* 2013, Kløve *et al.* 2011). A key factor here is groundwater input to surface water bodies, which needs to be better understood and quantified. Groundwater and surface water should be considered as one management unit, because they are both highly relevant and interlinked in creating environmental conditions for biological communities (Hayashi & Rosenberry 2002, Katko *et al.* 2006, Sophocleous 2002, Winter *et al.* 1998).

## **1.2 Towards integrated management of GW and SW**

Groundwater (GW) and surface water (SW) are interlinked parts of the hydrological cycle, but are often erroneously treated as individual components. In reality, they

interact in most landscapes and climates. The main reason for ignoring the interaction between these to date has been lack of a conceptual process understanding and technical shortcomings. As Winter *et al.* (1998) put it: “*Surface water is commonly hydraulically connected to groundwater, but the interactions are difficult to observe and measure*”.

Winter (1995) summarises GW-SW interaction studies over their 100-year history, from aquifer contribution to streamflow in early studies, moving in the 1960s to groundwater and lake environments due to acid rain and eutrophication, and expanding to wetlands and estuaries because of loss of ecosystems in the 1980s. A final spurt in the number of GW-SW studies appeared in the 1990s, when the work focused on physical and biochemical process understanding (Sophocleous 2002).

Increased process understanding and technological advances during recent decades have generated numerous GW-SW interaction measurement techniques covering a wide array of temporal and spatial scales (Kalbus *et al.* 2006, Rosenberry & LaBaugh 2008). The underlying message from these studies is that water exchange between groundwater and surface water is highly transient in time and variable in space and is controlled by numerous interconnected features and processes, such as subsurface heterogeneities, groundwater flow systems, microtopography of the surface water bed, climate conditions and near-shore vegetation. In this regard, even though process understanding has markedly increased and novel technologies have offered a variety of tools to measure the interaction, the message in Winter *et al.* (1998) still holds; because of process complexity, measuring GW-SW interactions is difficult.

The research question as regards GW-SW interactions is moving from how to *measure* towards how to *manage*. Water resources management commonly operates on large (watershed or aquifer) scale, but processes at the GW-SW interface can be found on metre scale and revealed only with laborious measurements. In addition, several techniques are commonly needed to obtain an adequate process understanding of GW-SW interactions at a given study site (Bertrand *et al.* 2013). Even with various methods, it can be difficult to transform and extrapolate information across scales (Krause *et al.* 2014, Smith *et al.* 2008, Sophocleous 2002). A major research question is thus how to produce information of relevant spatial and temporal resolution in order to facilitate integrated management of water resources and ecosystems.

### 1.3 Research questions and objectives

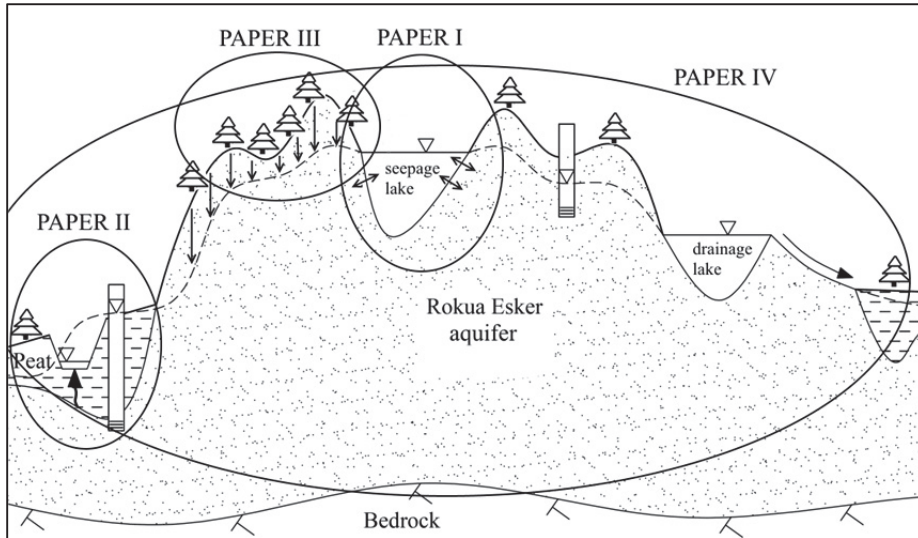
The work presented in this thesis was conducted to gain a comprehensive understanding of hydrological processes in the Rokua esker aquifer in Finland and to provide tools for integrated water resources management for Rokua and esker aquifers in general. The primary focus was to reveal the anticipated, but yet unknown, connections between groundwater and surface water in the aquifer and to study the relevance of GW-SW connectivity for water resources management. The work began by identifying the GW-SW exchange processes between the aquifer and small headwater lakes and streams by using various field techniques. After developing a conceptual model for the aquifer hydrology with field methods, the work proceeded to apply advanced numerical modelling methods for studying aquifer hydrological processes, in particular GW-SW interaction (Fig. 1).

In Papers I and II, the focus was on validating the assumption that the GW-SW exchange processes are present with meaningful intensity in the study site hydrology. The work in Paper I examined the groundwater-lake interactions in the groundwater *recharge area* using seepage meters and environmental tracers. The main objective was to determine the spatial and temporal variability in lake seepage for a pilot lake and apply environmental tracers to study whether GW-SW interactions can be found in other lakes in the area. Paper II focused on interaction between the aquifer and headwater streams located in the groundwater *discharge area*. The study used various field methods to study groundwater exfiltration to peatland drainage channels with the aim of verifying the existence and studying the magnitude of GW-SW connections.

To rigorously study the esker aquifer hydrology, detailed information on the water input to the system was needed. However, little research has been performed to date on the spatial and temporal variations in groundwater recharge amount and residence time in esker aquifers. Paper III studied how groundwater recharge is affected by the site-specific characteristics of esker aquifers, variable tree canopy due to forestry, aquifer geometry and hydrological parameterisation. The work utilised numerical modelling of the unsaturated zone and developed methodology to estimate groundwater recharge in esker aquifer systems using forest inventory data.

The understanding of the interactions present and the functioning of the esker hydrological processes gained from Papers I, II and III was compiled into a fully integrated surface-subsurface modelling study in Paper IV. The paper examined whether the previously found GW-SW interactions and land use impacts could be captured by state-of-the-art numerical modelling at the aquifer scale. In addition, model performance in reproducing fluxes at the GW-SW interface was compared

against field observations of groundwater influx magnitude and spatial distribution in a novel way using airborne infrared imaging.



**Fig. 1. Conceptual cross-section of the Rokua esker aquifer and the main focus of different studies. Paper I: Groundwater (GW)-lake interaction, Paper II: GW-peatland interaction, Paper III: GW recharge, and Paper IV: fully integrated surface-subsurface simulation of the aquifer system.**

The usual practice in managing groundwater and surface water bodies is to treat them as separate entities. This thesis addresses the validity of this approach by studying how the omnipresent contact between subsurface and surface water bodies can be better acknowledged in water investigations. In what way is the groundwater influence manifested in surface water bodies connected to esker aquifers? Furthermore, what methods can or should be applied to study GW-SW interactions, in order to gain an adequate understanding of the esker aquifer hydrology?





## 2 Interactions between groundwater and surface water

### *Darcy's Law as the fundamental concept*

The driving force in the water exchange between groundwater and surface water is the never-ending attempt of water molecules to move to a lower energy state. In the terminology of hydrogeology, energy is commonly stated as hydraulic potential or *hydraulic head*, combining concepts of energy in the form of pressure and elevation (Freeze & Cherry 1979). Differences in hydraulic head, i.e. the difference in fluid potential to flow through porous media, is then referred to as the *hydraulic gradient*. A relationship to calculate water flow in porous media using the hydraulic gradient was formulated experimentally by Darcy (1856) and is known as Darcy's Law:

$$v = -K \frac{dh}{dl} \quad (1)$$

where  $v$  is specific discharge ( $\text{m s}^{-1}$ ),  $dh/dl$  is hydraulic gradient ( $dh$  is the change in hydraulic head and  $dl$  the change in distance) and  $K$  is hydraulic conductivity ( $\text{m s}^{-1}$ ).

The negative sign in equation (1) indicates that water flows towards lower hydraulic head. In a simplified example of a GW-SW interaction process, if the water level in the surface water body is lower than that in the adjacent groundwater, water flows towards the lower head, i.e. surface water, or *vice versa*.

In practice, if the surface water body is in contact with a saturated porous medium in natural environments, where long-term zero gradients are unusual, there is always some exchange taking place between groundwater and surface water. Whether the exchange rates are meaningful in a hydrological perspective depends on the magnitude of the hydraulic gradient and the value of hydraulic conductivity, a proportionality based on the properties of the porous material and the characteristics of the fluid.

The literature provides numerous methods to estimate the exchange fluxes between groundwater and surface water, which are comprehensively covered in textbooks and review papers (Brodie *et al.* 2007, Clark & Fritz 1997, Dingman 2008, Domenico 1972, Freeze & Cherry 1979, Kalbus *et al.* 2006, Rosenberry & LaBaugh 2008, Sophocleous 2002), together with their main advantages and limitations. Only the key concepts of the methods and their underlying assumptions are presented below.

### *Field methods in measuring GW-SW exchange*

One of the simplest and most widely applied methods to estimate fluxes across the GW-SW interface is to apply Darcy's Law by measuring hydraulic gradients and hydraulic conductivity near or at the GW-SW water interface (Freeze & Cherry 1979). Hydraulic head, and thereby hydraulic gradient, can be measured accurately with various installations, usually consisting hollow pipes or rods that are mounded to known depth in the groundwater flow system (Cherkauer & Zager 1989, Lee & Cherry 1979, Smerdon *et al.* 2005, Winter 1976). The difference in hydraulic head and distance between the mounded location and surface water elevation can be used to establish the hydraulic gradient. The main problem with applying the Darcy's Law is the inherent uncertainty in determining a representative value for the hydraulic conductivity of the porous medium between the points of measured hydraulic head (Kalbus *et al.* 2006).

Instead of relying on an indirect flux estimate via the hydraulic gradient, flux at the GW-SW interface can be directly measured with a seepage meter. The seepage meter, also referred to as a seepage chamber, is a simple, inexpensive and most commonly used method for directly measuring seepage flux between groundwater and surface water bodies (Brodie *et al.* 2007, Rosenberry *et al.* 2008). In its original design (Lee 1977), the device consists of a chamber enclosing a part of a lake or stream bed. Volume of water flowing in to or out of the bed section enclosed by the chamber is then measured using a collection system. When water volume change over time is measured for a given cross-sectional area, specific discharge ( $v$ ) can be calculated. Several modifications have been successfully made to the original design to integrate larger spatial scope or to measure the flux continuously (e.g. Cherkauer & McBride 1988, Kidmose *et al.* 2011, Krupa *et al.* 1998, Rosenberry 2008, Rosenberry 2005, Rosenberry *et al.* 2013, Tryon *et al.* 2001).

The above methods rely on hydraulics either by measuring specific discharge directly or by resorting to estimates of hydraulic gradient and hydraulic conductivity. However, GW-SW exchange can also be estimated based on the observation that physical and chemical properties are often different for groundwater and surface water, as a result of various interactions between water molecules and soil particles in the subsurface (Freeze & Cherry 1979). Thus the naturally occurring increase in concentrations of e.g. major cations and silicate along groundwater flow can be used to show the groundwater influence in surface water bodies (Soveri *et al.* 2001, Webster *et al.* 1996, Wels *et al.* 1991, Winter & Carr 1980). In addition to water chemistry, water isotopic composition is widely used as an environmental tracer

(Clark & Fritz 1997, Gat 1996). Data on environmental tracers, chemical or isotopic, can be used qualitatively to increase conceptual process understanding of the exchange. They are also suitable for quantitative estimates of groundwater inflow via mass balance and mixing analysis (Jones *et al.* 2006, Krabbenhoft *et al.* 1990b, Laudon & Slaymaker 1997, Rozanski *et al.* 2001).

In addition to tracers analysed in water samples, heat provides a good environmental tracer, as there is often a marked temperature difference between GW and SW (Anderson 2005). Temperature is easy and inexpensive to measure, and the physical basis of energy transport is well established (Kalbus *et al.* 2006). Therefore use of the tracer has generated a multitude of applications spanning a range of spatially detailed temperature profiling (Anibas *et al.* 2011, Brookfield *et al.* 2009, Conant 2004, Jensen & Engesgaard 2011, Sebok *et al.* 2013) to areal thermal imaging using aircraft and satellites (Handcock *et al.* 2006, Mallast *et al.* 2013, Rundquist *et al.* 1985). Differences in temperature can be used to establish rate of GW-SW exchange and spatial occurrence of the exchange.

### *Numerical modelling*

Since early stages, analytical and numerical solutions to groundwater flow equations have played a key role in developing process understanding and formulating new hypotheses to be tested in the field of GW-SW interaction studies. Early studies on groundwater-lake interactions, many of them conducted by T.C Winter, commonly focused on two-dimensional (2-D) cross-sections with simple geometries and geological settings due to computational limitations (Winter 1976, Winter 1981, Winter & Pfannkuch 1984). Even though modelling (and research) communities were, and still largely are, divided into groundwater and surface water hydrologists, already Freeze and Harlan (1969) outlined a blueprint for a physically-based hydrological model which could eventually combine the groundwater and surface water domains. Later, with the advances in computational technology, the simulation problems for GW-SW interactions have increased notably in size and complexity (Hunt *et al.* 2003, Sophocleous 2002), with rapid ongoing development to fulfil the concept of Freeze and Harlan (Maxwell *et al.* 2014).

The majority of GW-SW interaction field studies involving numerical modelling are performed within the context of spatially distributed hydrological models. In these models, fully saturated subsurface flow is solved using spatially (and sometimes temporally) discretised partial differential equations based on Eq. (1), which can be extended to consider variably saturated conditions by modifying it to include the

Richards equation (Richards 1931). Surface water features in the models are commonly treated as: 1) Model boundary conditions with only one-way water exchange (Ataie-Ashtiani *et al.* 1999, Okkonen & Kløve 2011); 2) discrete features with mass balance and linear water exchange with the subsurface system (Anderson & Cheng 1993, McDonald & Harbaugh 1988, Prudic *et al.* 2004); or 3) partial differential equations, most commonly the Saint-Venant equation, simulating spatially distributed surface water flow (Maxwell *et al.* 2009, Panday & Huyakorn 2004).

A fundamental concept to note from the model concepts above is that the water flow (and/or storage) in the GW and SW domains is expressed with different mathematical formulations. Therefore the GW and SW domains must communicate in a way which ensures conservation of mass and continuity of momentum at the model interface (Furman 2008). The modelling community refers to this exchange of information as model coupling, which is necessary for all models simulating GW-SW exchange. However, the physical conceptualisation and numerical implementation of model coupling varies between applications. Regardless of the approach, the GW-SW interaction is simulated when water is exchanged between the domains.

HydroGeoSphere (HGS), which was used to simulate GW-SW interactions in this thesis, is an example of a state-of-the-art, fully integrated surface-subsurface model (Aquanty 2013). HGS uses a controlled volume finite element approach and is capable of simulating the interconnected flow processes of subsurface and surface water. The fully integrated approach allows water input as rainfall and snowmelt to be partitioned into different components (surface or overland flow, evaporation, infiltration to unsaturated soil or directly to groundwater) in a physically-based fashion. Both surface and subsurface (saturated and unsaturated) flow regimes are solved simultaneously at each time step, allowing water to be exchanged naturally between the domains. Surface flow is solved with a 2-D diffusion-wave approximation of the Saint-Venant equation and saturated/unsaturated subsurface flow with the Richard's equation. An integrated evapotranspiration (ET) module is used to simulate actual ET from surficial soil layers based on potential ET time series and soil moisture conditions. HGS has proven to be versatile and high performing in simulating hydrological responses of systems ranging from metres to catchment and continental spatial scale (Brookfield *et al.* 2009, Brunner & Simmons 2012, Goderniaux *et al.* 2009, Lemieux *et al.* 2008, Sudicky *et al.* 2010). It has been used as a reference code in simulating GW-SW interactions (Brunner *et al.* 2010). Even though benchmark testing of HGS and other surface-subsurface codes has only just started (Maxwell *et al.* 2014), the main conclusion so far is that the models are

capable of successfully reproducing the main hydrological processes in both surface and subsurface flow.



## 3 Study site: Rokua esker aquifer

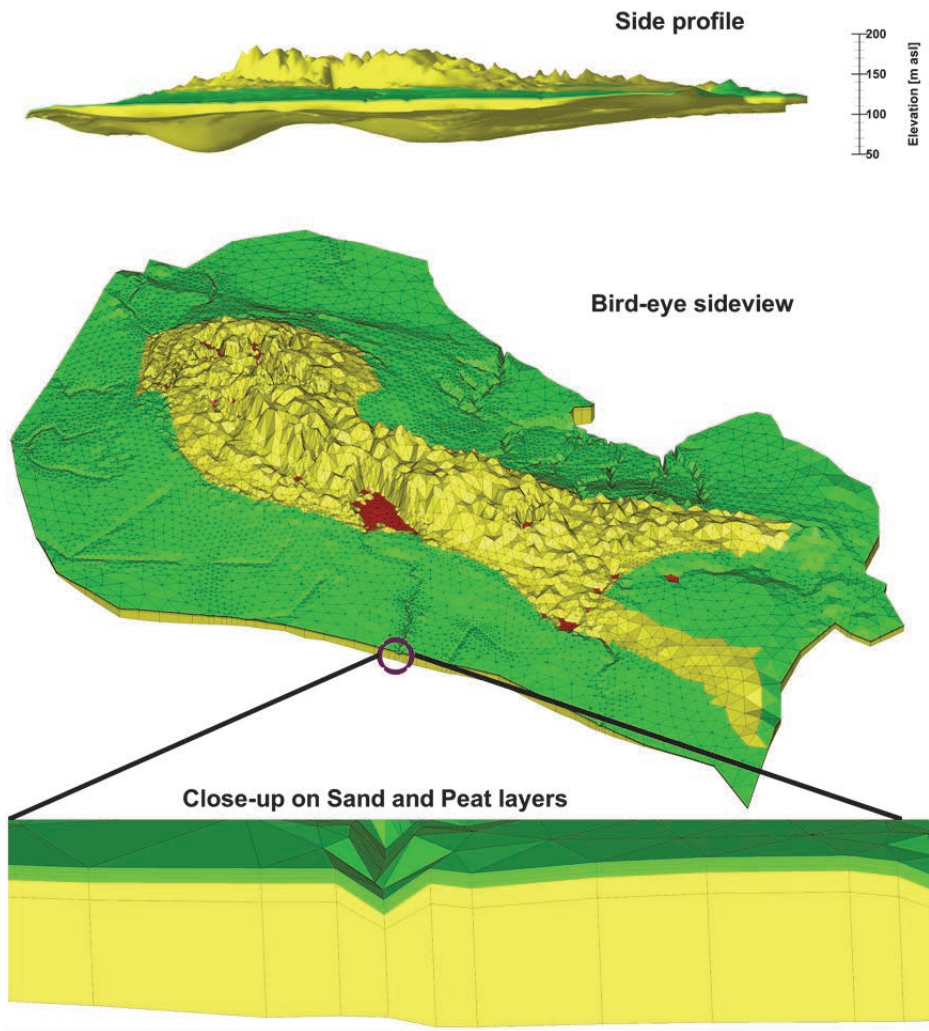
### 3.1 Hydrogeological characteristics

Esker aquifers are abundant in the Fenno-Scandinavian shield and are common in other regions covered by the last glaciation (Svendsen *et al.* 2004). Eskers are permeable, unconfined sand and gravel aquifers associated with deglaciation (Banerjee 1975). Rivers of melting ice deposited sandy sediments in the river channel under the ice sheet. A gravel core is usually found in the central part of esker aquifers in the direction of glacier withdrawal, as the first phase of the glacialfluvial sediment is stratified in a high velocity meltwater flow (Mälkki 1999).

The Rokua esker aquifer is part of a long esker ridge stretching inland from the North Ostrobothnian coast (Aartolahti 1973). The deposited overburden of glaciofluvial origin consists of fine and medium sand sediments, mainly of quartz, originally eroded from sedimentary rock of the Muhos formation (Aartolahti 1973, Pajunen 1995). Rokua has rolling terrain because of kettle-holes, wave action and aeolian dunes. The thickness of the sand deposits varies from 30 m to more than 100 m above the bedrock (Fig. 2). The sandy aquifer is underlain by crystalline bedrock consisting mainly of igneous migmatite gneiss and granite (Aartolahti 1973).

Hydrologically, the Rokua esker aquifer is a very complex, unconfined aquifer system with lakes and streams in the aquifer recharge area and groundwater-fed springs and streams in the groundwater discharge area (Figs. 1 and 3). The most important landscape feature as regards the work in this thesis is kettle-holes, which formed during deglaciation from large blocks of ice encased within the sand deposits. When the ice later melted, a depression was left in the landscape (Mälkki 1999). The size of these kettle-holes at Rokua varies widely, with their depth ranging from 1–2 m to 40 m and their diameter from some 10 m to 1.5 km long by 0.4 km wide (Aartolahti 1973). The majority of the kettle-holes are dry, but approximately 90 lakes or ponds with surface area ranging from 0.02 to 165 ha are located in the area.

Eskers consist of permeable sandy soils and gravels and therefore surface runoff is usually minor. Instead, water from subsurface flow ponds in landscape depressions such as kettle-holes. Kettle-hole lakes are usually embedded in the aquifer and their water level and water chemistry are highly dependent on the groundwater system (Winter *et al.* 1998). In addition to the physical characteristics of the lakes, groundwater exchange affects lake ecosystems by providing nutrients, inorganic ions and a stable water temperature (Hayashi & Rosenberry 2002).



**Fig. 2. Conceptual model of aquifer geology as used in Paper IV for the porous media domain. Yellow represents sand soil layers and green peat soil layers blanketing the sandy aquifer in the discharge area. Red areas represent lake bed sediments. Vertical exaggeration is 25 times the horizontal in all three meshes.**

The groundwater discharge zone at Rokua is extensively covered by peatlands (Fig. 2), which started to form between littoral deposits of different phases of the Baltic Sea after the glacial retreat, around 8000 years ago (Pajunen 1995). Peat is an organic soil



type characterised by high water content and low hydraulic conductivity (approx.  $10^{-7}$ – $10^{-9}$  m s<sup>-1</sup>), especially in the humified catotelm layer in deep parts of the peat soil profile (Päivänen 1973, Price 1992, Ronkanen & Kløve 2005, Silins & Rothwell 1998). However, double porosity, where preferential ‘pipe-like’ flow channels are found in the peat matrix, can introduce a bypass route for water flow (Holden & Burt 2002, Ours *et al.* 1997). The majority of the Rokua peatlands were drained during the 1950s to 1980s by excavating open channel ditches to improve conditions for forest growth.

### *Problems with varying lake water levels and eutrophic water quality*

The geological and ecological uniqueness of the Rokua esker area is widely acknowledged. Rokua was recently granted membership of the UNESCO GeoPark Network and it is also part of the Finnish nature reserve network, since part of the area is protected as a Finnish National Park (Fig. 4). Some ecosystems in the area are protected by Natura 2000 (Metsähallitus 2008). Most of Rokua’s kettle-hole lakes and ponds are of high ecological and recreational value because of their crystal clear waters (Anttila & Heikkinen 2007). The lakes are widely used for recreational activities such as fishing, swimming and scuba diving, and many of the lake shores are populated with holiday homes and hotels.

Kettle-hole lakes in the Rokua esker aquifer are affected by two problems: 1) Periodically declining water level in closed basin lakes (seepage lakes); and 2) eutrophication of lakes with a surface water outlet (drainage lakes). The periodic decline in lake water level, especially after a dry period at the beginning of the 2000s, has raised concerns about the future of the lakes (Anttila & Heikkinen 2007). At this point, several factors have been suggested as the reason for the decline. Land use in the surrounding peatlands is suspected to be one of the main reasons, but more scientific research is needed to understand the magnitude of different factors contributing to lake level variability (Koundouri *et al.* 2012). Water quality in the closed basin lakes is optimal for recreational use, but a permanent lake water level decline would be disadvantageous for both the ecological and recreational values of the Rokua area.

The lakes that are suffering from eutrophic conditions, manifested in poor water quality (high phosphorus concentrations and occasional oxygen depletion) and algae blooms (Väisänen *et al.* 2007), are different from those in which water levels are periodically declining. Nutrient loading from anthropogenic sources can be considered to be a minor nutrient source for both oligotrophic and eutrophic lakes.

The only obvious difference between the two lake types is surface water outlets, which exist only in the eutrophic chain of lakes. However, previous studies have not explained why some lakes in the Rokua area are distinctly more eutrophic than others, despite being located in similar hydrogeological settings.

### **3.2 Data collection network**

The data presented in this section are common to Papers I-IV. The majority of the collected data refer to geological structure, climate variables, groundwater and lake level recording and stream flow monitoring.

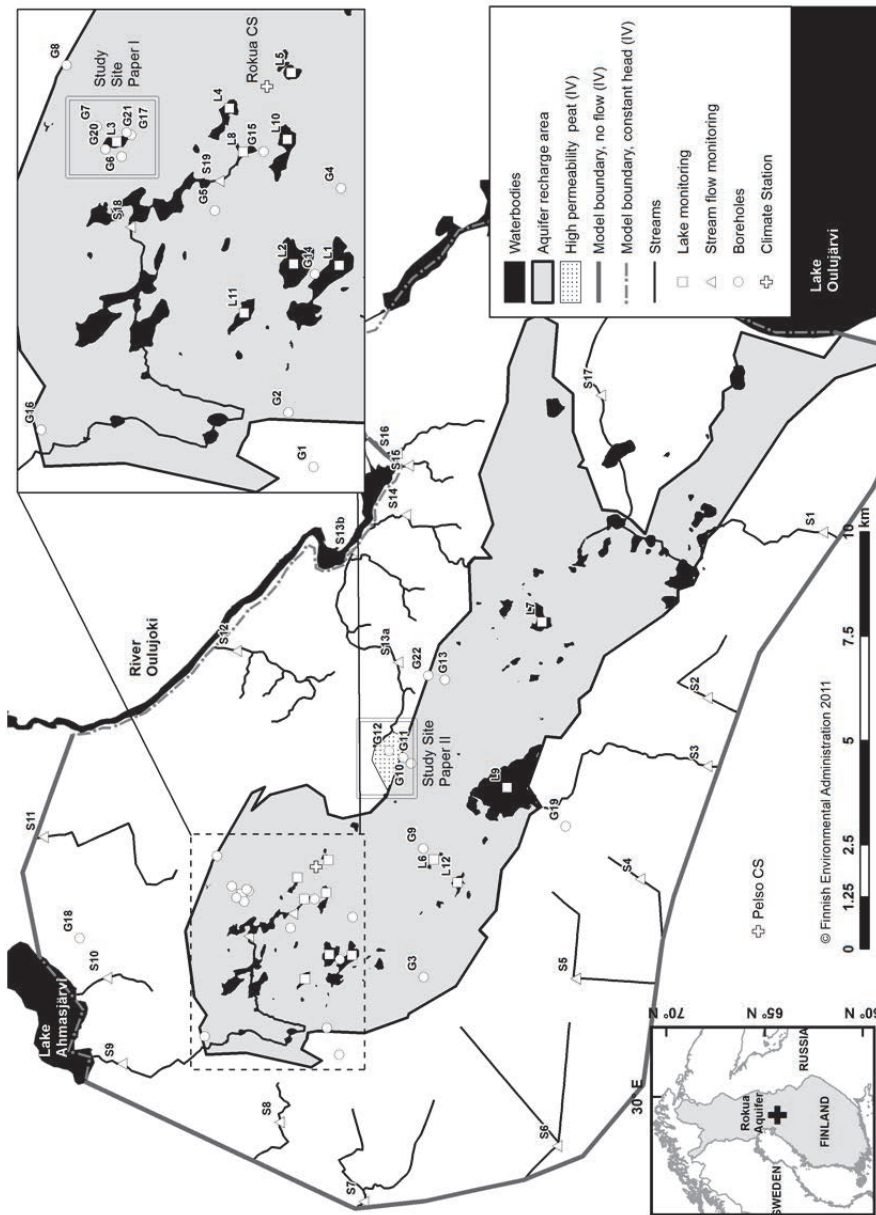
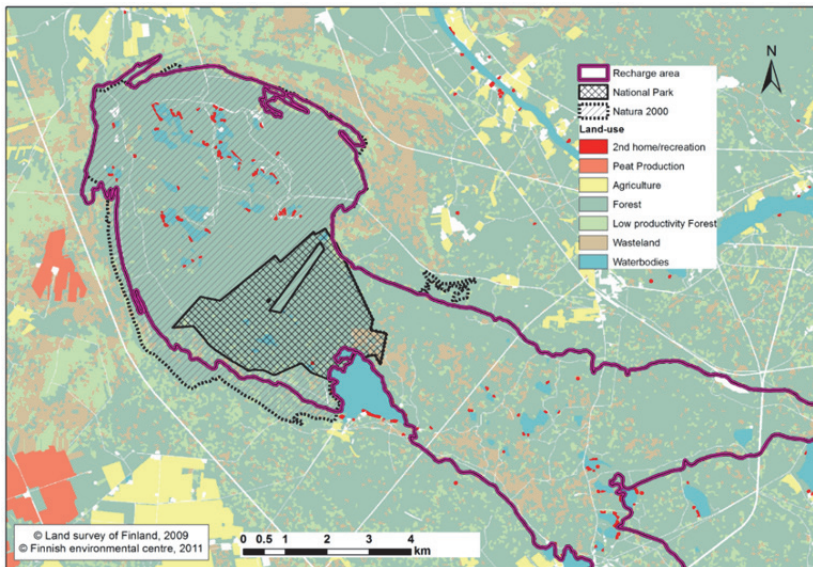


Fig. 3. Monitoring network for lake and groundwater levels, stream flow and climate stations. The map shows the model boundaries used in Paper IV and the study site locations for Papers I and II.

## Land use

Land use in the Rokua aquifer and the surroundings consists mostly of forests used for commercial forestry activities (Fig. 4). Some agricultural and peat production areas are present outside the groundwater recharge area. Small-scale anthropogenic developments, such as second homes, recreation facilities and paved roads, have been constructed around kettle-hole lakes. Water extraction from four intake stations in the aquifer was in total below 500 m<sup>3</sup>/d and has been concluded to have minimal effects on aquifer water storage.



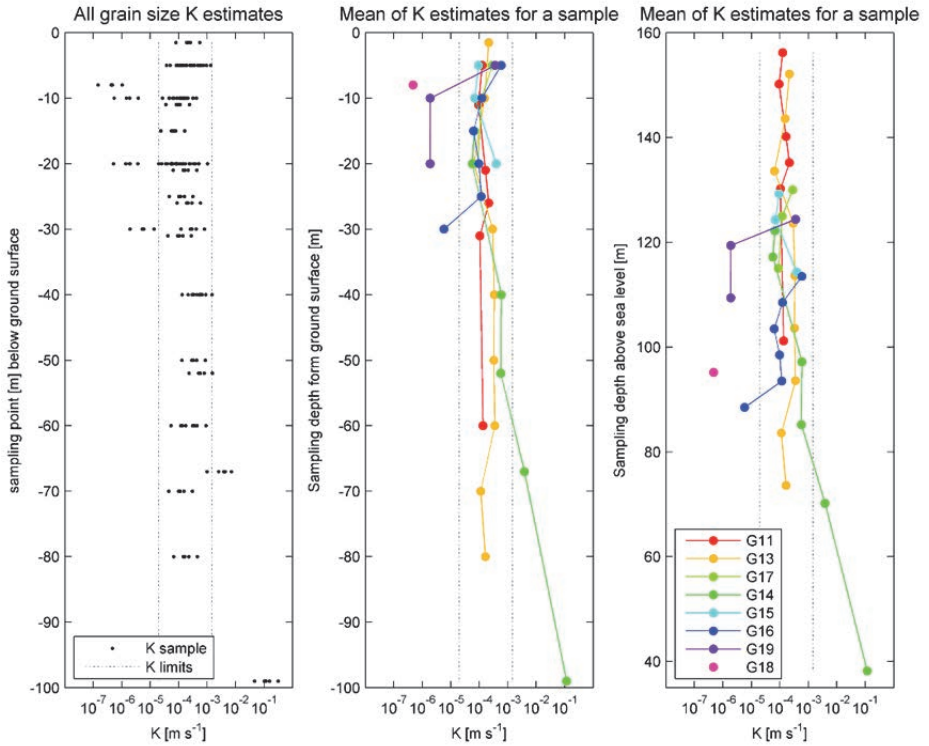
**Fig. 4. The main land coverage types in the Rokua esker area. Forest land dominates, with most of that outside the natural conservation areas being used for commercial forestry (National Land Survey of Finland 2009).**

## Geological data

Rokua has been geologically surveyed with partially penetrating borehole drillings in previous studies, but to a maximum depth of 20–30 m and without any bedrock confirmation (Heikkinen & Väisänen 2007, Tuomikoski 1987). From 2008 to 2010, the University of Oulu and Geological Survey of Finland mapped the Rokua esker geology with 150 km of ground-penetrating radar line and 5 km of seismic

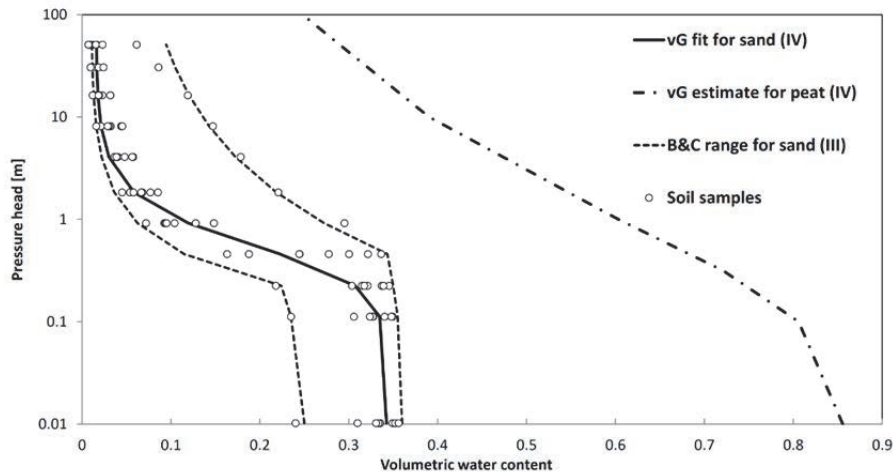
refraction/reflection measurement line (Rossi *et al.* 2014). These surveys revealed fine and medium sand in the esker area, with deposit thicknesses of over 80 m above the bedrock. Borehole logs of soil type from earlier studies characterised the soil type mainly as medium, fine or silty sand throughout the model domain, with some local loam lenses and gravel deposits (Aartolahti 1973, Heikkinen & Väisänen 2007, Tuomikoski 1987). However, detailed information on soil hydraulic properties was not available. The existing borehole logs were supplemented with additional borehole drillings, both partially and fully penetrating, during the course of this thesis work (Fig. 3 and Appendix 1). Bedrock surface was identified from geophysical data and fully penetrating borehole drillings with bedrock confirmation, and a full bedrock surface was interpolated using the points of observed bedrock.

Particle size distribution was determined for 37 soil samples taken from eight boreholes of various depths (Appendix 1, Fig. 3, Fig. 5). Particle size distribution data were employed to calculate the range of saturated hydraulic conductivity for the samples, using empirical equations by Hazen, Kozeny-Carman, Breyer, Slitcher and Terzaghi (Freeze & Cherry 1979, Odong 2007). Soil sample hydraulic conductivities were plotted as a function of sampling depth (below ground surface and above sea level; Fig. 5). The samples were mainly characterised as fine or medium sand, similarly to previous borehole logs reported in Heikkinen and Väisänen (2007) and Tuomikoski (1987). In borehole G14 (see Fig. 3), a gravel deposit was found in the bottom of the borehole. Coarse material was also found in the eastern parts of Rokua, near Lake Oulujärvi, in earlier surveys, but besides these observations no continuous gravel was found based on data from the other boreholes or any of the geophysical measurements. Four soil samples consisted of finer sediments with order of magnitude lower K values. On combining the available data from prior borehole logs and the geophysics and drillings performed, there was no evidence of different stratigraphical layers, which could have been used to assign different permeability to soil layers in a scale relevant for the models used in Papers III and IV.



**Fig. 5. Hydraulic conductivity (K) values calculated from the soil sample particle size distributions. Plots show (left) the estimated K values for all samples (5 calculations per sample), (centre) the geometric mean K for each sample as a function of sampling depth below the ground surface, and (right) the geometric mean K for each sample as a function of sampling depth above sea level. The dashed line ‘K limits’ indicates the range of soil hydraulic conductivity ( $1.99 \cdot 10^{-5}$ – $1.47 \cdot 10^{-3} \text{ m s}^{-1}$ ) used in Papers III and IV.**

Nine samples taken from borehole G10 were used to estimate pressure-saturation data from parameterisation of the Brooks and Corey equation (Paper III) and van Genuchten equation (Paper IV) (Fig. 6).



**Fig. 6. Soil sample pressure-saturation data for sandy soil and parameterisation of the soil pressure-saturation relationship used in Papers III and IV.**

The soil data were used to define ranges for sand hydraulic conductivity in Papers III and IV. In Paper III, the range  $1.99 \cdot 10^{-5}$ – $1.47 \cdot 10^{-3} \text{ m s}^{-1}$  was selected to cover the minimum and maximum hydraulic conductivities based on the boreholes in the recharge area (excluding G18 and G19) and within the unsaturated layer thickness (sampling depth <50 m, excluding deep samples in G14). This range is in line with typical hydraulic conductivity values for medium, fine and silty sand (Freeze & Cherry 1979). The range was considered to reasonably represent the typical hydraulic conductivity range in the study area for both of the modelling studies.

The Geological Survey of Finland has mapped peat thickness in parts of the study area with peat cores ( $n = 4000$ ) through the peat layer (Häikiö 2008, Pajunen 2009). The peat thickness varies from zero to over 5 m in the aquifer discharge zone, with an average thickness of 1.4 m. In the present work, peat hydraulic conductivity was measured for the peatland catchment study site (S13 in Fig. 3) with a direct-push piezometer with a falling head (Hvorselv 1951). The measurements verified the expected low hydraulic conductivity towards the bottom layer of the peat, with a  $K$  values of  $10^{-5} \text{ m s}^{-1}$  at a depth of 20 cm and  $10^{-9} \text{ m s}^{-1}$  at a depth of 200 cm.

An organic gyttja layer covers lake bottoms in the area and is generally known to affect groundwater inflow to lakes (Kidmose *et al.* 2013, Smerdon *et al.* 2007, Viridi *et al.* 2013). This lakebed gyttja in Rokua has its origins in peat accumulated in the bottom of ancient kettle-holes, which were later submerged and turned into lakes and

ponds as a result of rising groundwater level (Pajunen 1995). The extent of the gyttja layer was studied with ground-penetrating radar at site L3, by using the equipment on top of lake ice cover. The gyttja was absent in the immediate vicinity of the shoreline, but in the middle of the lake the gyttja layer reached a thickness of 5 m. A similar structure of the bottom cover, with sand near the shoreline and gyttja in the centre, has been observed on dives in several of the area's lakes. Field analysis of the gyttja core showed that it contained highly decomposed organic matter with increasing mineral soil content towards the bottom.

### *Climate data*

The climate at the Rokua aquifer is characterised by precipitation exceeding evaporation on an annual basis. Mean annual values (and standard deviations) during 1960–2010 were 591 mm (91 mm) for precipitation and 426 mm (26 mm) for FAO reference evapotranspiration calculated according to Allen *et al.* (1998). Another important feature of the climate is annually recurring winter periods when most precipitation accumulates as snow. Mean annual temperature for the period 1960–2010 was  $-0.7\text{ }^{\circ}\text{C}$  ( $1.1\text{ }^{\circ}\text{C}$ ).

Meteorological data were mainly obtained from two sources; the Finnish Meteorological Institute (FMI), and measurements made with a climate station established during the project (see Fig. 3). Other databases were also utilised to some extent, for details see Appendix 2. Data obtained from FMI had been collected according to the Institute's standard practices and were supplied as time series from FMI databases. Because long historical time series of data were available only from FMI, climate data records from Rokua climate station were used to verify the applicability of FMI data for study site conditions.

### *Monitoring of lake and groundwater levels and stream discharge*

Data on groundwater and lake levels were collected with manual measurements and automated dataloggers (Solinst Levellogger Gold). The Centre for Economic Development, Transport and the Environment (ELY Centre) started the first intensive water level measurement campaign by installing groundwater boreholes and lake level scales in the area for manual water level recording (Anttila & Heikkinen 2007). The earliest data available are from 2004, with increasing temporal resolution and spatial scope since 2007. The automated dataloggers used in the present thesis were installed during 2008–2010 in the boreholes indicated in Appendix 1. Stilling wells



were installed in selected lakes to ensure high quality of lake level data. Groundwater and lake levels were recorded with hourly resolution and the quality of the automated measurements was verified with manual level measurements several times per year.

The outflow from the aquifer was monitored by measuring stream discharge in the aquifer recharge and discharge area (Fig. 3). The flow was measured by determining the flow velocity [ $\text{m s}^{-1}$ ] at different points of stream cross-section using a portable flow meter (Mini Air 20) and calculating the outflow [ $\text{m}^3 \text{s}^{-1}$ ] with respect to the cross-sectional surface area. All measurement locations were surveyed within 2-3 days in a given measurement round. Frequency of measurements was approximately every six weeks during May 2009–July 2011 and every three months from August 2011 to October 2012.

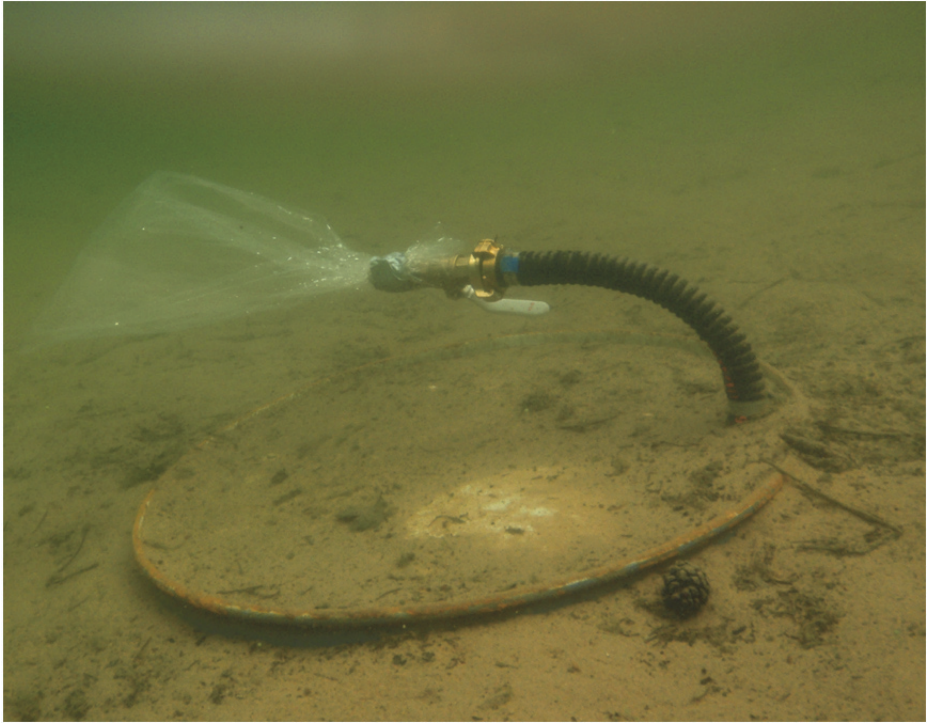


## **4 Materials and methods**

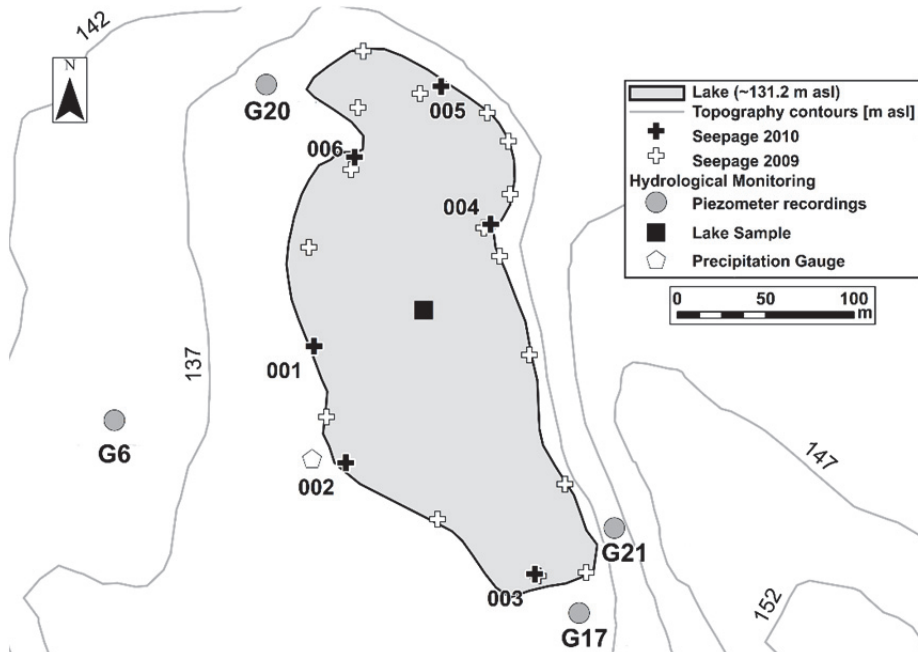
### **4.1 Field methods to study GW-SW interactions**

#### ***4.1.1 Seepage meter measurements (I)***

Seepage meter measurements were performed in lake L3 in order to: 1) Verify the interaction between the lake and the aquifer; 2) determine the spatial distribution of lake seepage rates; 3) study temporal variations in seepage rate within specific locations; and 4) compare the temporal variations in lake seepage and changes in lake and groundwater levels and determine whether changes in levels were reflected in lake seepage rates. The seepage meters constructed in Paper I resembled the design introduced by Lee (1977). The equipment consisted of a 208-L steel drum barrel (diameter 57 cm) with a cut-off end, a plastic bag and a smooth 20 cm connection hose between the bag and the chamber (Fig. 7) A total of six seepage meters, all identical in design and components, were used in Paper I. Most common sources of error occurring in seepage meter studies according to Rosenberry *et al.* (2008) were acknowledged in both seepage meter design and in carrying out the measurements (for full details see Paper I).



**Fig. 7. Seepage meter in operation in Lake Ahveroinen (L3). The chamber was pushed into the sandy lake bed sediment and water flowed into the plastic bag through the connection hose. Picture by Riku Eskelinen.**



**Fig. 8. Hydrological monitoring locations in Lake Ahveroinen (L3). Spatial distribution of seepage meter measurements for the two years is represented as crosses of different colours and the locations used to study temporal seepage variability during 2010 are named (001–006). Reprinted with permission from Elsevier (Paper I).**

The first set of seepage meter measurements focused on determining the spatial distribution of seepage direction and rate at site L3 (Lake Ahveroinen). The spatial distribution of seepage rates around the lake in 2009 was determined at 16 locations (Fig. 8). The second set of seepage meter measurements studied temporal variations in seepage rate. Eight seepage meter measurements were made at six locations (Fig. 8), at approximately 3-week intervals. A full description of the measurements is given in Paper I.

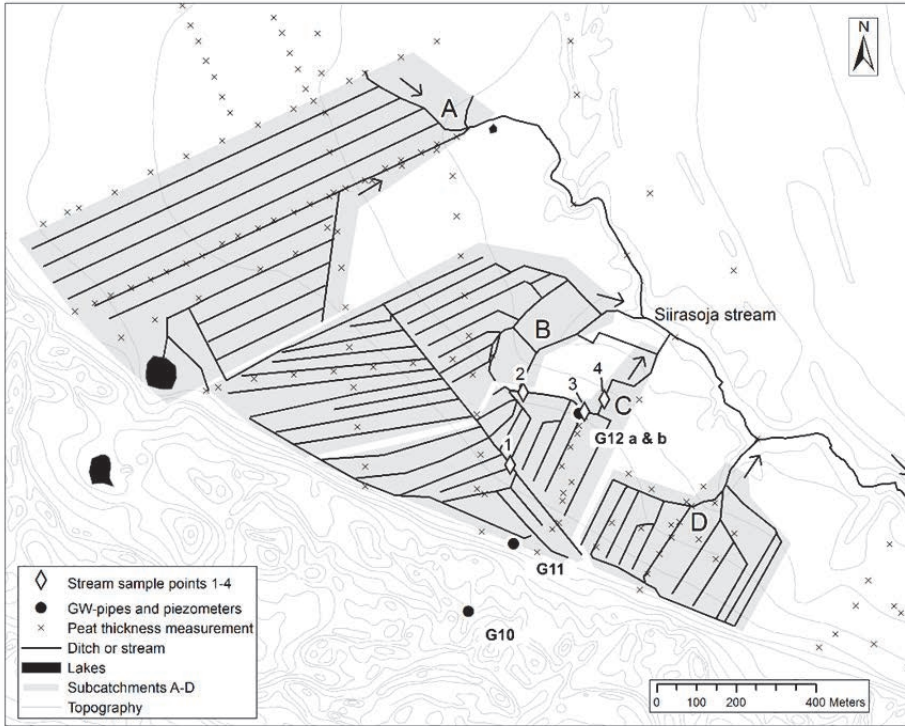
*Statistical analysis of seepage meter measurements and hydrological observations*

In order to detect whether changes in seepage rate co-varied with changes in the surrounding hydrogeology, the correlation between seepage velocities and lake and

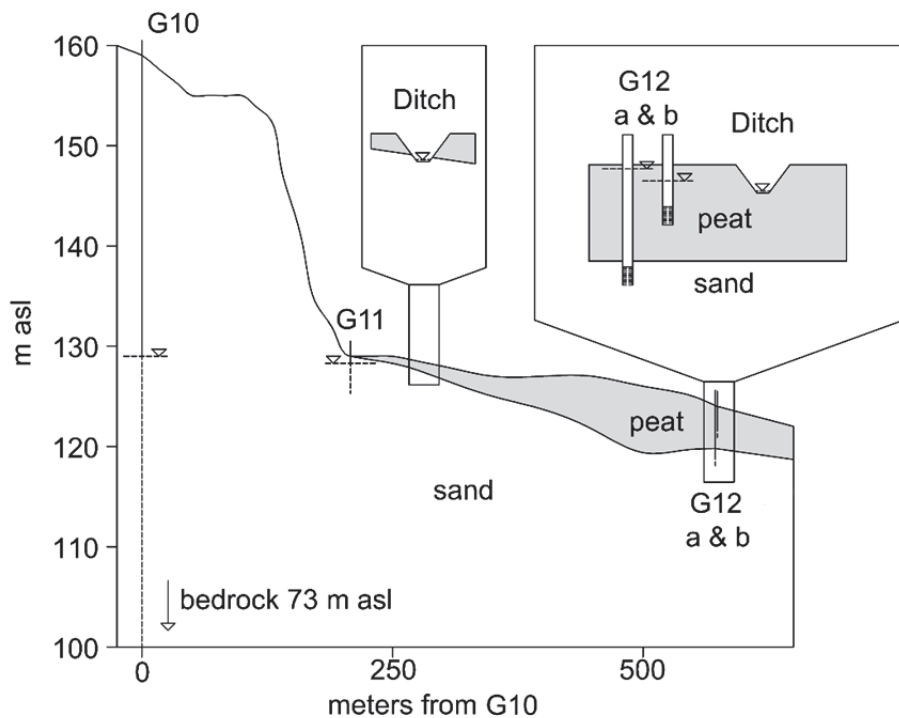
groundwater levels was analysed on the date of seepage measurements. In order to acknowledge the linear relationship between hydraulic gradient and groundwater flow velocity (in this case seepage velocity), Pearson correlation coefficient expressing linear correlation was used in the analysis and correlations with p-values below 0.05 were considered to demonstrate a strong correlation. It should be noted that reported p-values for correlations between seepage measurements and hydrological observations are prone to type I errors, because the seepage measurements themselves are correlated and thus the variables are not independent. However, the aim in the present work was to examine whether the seepage rates respond to different parts of the hydrogeological system and for that purpose p-values provided a convenient cut-off point to classify locations into correlated and non-correlated, even though the statistical validity of significance was compromised.

#### ***4.1.2 Hydraulic measurements in the peatland drainage network (II)***

Groundwater discharge into drained peatland was studied in the upper catchment area of the Siirasoja stream (S13, see Fig. 3). S13 had one of the highest baseflow runoff values recorded in the Rokua study site catchment and therefore a strong groundwater influence on the drainage ditch network was suspected in the area. The study site (1.5 km<sup>2</sup>) was divided into four subcatchments A–D (Fig. 9) to study the spatial variability in groundwater discharge. At the southern side of the peatland, where the soil type transitions from peat to sand, the sandy esker formation rises with a steep 30% slope (Fig. 10).



**Fig. 9. Diagram of the Siirasoja stream catchment study site (S13) showing its four subcatchments A–D, groundwater monitoring wells (G10, G11), piezometers (G12a & b), stream water sampling points, and peat thickness measurement points. Reprinted with permission from Elsevier (Paper II).**



**Fig. 10. Cross-section along the monitoring well installation line in the Siirasoja stream catchment (S13) (with 10:1 vertical exaggeration) showing the thickness of peat and sand deposits and the groundwater monitoring well installation set-ups. Reprinted with permission from Elsevier (Paper II).**

The drainage ditches in the subcatchments were mapped for water flow rate and presence of spring-like groundwater exfiltration points *in situ* during low-flow season in July 2009. Point discharges were first visually identified and then confirmed with water temperature measurements before and after the observed point discharge. Groundwater during the monitoring period was colder than rain-fed surface water, and the temperature difference was used as a tracer for groundwater inflow. When no point discharge was observed but the flow rate in the drainage ditch was increased and water temperature was low, ditches were considered to receive groundwater seepage. Groundwater level in both the sand aquifer and peat soil (Figs. 9 and 10) was recorded with automated levelloggers (see Section 3.2) to establish the hydraulic gradients at the site.



### **4.1.3 Environmental tracers (I & II)**

The environmental tracers calcium ( $\text{Ca}^{2+}$ ), silica ( $\text{SiO}_2$ ) and the ecologically significant nutrient phosphate ( $\text{PO}_4^{3-}$ ) were used to study GW-SW interactions at aquifer scale (Paper I) and surface water body scale (Papers I and II) in the Rokua aquifer. The environmental tracers were used to look for similarities and/or differences in groundwater and surface water chemical composition throughout the aquifer. Of the selected tracers, phosphate is not a suitable environmental tracer as such because of its active biological uptake and tendency to be adsorbed on soil minerals and organic matter. However, below the organic-rich and biologically active soil zone, the amount of phosphorus in groundwater is mainly controlled by the solubility of sparingly soluble phosphate-bearing minerals (Freeze & Cherry 1979). In this respect groundwater inflow can provide a phosphate source to lakes (Devito *et al.* 2000, Kidmose *et al.* 2013, Shaw *et al.* 1990).

#### ***Sampling strategies for environmental tracers***

Water samples were taken in all relevant hydrological compartments of the study aquifer (10 piezometers, 13 lakes, 9 streams, 1 snowfall) at a total of 33 locations (Fig. 3, Appendix 1). Details about the sampling procedure and analysis methods are given in Paper I. On aquifer scale, tracer concentrations were statistically compared against the altitude of the sampling location using the rank-based Kendall correlation analysis. The underlying assumption was that water sampled at lower altitudes had travelled along a longer flow path in the subsurface and would therefore be richer in tracers indicating mineral weathering and dissolution (Kenoyer & Bowser 1992, Webster *et al.* 1996, Winter & Carr 1980, Winter 1999). In addition, phosphate concentrations were compared with calcium and silica concentrations in order to determine whether the phosphate concentrations in different parts of the study site were related environmental tracers known to reflect the length of the subsurface flow path. For descriptive statistics, the median was selected as the measurement of central location and the interquartile range as the measurement of spread because of observed non-normal distribution, especially of phosphate samples.

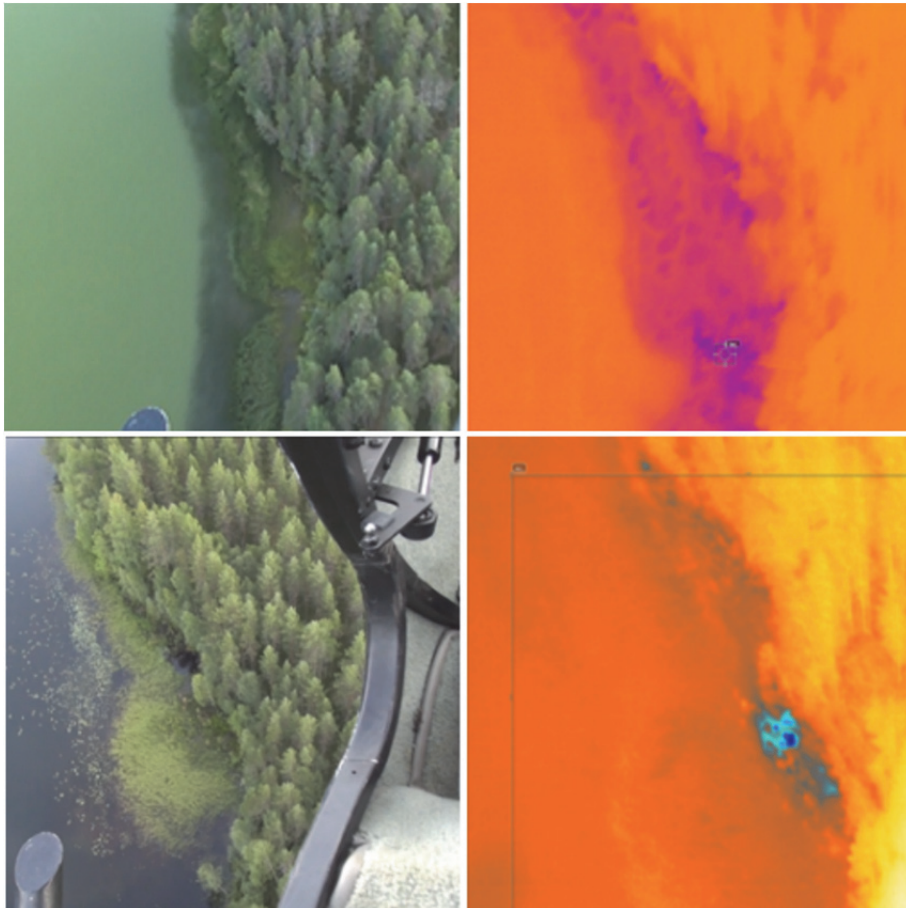
On the scale of a single lake, tracer concentrations of a surface water body (L3) and the adjacent groundwater were examined. In this case the aim was to look for differences in lake water and groundwater tracer concentrations and from that estimate the magnitude of groundwater influence and water flow directions. Sampling

was performed in piezometers near the lake (Fig. 8, Appendix 1) as part of the aquifer sampling.

In the drained peatland at the Siirasoja stream study site (Figs. 9 and 10), environmental tracers were used to characterise the groundwater flow path in the aquifer beneath the peat layer and to estimate the contribution of groundwater exfiltration to stream flow. Samples were taken during the field study campaign in June 2010. Water was sampled from stream water (sample points 1–4), groundwater wells and piezometers, and precipitation (Fig. 9, Appendix 1). In the drained peatland area, the samples were also analysed for pH and electrical conductivity (EC) to supplement the other analyses.

#### **4.1.4 Airborne thermal infrared imaging (IV)**

Water surface temperature was used as a tracer to identify locations where groundwater discharges into lakes. Airborne thermal infrared imaging (TIR) for the lakes was conducted from a helicopter on 5 August 2013, because at around this time of year the temperature difference between the lake water (~20 °C) and the groundwater (~4.5 °C) is highest. Imaging was performed using the Flir Thermacam P-60 thermal camera with 320 x 240 pixel sensor resolution and an aperture of 24°. It covered the electromagnetic spectrum from 7.5 to 13 µm. The imaging was carried out from 150 m above the lake surface, making the pixel size approximately 15 cm x 15 cm. Temperature gradients were identified visually from the TIR images. Lakes were imaged only for their shoreline and the central areas of the larger lakes were omitted. Theoretically the groundwater in seepage rates should be greatest near the shoreline, close to the 'break in slope' the surface water body exerts on the groundwater level (Freeze & Cherry 1979), a phenomenon previously shown in field and modelling studies (Barwell 1981, Cherkauer & Nader 1989, Rosenberry & LaBaugh 2008). Another reason to focus on lake shorelines was that the method records the skin temperature of the water surface and therefore groundwater discharge deeper in a lake is likely to be undetectable as colder groundwater is mixed within the water column (Torgersen *et al.* 2001). When a temperature pattern on the lake shoreline suggested anomalously cold temperature (Fig. 11), the spatial coordinates were saved in ArcGIS software (ESRI 2011).



**Fig. 11.** Example of data obtained from air-borne thermal imaging (TIR) comprising (left) screenshots from a normal video camera and (right) thermal infrared images at the same location showing (upper image) an example of diffuse inflow (large purple area) and (lower image) focused inflow (small blue area). The maximum temperature difference is  $\sim 5$  °C in the upper image and  $\sim 10$  °C in the lower image. The colour schemes vary between the pictures. Pictures by Pekka M. Rossi.

## **4.2 Simulations for spatially and temporally distributed recharge (III)**

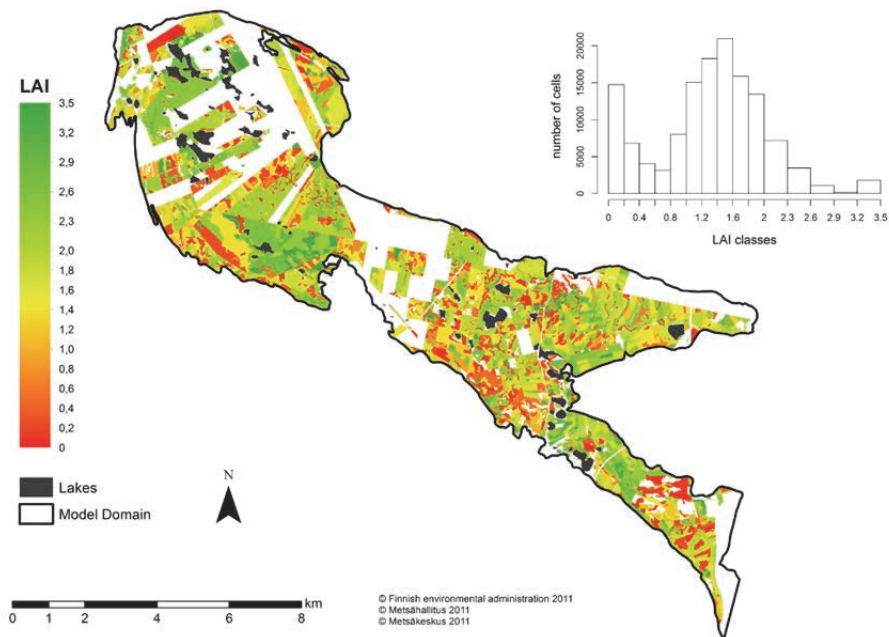
Detailed information about the groundwater recharge in Rokua esker aquifer was acquired by a numerical modelling study (Paper III). This sought to expand the application of physically-based 1-D unsaturated water flow modelling (Assefa & Woodbury 2013, Hunt *et al.* 2008, Jyrkama *et al.* 2002, Keese *et al.* 2005, Okkonen & Kløve 2011) to simulate spatial and temporal variations in groundwater recharge, while taking into account detailed site-specific information on vegetation (pine, lichen), unsaturated soil thickness, cold climate and simulation parameter uncertainty. CoupModel (Jansson & Karlberg 2004) was used in simulations because of its ability to represent the full soil-plant-atmosphere continuum adequately and to include snow processes in the simulations (Okkonen & Kløve 2011). The modelling set-up developed in Paper III uses spatially detailed information on tree canopy properties and concentrates on simulating different components of evapotranspiration. Furthermore, it considers the effect that forestry land use has on vegetation parameters and how this is reflected in groundwater recharge. The simulation approach takes into account the variability in the unsaturated zone thickness throughout the model domain. Parameter uncertainty, often neglected in recharge simulations, is considered by using multiple random Monte Carlo simulation runs in the process of distributing the 1-D simulations spatially. The overall aim of Paper III was to provide novel information on groundwater recharge rates and factors contributing to the amount, timing and uncertainty of groundwater recharge in unconfined sandy eskers aquifers.

### **4.2.1 Vegetation and unsaturated zone parameterisation**

Forestry inventory data from the Finnish Forest Administration (Metsähallitus, MH) and Finnish Forest Centre (Metsäkeskus, MK) were used to estimate leaf area index (LAI) for the Rokua esker groundwater recharge area. The available data consisted of 2786 individual plots covering an area of 52.4 km<sup>2</sup> (62.4% of the model domain). The forestry inventories, performed mainly during 2000–2011, showed that Scots pine (*Pinus sylvestris*) is the dominant tree in the model area (94.2% of plots). For details of LAI calculation, see Paper III.

The calculated spatially distributed information on LAI (Fig. 12) was used to obtain an estimate of how different land use management options, already actively in operation in the area, could potentially affect groundwater recharge. Clear-cutting is

an intensive land use form in which the entire tree stand is removed, and it is carried out in some parts of the study area. The first scenario simulated the impact of clear-cutting by not resorting to the estimated LAI pattern at the site, but by using an LAI value of 0–0.2 for the whole simulated area. In the second scenario, which was the opposite of clear-cutting, the mature stand was assumed to have high LAI values of 3.2–3.5 found at the study site and reported in the literature (Koivusalo *et al.* 2008, Rautiainen *et al.* 2012, Vincke & Thiry 2008, Wang *et al.* 2004).



**Fig. 12. Spatial distribution of leaf area index (LAI) and a 20 m x 20 m cell-based histogram of LAI values. In areas where forestry inventory data were lacking, a weighted average value of 1.25 was used in simulations. CC BY 3.0 (Paper III).**

An organic lichen layer covers much of the sandy soil at the Rokua study site (Kumpula *et al.* 2000), so a lichen layer was included in soil evaporation (SE) calculations. Lichen vegetation has the potential to affect SE by influencing the evaporation resistance of soil and by intercepting rainfall before it enters the mineral soil surface (Kelliher *et al.* 1998). Although lichens do not transpire water, their structural properties allow water storage in the lichen matrix and capillary water

uptake from the soil (Blum 1973, Larson 1979). The lichen layer also increases soil surface roughness and thereby retards surface runoff (Rodríguez-Caballero *et al.* 2012).

In this thesis, water interception storage by the lichen layer was estimated from lichen samples. The mean water retention capacity of the lichen samples was found to be 9.85 mm (standard deviation (SD) 2.71 mm) and approximations for these values were used in model parameterisation (Table 1). In the simulations, the lichen layer was represented as an organic soil layer with similar Brooks and Corey (B&C) parameterisation as for mineral soil and the B&C parameters were included in the uncertainty analysis.

The thickness of the unsaturated layer was estimated by subtracting interpolated groundwater level from digital elevation model (DEM) topography calculated based on LiDAR data (National Land Survey of Finland 2012). Groundwater elevation was estimated with the ordinary Kriging interpolation method from four types of observations: groundwater boreholes, stages of kettle-hole lakes, elevation of wetlands located in landscape depressions, and land surface elevation at the model domain. Spatial distribution and details about the calculation of unsaturated layer thickness are presented in Paper III.

#### **4.2.2 Simulation framework**

Recharge was estimated by simulating water flow through an unsaturated 1-D soil column with the Richards equation using CoupModel (Jansson & Karlberg 2004). To distribute the simulations spatially, the recharge area was subdivided into different recharge zones, similarly to e.g. Jyrkämä *et al.* (2002). As each zone requires a unique simulation, the number of simulation set-ups rapidly increases, leading to high computational demand and/or laborious manual adjustment of model set-up. In the present work, this was avoided by simulating water flow in a single unsaturated 1-D soil column multiple times with different random parameterisations and distributing the results spatially to model zones. Spatial coupling was done with the ArcGIS software (ESRI 2011).

Zonation in the model was based on two variables: LAI and unsaturated zone thickness (UZD). Both variables were spatially distributed to a grid map with 20 m x 20 m cell size, resulting in a total of 205 708 cells for the model domain. The spatially distributed data were then divided into 15 classes for LAI and 30 classes for UZD (see Fig. 12 for LAI). Finally, the classified LAI and UZD data were combined to a raster

map with 20 m x 20 m cell size, producing 449 different zones with unique combinations of LAI and UZD values.

Simulations for the unsaturated 1-D soil profile were made for the period 1970–2010, and before each run 10 years of data (1960–1970) were used to spin up the model. The time variable boundary condition for water flow at the top of the column was defined by driving climate variables and affected by sub-routines accounting for snow processes. All water at the top of the domain was assumed to be subjected to infiltration. Deep percolation as gravitational drainage was allowed from the soil column base using the unit-gradient boundary condition (see e.g. Scanlon *et al.* 2002b). The column was vertically discretised into 60 layers with increasing layer thickness deeper in the profile: Layer thickness was 0.1 m until 1.6 m depth (the first layer lichen), 0.2 m between 1.6 and 3 m, 0.5 m between 3 and 10 m, 1 m between 10 and 17 m and 2 m from 17 m to the bottom of the profile (51 m).

The simulation was performed as 400 Monte Carlo runs to ensure enough model runs would be available for each LAI range. The model was run each time with different parameter values as specified in Table 1. The parameters for which values were randomly varied were chosen beforehand by trial and error model runs exploring the sensitivity of parameters with respect to cumulative recharge or evapotranspiration. The parameter ranges were specified from field data when possible; otherwise we resorted to literature estimates or in some cases used  $\pm 50\%$  of the CoupModel default providing a typical parameter for the equation. Paper III provides an illustrated example how the 1-D simulations were spatially distributed in the model domain.

**Table 1. Randomly varied parameters, related equations and parameter ranges included in the model runs. For a full description of parameters and equations, see Jansson and Karlberg (2004).**

Parameter	Part of the model affected	Range	Units	Source
LAI (leaf area index)	Transpiration	0...3.5	-	Data, see Section 4.2.1
h (canopy height)	Transpiration	5...15	m	Data
$r_{\text{lai}}$ (increase in aerodynamic resistance with LAI)	Soil evaporation	25...75	-	±50%, estimate
$r_{\psi}$ (soil surface resistance control)	Soil evaporation	100...300	-	±50% approximately to cover the surface resistance reported in (Kelliher <i>et al.</i> 1998)
$\lambda_L$ (pore size distribution index)	Soil evaporation, lichen	0.4...1	-	Estimate, to cover an easily drainable range of pressure-saturation curves
$\Psi_L$ (air entry)	Soil evaporation, lichen	1.5...20	-	Estimate, to cover a easily drainable range of pressure-saturation curves
$\theta_L$ (porosity)	Soil evaporation, lichen	7.5...12.5	%	Data, lichen mean water retention ±SD from samples
$k_{\text{mat,L}}$ (matrix saturated hydraulic conductivity)	Soil evaporation, lichen	$5 \cdot 10^4 \dots 5 \cdot 10^7$	mm d <sup>-1</sup>	Estimate, high K values assumed
$t_{\text{WD}}$ (coef. temperature response function)	Water uptake	10...20	-	±50%, estimate
$\Psi_c$ (critical pressure head for water uptake)	Water uptake	200...600	-	±50%, estimate
$k_{\text{mat,S}}$ (matrix saturated hydraulic conductivity)	Soil profile	$1.71 \cdot 10^3 \dots 127 \cdot 10^3$	mm d <sup>-1</sup>	Data from soil sample particle size analysis
$k_{\text{minuc}}$ (min. unsat. hydraulic conductivity)	Soil profile	$1 \cdot 10^{-4} \dots 1 \cdot 10^{-1}$	mm d <sup>-1</sup>	Estimate $k_{\text{mat}} \cdot 10^{-5}$
$\lambda_s$ (pore size distribution index)	Soil profile	0.4...1	-	Range to cover measured pressure-saturation curves
$\Psi_s$ (air entry)	Soil profile	20...40	-	Range to cover measured pressure-saturation curves
$\theta_s$ (porosity)	Soil profile	0.25...0.36	%	Range from soil samples
$\theta_r$ (residual water content)	Soil profile	0.01...0.05	%	Range to cover measured pressure-saturation curves



After completing the 400 CoupModel simulations for the unsaturated soil column, each unique recharge zone (a combination of UZD and LAI class) had on average 27 recharge time series produced by different random combinations of parameters. To propagate the variability in the 27 time series into the final areal recharge, a recharge value was randomly selected for each time step and each recharge zone from the ensemble of 27 (on average) and multiplied by the number of model cells belonging to the recharge zone in question (Eq. 2). This procedure was carried out for all time steps and then repeated a number of times (here 150 times) to ensure that all of the simulated time series for each recharge zone were represented in the random selection process.

$$R_{i,j} = \frac{\sum_{l=1}^{449} n(l) * R_{s_{i,rand(1:k)}} * A_c}{A_{tot}} \quad (2)$$

where  $R_{i,j}$  is the final sample of areal recharge [ $\text{mm d}^{-1}$ ],  $i$  is the index for simulation time step ( $= 1:14975$ ),  $j$  is the index for sample for a given time step ( $1:150$ ),  $l$  is the index for unique recharge zone,  $n(l)$  is the number of cells in a given recharge zone,  $R_s$  is the recharge sample [ $\text{mm d}^{-1}$ ] for a given recharge zone at time step  $l$ ,  $k$  is the number of time series for a given recharge zone,  $A_c$  is the surface area of a model raster cell ( $=20 \text{ m} * 20 \text{ m} = 400 \text{ m}^2$ ), and  $A_{tot}$  is the surface area of the total recharge area.

The resulting R matrix has 150 time series for areal recharge produced by simulations with different parameter realisations. The variability between the time series provides an indication of how much the simulated recharge varies due to different model parameter values. The method allows computationally efficient recharge simulations, because the different recharge zones do not all have to be simulated separately.

Four different evaporation processes were considered in this thesis; soil, snow, and lake evaporation and transpiration. In areas with unsaturated soil zones, the first three evaporation components were estimated, along with water flow simulations, using CoupModel. However, as 3.6% of the surface area of the study site consists of lakes (Fig. 3), lake evaporation from free water surfaces was calculated independently from the CoupModel simulations. Kettle-hole lakes in esker aquifers often lack surface water inlets and outlets and are therefore an integral part of the groundwater system (as shown in Section 5.1.1), so these lakes were considered as contributors to total groundwater recharge. In other words, rainfall per lake surface area was treated as an equal addition to aquifer water storage as groundwater recharge. As a difference, lake water table is subjected to evaporation unlike the groundwater table.

A detailed description of calculation of evaporation components is provided in Paper III.

The modelling method assumes that:

1. Over the long-term, the water table remains at a constant level, i.e. the unsaturated thickness for each model cells stays the same. Monitoring data shows water table variability of 1–2 m, with lowering and recovery of the water table. This variability is within the accuracy of water table estimation by interpolation, and therefore the assumption of long-term equilibrium was acceptable for the study site.
2. Surface runoff is negligible primarily due to the permeable soil type, and also due to lichen cover inhibiting runoff (Rodríguez-Caballero *et al.* 2012).
3. Only vertical flow takes place in the unsaturated soil matrix, a typical assumption in recharge estimation techniques (Dripps & Bradbury 2010, Jyrkama *et al.* 2002, Scanlon *et al.* 2002a).
4. The capillary fringe in the sandy soil is thin enough not to affect the water flow before arriving at the ‘imaginary’ water table at the centre of each soil class.
5. Uncertainties in the estimation of spatially distributed LAI and UZD values justify the use of approximations (i.e. water flow at the UZD class range midpoint and LAI value specified only as a range for each cell) in the cell classification phase.

Model performance was tested by comparing the simulated recharge values with two independent recharge estimates on local and regional scale; the water table fluctuation (WTF) method and base flow estimation, respectively. The WTF method is routinely used to estimate groundwater recharge because of its simplicity and ease of use, and assumes that any rise in water level in an unconfined aquifer is caused by recharge arriving at the water table (Healy & Cook 2002). The WTF method was applied to six water table wells (Appendix 1). For details about the method application, see Paper III.

The recharge estimated with the WTF method was compared with the simulated recharge during the recorded water level rise in the well. For each well, the cumulative sum of simulated water flow was extracted from soil profile depth corresponding to well water table depth. As an example, the simulated recharge in well G4 (unsaturated depth on average 14.7 m) was extracted from soil class 12, corresponding to recharge for unsaturated thickness of 14–16 m. All 400 model runs

were used, providing 400 estimates of recharge for each time period of recorded water level rise.

A regional estimate of groundwater recharge was estimated as baseflow of streams originating at the groundwater discharge area (Fig. 3). The lowest total outflow during 9–10 February 2010 was recorded after three months of snow cover, when water contribution to streams from surface runoff was minimal. The minimum outflow was considered as baseflow from the aquifer reflecting long-term groundwater recharge in the area.

### **4.3 Fully integrated surface-subsurface flow modelling (IV)**

In Paper IV, magnitude, temporal variability and spatial distribution of water fluxes at the GW-SW interface were estimated using a fully integrated hydrological modelling code HGS (Aquanty 2013). This integrated the conceptual and hydrogeological understanding of the Rokua esker aquifer acquired in Papers I, II and III using a state-of-the-art numerical simulator. The model results were compared with field techniques used to estimate (1) GW-lake exchange *locations* with air-borne measurement of water temperature and water sampling to estimate (2) exchange *magnitude* with the stable isotope technique. Paper IV tested the ability of the fully integrated numerical model to reproduce exchange between groundwater and surface water in a complex unconfined aquifer system.

#### **4.3.1 Model application to Rokua esker aquifer**

##### *Model mesh and driving data*

The model domain was discretised into 6-node triangular prismatic finite elements. In the subsurface, a total of 117 264 elements and 69 244 nodes comprised the simulation domain in six vertical finite element layers (see Fig. 2). In the vertical direction, the discretisation was refined near the ground surface to better represent the variable soil moisture conditions in the evaporative zone (thickness 1 m) and the water exchange processes between the subsurface and surface domains. In the lateral direction, the mesh was refined near streams, lakes and the boundary of the groundwater recharge area to focus calculation efforts on areas where subsurface-surface exchange fluxes were expected. Details about the mesh refinement are given in Paper IV.

Boundary conditions in the porous media consisted of a no-flow boundary in the bottom of the model due to low permeability bedrock, prescribed head boundaries defined by regional surface water bodies and a no-flow boundary in the rest of the model domain perimeter because of bedrock outcrops and thin soil layers. Detailed rationale on the assignment of boundary conditions is presented in Paper IV. A critical depth boundary condition was assigned around the perimeter of the model surface domain. The critical depth boundary condition does not constrain the flow rate or flow depth in the surface flow domain, but allows discharge to change naturally with respect to the calculated water depth at the stream outlet.

The model was sequentially coupled with Coup Model described in Paper III, which provided input data for the simulations as time series of infiltration (water arriving at the soil surface as a result of precipitation and/or snowmelt) and potential evapotranspiration (PET) for the period 1 Oct 2000–30 Sept 2013. The data were acquired from the groundwater recharge simulations (Section 4.2), with the addition of extending the simulation time to provide time series until September 2013. The simulations included calibrated routines for snow storage and snowmelt, which are necessary for the correct timing of water input in the system. In addition to climate data, the recharge simulations provided daily time series for groundwater recharge. In this part of the work the recharge data were used to calculate the average recharge over the simulation period (1 Oct 2000–30 Sept 2013) and the average recharge was used to calibrate the soil hydraulic properties in steady state.

The model was run first in steady state as part of model calibration to match the groundwater and lake levels and stream outflow in the system (see Section 4.3.2). The final system state after the steady state calibration was then used as initial conditions for a transient spin-up period. A recent study by Ajami *et al.* (2014) demonstrated that the equilibration time for integrated surface-subsurface models may require from a couple of years up to more than 20 years, especially to stabilise water storage in the subsurface. In this thesis, a 20 year spin-up period was used to ensure the system had reached a state where the water storages and fluxes were represented correctly at the beginning of the actual simulation period. The spin-up was performed with infiltration and PET data for the period 1 July 1980–30 Sept 2000 taken from the recharge simulations (Section 4.2). The spin-up was performed only once because of the computational burden and therefore the criterion of the spin-up performance (see e.g. Ajami *et al.* 2014) was not calculated.

### *Assigning spatially distributed model parameters*

The geology of the study site was characterised based on data described in Section 3.2 of this thesis. Because continuous stratigraphic layers could not be interpreted from the geological data, an assumption of homogeneous structure in the sand aquifer was made. A data-based range of  $1.99 \times 10^{-5} - 1.47 \times 10^{-3} \text{ m s}^{-1}$  was used in this thesis for model calibration (Section 3.2, Table 2). A van Genuchten function which best fitted the overall behaviour of the pressure-saturation data was used in the unsaturated layer modelling (Fig. 6, Table 2). Average porosity values were obtained from the soil sample analysis and the value used for specific storage was taken from Domenico (1972).

The peat soil was explicitly represented as a uniform layer with thickness 1.4 m blanketing the groundwater discharge area (Fig. 2), where the layer thickness was taken as the average depth of peat probings (Section 3.2). Data on the saturated hydraulic conductivity of the peat were taken from Rossi *et al.* (2014) and the pressure saturation relationship was estimated according to Päivänen (1973) for highly humified peat (Fig. 6, Table 2). Similar values for peat hydraulic parameters are presented in the literature (Holden & Burt 2002, Schwarzel *et al.* 2002, Silins & Rothwell 1998). Excess exfiltration through the peat matrix was observed in one of the sub-catchments in the area, where the aquifer is locally confined by the peat layer (Figs. 3 and 9). As is demonstrated in Section 5.1.1, the groundwater reaches the ground surface as preferential flow and seepage directly through the peat matrix. In this thesis the preferential flow was represented in a lumped manner as one order of magnitude higher hydraulic conductivity value compared with the rest of the peat soil.

Lake beds in Rokua are covered with organic gyttja (see Section 3.2). Peat hydraulic properties were used in the model for the gyttja layer, making it a low permeability layer compared with the mineral soil. Values of same order of magnitude have been used in past modelling studies for lake bed gyttja (Kidmose *et al.* 2013, Krabbenhoft *et al.* 1990a, Viridi *et al.* 2013). The gyttja layer was assigned in the lake bed elements vertically within 1.4 m depth from the lake bottom and horizontally completely within the lake shorelines.

Vegetation plays an important role in aquifer recharge at Rokua (see Section 5.2.3). The spatial variability of canopy LAI presented in Fig. 12 was too high to be explicitly accounted for in this modelling study. The LAI data were generalised to low, intermediate and high zones, with LAI values of 0.75, 1.25 and 1.75, respectively. The division was based on manual delineation to areas with high or low LAI occurrence. A canopy root depth of 1 m was selected based on the literature

(Kalliokoski 2011, Vincke & Thiry 2008). *Pinus sylvestris* roots are concentrated near the soil surface (Helmisaari *et al.* 2007, Kalliokoski 2011) and an exponential function that allocates the transpiration losses in the topmost soil layers was used to describe the root distribution within the 1 m depth chosen. Overland flow properties were assigned to two different domains: stream channels and forests. Manning's n values for the domains were taken from the literature (Jones *et al.* 2008).

**Table 2. Model parameterisation for spatially distributed parameters that deviated from HydroGeoSphere (HGS) model default values (Aqunty 2013).**

Model Domain	Parameter	Value			
Porous media		Sand	Peat		
	Saturated $K_z$ [ $m\ s^{-1}$ ]	$2 \cdot 10^{-5}$ [1,2]	$1 \cdot 10^{-7}$ [3]		
	Anisotropy $K_z : K_y$	1 : 2 [2]	1:1		
	Specific storage [ $1\ m^{-1}$ ]	$2 \cdot 10^{-4}$ [4]	$1 \cdot 10^{-1}$		
	Porosity	0.3425 [1]	0.86 [3]		
	Residual saturation	0.044 [1]	0.058 [3]		
	van Genuchten $\alpha$	2.35 [1]	26.15 [3]		
	van Genuchten $\beta$	2.38 [1]	1.39 [3]		
	Minimum relative permeability	$1 \cdot 10^{-9}$	$1 \cdot 10^{-11}$		
Overland flow		Sand	Peat	Channel	
	Manning's n	0.6 [5]	0.6 [5]	0.04 [5]	
	Rill storage height	0.1 [6]	0.1 [7]	0.001 [5]	
	Obstruction height	0.05	0.05	0.001 [5]	
Evapotranspiration		Peat	Sand 1 [2]	Sand 2 [2]	Sand 3 [2]
	LAI	1.14	0.75	1.25	1.75
	Canopy storage parameter	0	0	0	0
	Initial interception storage	0	0	0	0
	Transpiration fitting C1	0.06	0.4	0.4	0.3
	Transpiration fitting C2	0.15	-0.1	-0.1	0
	Wilting point	0.06	0.06	0.06	0.06
	Field capacity	0.15	0.25	0.25	0.25
	Oxic limit	0.99	0.6	0.6	0.6
	Anoxic limit	1.0	0.9	0.9	0.9
	Evaporation lim. sat min	0.1	0.04	0.04	0.04
	Evaporation lim. sat min	0.25	0.40	0.37	0.30
	Root zone depth	1	1	1	1
Evaporation depth	1	1	1	1	

Data sources: [1] field data, [2] calibration, [3] Päivänen (1973), [4] Domenico (1972), [5] Jones *et al* (2008), [6] Paper III, [7] Frei and Fleckenstein (2014)

### 4.3.2 Model calibration and validation

Simulated GW-lake interaction was compared with that determined using field methods for estimating the spatial distribution and total influx of groundwater discharge. The spatial occurrence of groundwater inflow was estimated with airborne thermal imaging, as described in Section 4.1.4. The total groundwater inflow to lakes was calculated with a stable isotope technique by Isokangas *et al.* (2014). In addition, model output was compared to measured groundwater ( $n = 13$ ) and lake hydraulic head ( $n = 7$ ) and stream flow ( $n = 20$ ) (Section 3.2 and Appendix 1).

Time series of the exchange flux between groundwater and lakes for the whole simulation period (2000–2013) was extracted for lake bed nodes which showed groundwater inflow on 1 Aug 2013 (timing of lake water sampling (Isokangas *et al.* 2014) and areal thermal imaging). To compare the modelled influx with isotope calculations, the groundwater inflow to lakes was averaged for the period 1 July 2013–30 Aug 2013 to fully cover the timing of water sampling. The complete time series of exchange flux between the subsurface and surface domains was also studied for the selected cells. A similar approach was used in Sudicky *et al.* (2008) to study GW-stream interaction for single model nodes (flux in  $\text{m s}^{-1}$ ), whereas here the inflow was extracted from a set of lakebed elements (flux in  $\text{m}^3 \text{s}^{-1}$ ). The aim was to examine the extent and pattern of variability in the groundwater inflow component and to find out whether the inflow dynamics vary in different lakes. To facilitate comparison between lakes, the inflow time series was standardised as:

$$G_{std} = \frac{G_{in} - \mu_G}{\sigma_G} \quad (3)$$

where  $G_{std}$  is the standardised inflow time series,  $G_{in}$  is the simulated groundwater inflow time series,  $\mu_G$  is the mean of  $G_{in}$ , and  $\sigma_G$  is the standard deviation of  $G_{in}$ .

#### Model calibration

Hydraulic conductivity and anisotropy were subjected to manual calibration in order to find a combination of vertical hydraulic conductivity and anisotropy ratio from pre-limited combinations (Table 3) where the steady state modelled groundwater head, lake level and stream baseflow values best fitted the averaged field observations. Even with no prior data available on aquifer anisotropy, the reported soil type variability in borehole logs and the geological sedimentation history gave reason to assume that the bulk saturated  $K$  in the horizontal direction exceeded that in the vertical direction. The reported anisotropy ratio at glacial outwash sites varies mainly

from 1:2 to 1:10 (Hunt *et al.* 2013, Krabbenhoft *et al.* 1990a, Smerdon *et al.* 2007, Sudicky *et al.* 2010) and these values were selected for calibration. Recharge was applied only in the aquifer recharge area because of the complex recharge discharge pattern expected in the discharge area covered with peat. The water seeping to the streams from the aquifer was thus considered to represent the simulated steady-state stream baseflow, and peat layer contribution to baseflow was assumed to be minor.

**Table 3. Saturated hydraulic conductivity and anisotropy ratio ( $K_z$ :  $K_x$  and  $K_y$ ) values used in model calibration.**

	1	2	3	4	5	6	7	8	9
K [ $m s^{-1}$ ]	$2 \cdot 10^{-4}$	$2 \cdot 10^{-4}$	$2 \cdot 10^{-4}$	$6.5 \cdot 10^{-5}$	$6.5 \cdot 10^{-5}$	$6.5 \cdot 10^{-5}$	$2 \cdot 10^{-5}$	$2 \cdot 10^{-5}$	$2 \cdot 10^{-5}$
aniso. ratio	1:2	1:5	1:10	1:2	1:5	1:10	1:2	1:5	1:10

The steady state recharge values in the model calibration phase were based on the recharge estimation method presented in Section 4.2. Spatially distributed constant recharge values (Table 4) were applied to zones with different LAI. Because the recharge calculations did not provide recharge for unique LAI zones delineated in this thesis, the recharge in different zones was related to the ET in the recharge simulations (Table 4). After calibration, the model was run in transient mode with daily data for water input and PET. To maintain the consistency between steady state and transient simulations, the empirical ET parameters for each LAI zone in HGS (Table 3) were calibrated to match the total ET amount and to approximately reproduce the daily ET dynamics. With this procedure, the magnitude of both recharge (steady state calibration) and ET (transient runs) in this thesis was related to that in prior simulations for groundwater recharge. The best match between the two simulations for total evapotranspiration (Table 4) was found with ET parameters for a given LAI value presented in Table 2.

**Table 4. Mean areal evapotranspiration (ET) and recharge for zones with different leaf area index (LAI) values. For areas with LAI 0.75 and 1.75, recharge was calculated by multiplying the recharge for areas with LAI = 1.25 by 402.0 [ $mm a^{-1}$ ] with ET ratios 199.9/234.0 and 255.4/234.0, respectively.**

	LAI = 0.75	LAI = 1.25	LAI = 1.75
Paper III Recharge [ $mm a^{-1}$ ]	470.6	402.0	368.3
Paper III ET [ $mm a^{-1}$ ]	199.9	234.0	255.4
Paper IV ET [ $mm a^{-1}$ ]	202.7	227.7	252.7



## **5 Results and discussion**

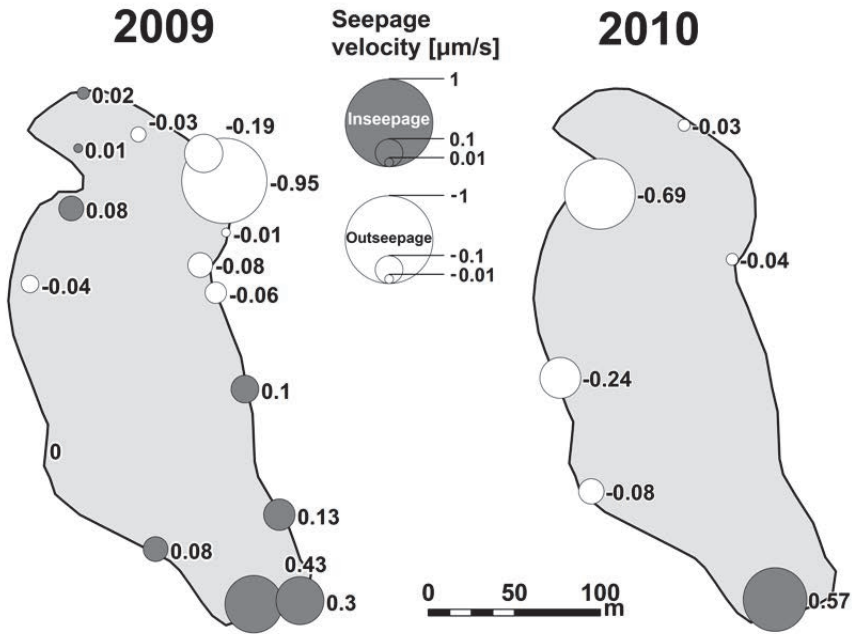
### **5.1 Field measurements to verify GW-SW interactions**

Field measurement techniques in both the groundwater recharge and discharge area show clear interactions with groundwater and the lakes and streams in the area. Environmental tracers proved additional verification of the exchange process at both water body and aquifer scale.

#### ***5.1.1 Interaction based on flux and hydraulic gradient (I & II)***

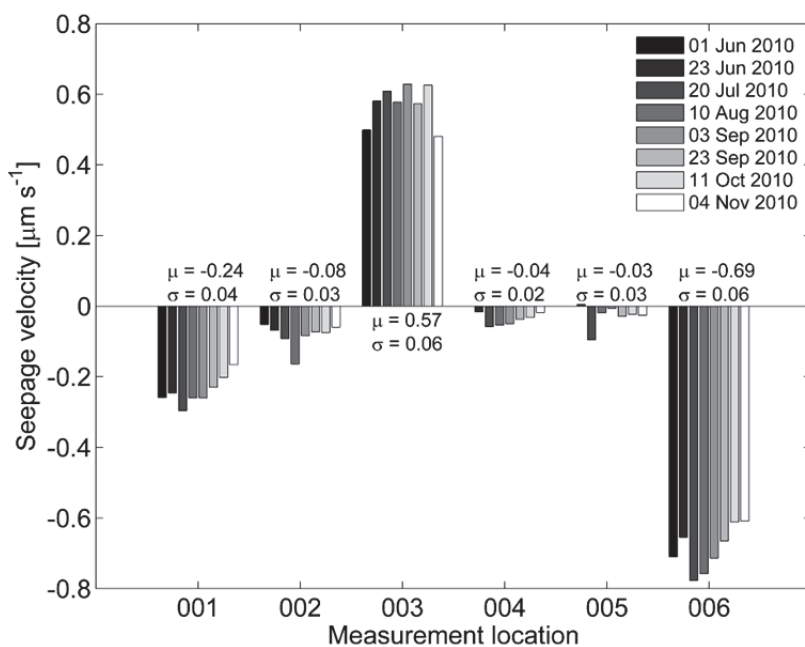
##### ***Spatially and temporally variable GW-lake interaction in the groundwater recharge area (I)***

GW-lake interaction was determined with seepage meters in a pilot lake (Lake Ahveroinen, L3). Strong spatial variations in seepage rates were observed in 2009 and the spatial distribution of seepage differed between 2009 and 2010, especially in the north-west part of the lake (Fig. 13). Similar strong spatial variability has been reported in numerous studies measuring lake seepage (Cable *et al.* 1997, Cherkauer & Nader 1989, Kidmose *et al.* 2013, Rosenberry 2005). The areas of highest inflow were in the south and south-east parts of the lake, and the highest outflow was observed in the northern part of the lake. In 2009, considerable outflow was only noted in the north-east corner of the lake.



**Fig. 13. Spatial variations in seepage ( $\mu\text{m s}^{-1}$ ) in two consecutive years. Seepage rates are presented as circles, with relative size and colour showing the rate and direction of seepage, respectively. For the year 2010, the average value from the eight measurements performed is shown. Reprinted with permission from Elsevier (Paper I).**

In 2010, temporal changes in seepage rates were observed at every observation point, but the temporal variation in seepage rates was low (Fig. 14). This variation, despite being small, cannot be attributed to measurement error or random natural variability because of the high observed covariation between seepage rates at four out of six measurement points. This demonstrates the capability and accuracy of the seepage meter measurement method to distinguish small changes in the groundwater flow environment as long as the meter chambers are not removed between measurements.



**Fig. 14. Temporal variations in seepage ( $\mu\text{m s}^{-1}$ ) during 2010 for each seepage measurement location in Lake Ahveroinen (L3). Positive values correspond to in-seepage,  $\mu$  denotes the mean and  $\sigma$  the standard deviation of the measurements. Reprinted with permission from Elsevier (Paper I).**

Variations in the seepage rates for the measurement locations were correlated with different parts of the hydrogeological system (Table 5). Locations 001 and 006, where the highest outseepage rates were measured, correlated with piezometers G20 and G6 in the direction of outseepage. Location 004, with low seepage rate, was correlated with lake stage and piezometer G21 where the water table closely followed lake level.

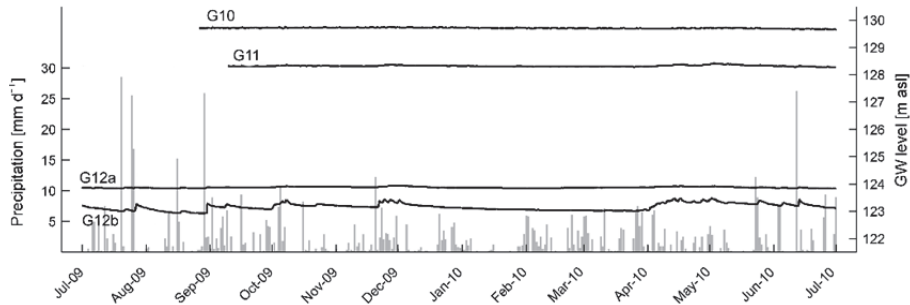
**Table 5. Pearson correlation coefficients for the relationship between seepage measurements at sampling locations 001–006 and lake and groundwater levels in adjacent piezometers.**

Measurement location	001	002	003	004	005	006
Lake stage	0.42	0.27	-0.68	0.76*	0.55	0.44
G21	0.20	0.46	-0.62	0.84*	0.43	0.31
G20	0.86*	0.25	-0.11	0.59	0.18	0.76*
G6	0.79*	0.15	-0.08	0.55	0.05	0.65

\*p<0.05

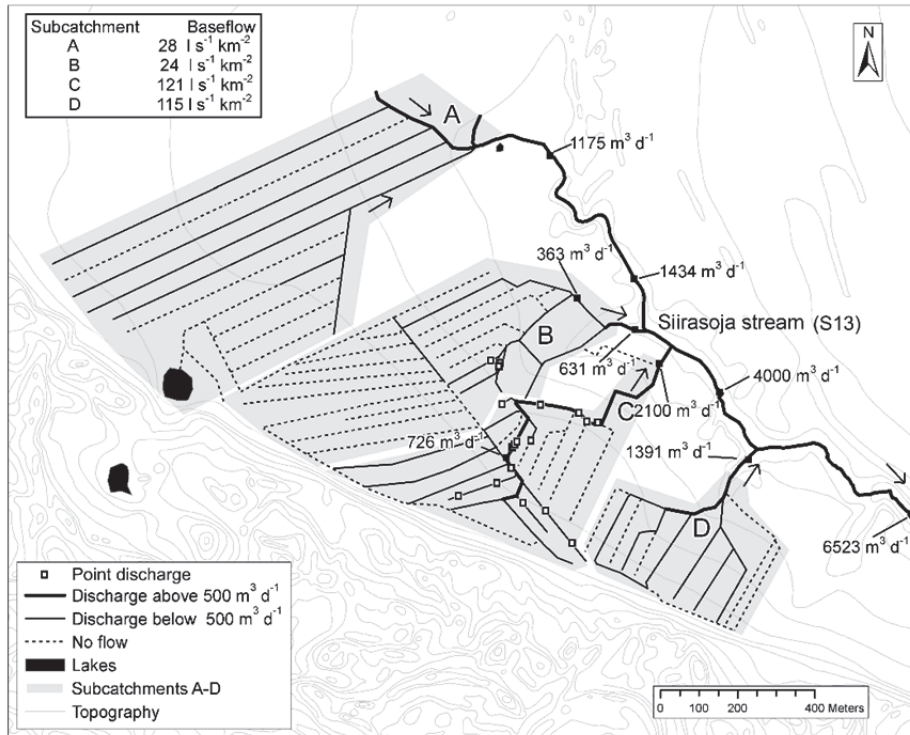
***Groundwater exfiltration to drained peatlands in groundwater discharge area (II)***

GW-SW interaction was studied in the groundwater discharge area, where a peat soil layer with low hydraulic conductivity (G12b) confined the underlying sand aquifer (G12a) at the location of piezometer installation (Fig. 15). The level of ditch bed next to the piezometers was still approximately 2 m below the level of measured peat soil hydraulic head. Therefore the drainage ditch created artesian conditions in the sand aquifer, and water exfiltrated through a point discharge channel observed in the ditch bed next to the piezometers. Hydraulic conditions promoted water flow to the drainage network from both groundwater discharge from the underlying sand aquifer and gravitational drainage from the confining peat layer. In addition to changing the hydraulic conditions, the drainage network also reduced surface flow resistance in the area by conveying the exfiltrated groundwater rapidly downstream via the drainage network.



**Fig. 15. Time series for the hydraulic head in the sand aquifer (G10, G11, and G12a) and in the peat soil (G12b). Reprinted with permission from Elsevier (Paper II).**

Groundwater exfiltrated to the drained peatland by two mechanisms: point discharge as preferential flow through the peat matrix and as diffuse seepage through the ditch bed. All and all, groundwater exfiltrated into the drained peatland in a spatially complex pattern, with high variability in discharge rates and mechanisms between subcatchments. Outflow occurred via point discharges, which were spring-like features in a ditch bed or bank. Such point discharges were present in catchment C, exhibiting high baseflow and thick peat layers (Fig. 16). It is not known whether the point discharges appeared as a result of peatland drainage, or whether the preferential flow channels in the peat matrix existed as natural springs prior to drainage. Because of the low hydraulic conductivity in the peat matrix itself, dual porosity controls the water discharge in the peatland area in subcatchment C. Exfiltration is very localised and is concentrated to certain ditches, whereas some of the ditches remain virtually dry (Fig. 16).



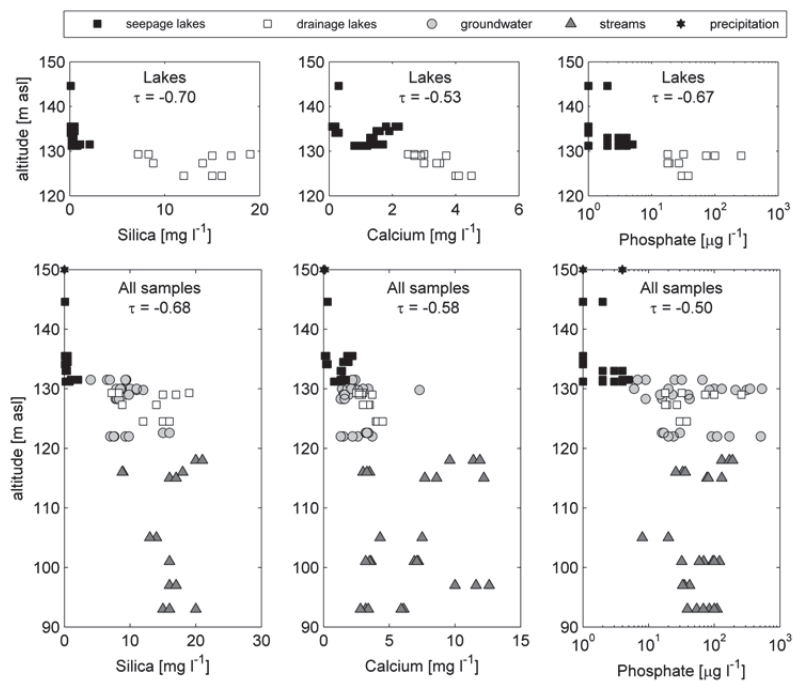
**Fig. 16. Spatial variability in groundwater discharge into drained peatlands, seen as highly variable stream baseflow in adjacent subcatchments. Subcatchments A and B show small baseflow amounts compared with subcatchment C (groundwater input as point discharge) and subcatchment D (diffuse groundwater in seepage). Reprinted with permission from Elsevier (Paper II).**

Diffuse seepage occurred in subcatchment D, where a high baseflow value was present but no groundwater point discharges through preferential flow channels were observed (Fig. 16). Instead, some of the drainage ditches had been cut through the thin (0.5–2 m) peat layer, providing a direct flow route from the sand aquifer into the drainage ditches. The drainage network increased the hydraulic gradient between the drain and the aquifer, because the elevation of the drain bed was notably lower than the hydraulic head in the peat matrix.

### 5.1.2 Environmental tracers at aquifer and water body scale (I & II)

#### Environmental tracers showing groundwater input to surface water bodies in aquifer scale

Analysis of environmental tracers suggested a link between the landscape position of a sampling location and water quality at the location on aquifer scale. On moving sampling location progressively to lower sites in the landscape, the water was generally richer in silica, calcium and phosphate (Fig. 17 and Table 6). A significant Kendall correlation was observed between concentration and altitude ( $p < 0.001$ ) for all three tracers.



**Fig. 17. Concentrations of environmental tracers (silica, calcium, phosphate) as a function of landscape altitude (m above sea level, asl) at the sampling locations for all three sampling years. The upper diagrams show only the lake concentrations (n = 39) and the lower diagrams include all sampling locations (n = 95). Reprinted with permission from Elsevier (Paper I).**

The water bodies were subdivided into four categories to emphasise the differences in seepage lakes, drainage lakes, groundwater and streams. Seepage lakes stood out as a separate group, with high landscape position and low concentrations of each compound (Fig. 17, Table 6). The difference between the other groups and seepage lakes was especially distinct in terms of silica concentrations, for which there was no overlap between the groups. In terms of calcium and phosphate, the concentrations moved gradually from precipitation quality towards groundwater quality with decreasing altitude.

Concentrations of silica and calcium in the groundwater were slightly lower than in drainage lakes (Table 6 and Fig. 13) or in similar sand and gravel aquifers in Finland (median for Ca = 3.2 mg L<sup>-1</sup> and SiO<sub>2</sub> = 12.0 mg L<sup>-1</sup>; Soveri *et al.* 2001). Because the groundwater was sampled from groundwater table wells with variable unsaturated zone thickness and presumably different residence times in the saturated zone, some variability in the tracer concentration is inherent due to the sampling strategy. Phosphate concentrations, in particular, varied both spatially and interannually (see e.g. Table 7) and were distinctly higher than in Finnish aquifers in general (median = 6 µg L<sup>-1</sup>, 90<sup>th</sup> percentile 28 µg L<sup>-1</sup>; Soveri *et al.* 2001). The interannual variability suggests that leaching from the uppermost soil layers is highly variable between hydrological years, especially for the samples with a shallow unsaturated zone.

**Table 6. Mean and standard deviation (std) of sampling location altitudes and median and interquartile range (IQR) of tracer samples (silica (SiO<sub>2</sub>), calcium (Ca) and phosphate (PO<sub>4</sub><sup>3-</sup>)) divided into different hydrological compartments for all three sampling years.**

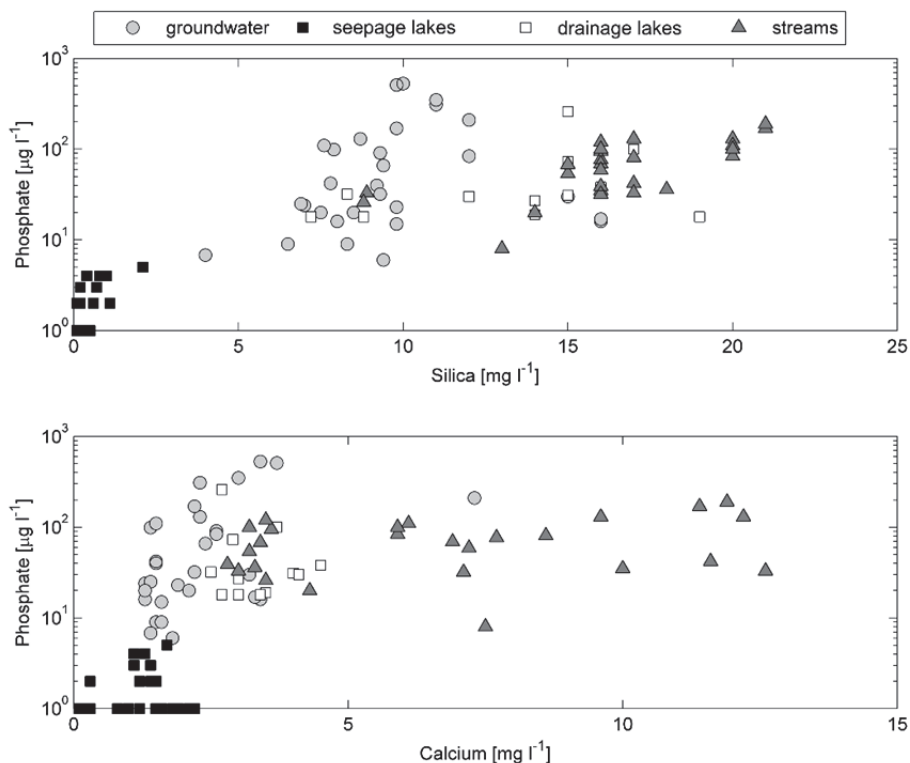
Water body type	Altitude [m asl]		SiO <sub>2</sub> [mg L <sup>-1</sup> ]		Ca [mg L <sup>-1</sup> ]		PO <sub>4</sub> <sup>3-</sup> [µg L <sup>-1</sup> ]	
	mean	std	median	IQR	median	IQR	median	IQR
Seepage lakes (n = 27)	134.7	3.9	0.3	0.4	1.2	1.2	1	1
Drainage lakes (n = 12)	127.5	1.9	14.5	4.1	3.2	0.9	30.5	28.0
Groundwater (n = 30)	127.7	3.7	9.3	2.1	2.1	1.1	32.0	93.0
Streams (n = 27)	104.3	9.2	16.0	1.8	6.5	5.9	68.5	64.8



Streams were a distinctly separate group because of both their low landscape position and high tracer average concentration and variability (Table 6). All the sampled streams originated in the groundwater discharge area (Fig. 3) covered by peat soils. During late winter, when the sampling was performed, streams receive very little water from precipitation or surface runoff and most of their discharge can be assumed to consist of base flow provided by the aquifer. Therefore it is reasonable to expect that groundwater entering the streams as base flow has travelled along longer subsurface flow paths than the water sampled from lakes and piezometers in the recharge area. As a result, groundwater seepage to the streams is likely to be richer in weathering compounds, which is in turn seen as elevated tracer concentrations in the stream samples.

Phosphate concentration at a given sampling location showed a statistically significant ( $p < 0.001$ ) monotonic Kendall's correlation with both silica and calcium concentrations (Fig. 18). The phosphate increased in a log-linear fashion with increasing silica concentration, whereas the trend in correlation between phosphate and calcium was less obvious but still monotonically increasing. Even though phosphate concentration did not correlate strongly with landscape position in the aquifer (Fig. 17), it nevertheless increased together with silica and calcium.

The finding is interesting, because even small differences in phosphate inputs can change the ecological structure of sensitive surface water bodies. The subsurface is traditionally considered a dilution system for phosphate, as in the study by Devito *et al.* (2000) which suggests that total phosphorus loading caused by forestry logging and ending up in lakes is lower for lakes which receive groundwater via long subsurface flow paths. Sorption processes responsible for dilution along long flow paths can be expected if phosphorus concentration in the infiltrating water is elevated significantly above the natural background concentration for some reason. However, the results obtained in this thesis provide support for the claim made by Holman *et al.* (2010) that the subsurface can act as a source of phosphate in certain geological settings, as also shown by Kidmose *et al.* (2013). This is best seen in the correlation of phosphate with tracers indicating long residence time in the subsurface (Fig. 18).



**Fig. 18. Crossplots of phosphate concentrations with silica ( $\tau = 0.60$ ,  $p < 0.001$ ) and calcium ( $\tau = 0.50$ ,  $p < 0.001$ ). Reprinted with permission from Elsevier (Paper I).**

### *Environmental tracers at lake (L3) and peatland catchment (S13) sites*

Data on environmental tracer concentrations in the vicinity of L3 showed generally higher concentrations of tracers at all groundwater sampling locations compared with the lake (Table 7). Silica appeared to provide the strongest and most consistent signal separating lake water from groundwater. It should be noted that cation concentrations in inland piezometers may overestimate the concentrations in water actually discharging to the lake (Brock *et al.* 1982, Krabbenhoft & Webster 1995).

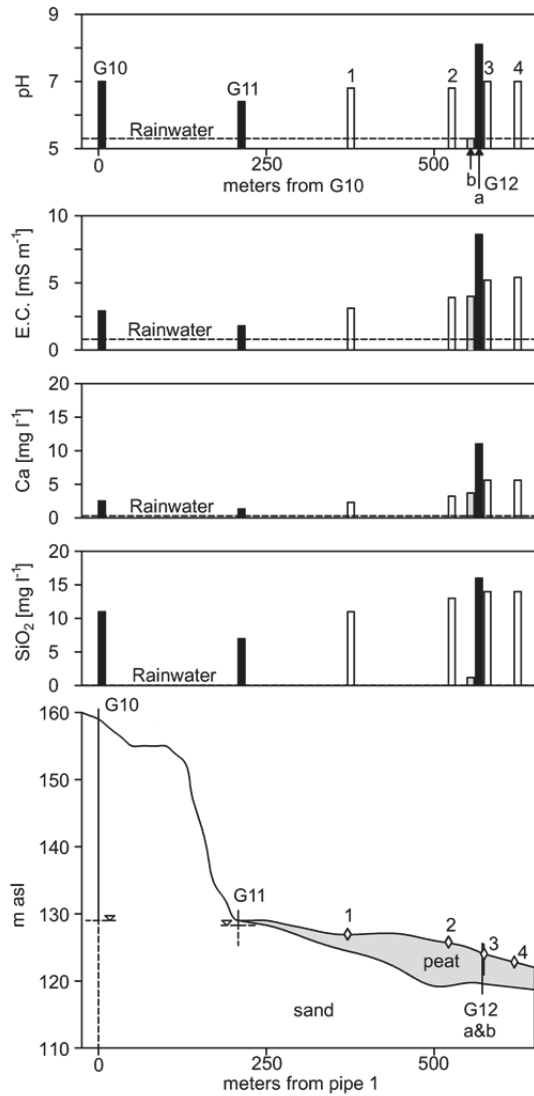
Because the tracer concentrations in the lake do not resemble the concentrations in the surrounding aquifer, the solute-rich groundwater input to lake water balance seems to be of minor importance in comparison with solute-poor inputs from precipitation. This conclusion is to some extent supported by the seepage meter

measurements, where the only consistent location of groundwater inflow was observed in the south-east part of the lake. However, the tracer concentrations in L3 (Table 7) were slightly higher than in other seepage lakes in the area (Table 6), which suggests there is more groundwater influence in L3 than in the average seepage lake.

**Table 7. Concentrations of environmental tracers (silica (SiO<sub>2</sub>), calcium (Ca) and phosphate (PO<sub>4</sub><sup>3-</sup>)) in Lake Ahveroinen (L3) and adjacent piezometers, 2010–2012.**

Sampling location	SiO <sub>2</sub> [mg L <sup>-1</sup> ]			Ca [mg L <sup>-1</sup> ]			PO <sub>4</sub> <sup>3-</sup> [µg L <sup>-1</sup> ]		
	2010	2011	2012	2010	2011	2012	2010	2011	2012
L3	2.1	1.1	1.0	1.7	1.5	1.3	5	2	4
G6	9.4	10	11	1.8	3.4	3	6	550	350
G21	6.5	6.9	4	1.5	1.4	1.4	9	25	7
G20	7.9	8.7	8.5	1.4	2.3	2.1	99	130	20
G17		9.4	9.3		2.4	2.2		66	32

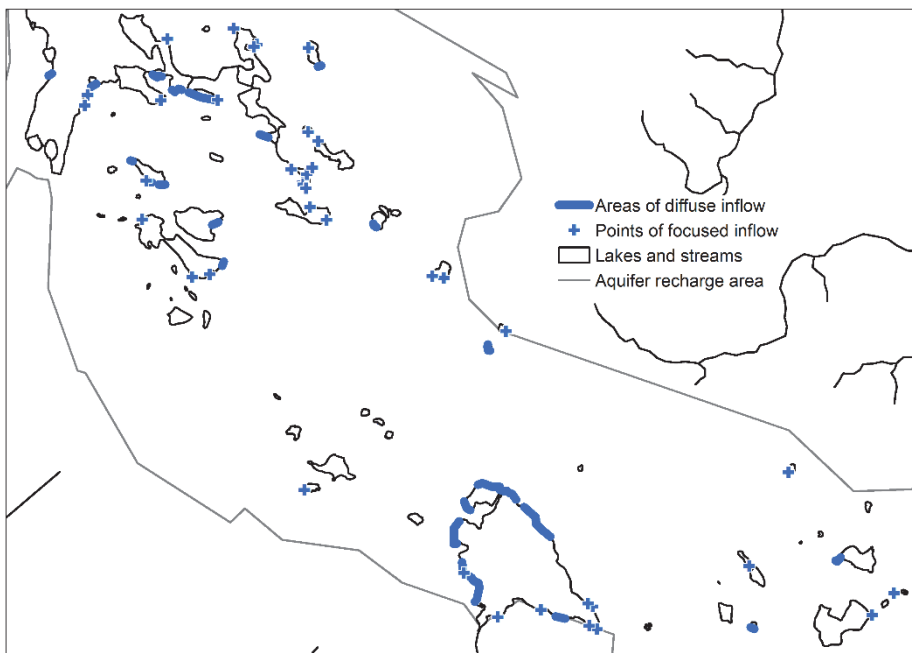
Environmental tracers showed a clear groundwater signal in surface water drainage ditches in the groundwater discharge area (Fig. 19). The silica concentrations in particular suggested that majority of the water in the drainage network originates from the underlying sand aquifer with distinctly higher silica concentrations (7–16 mg L<sup>-1</sup>) than in peat groundwater (1.2 mg L<sup>-1</sup>) or rainfall (<0.1 mg L<sup>-1</sup>). The tracer results also showed the evolution of groundwater composition along the groundwater flow path (Kenoyer & Bowser 1992). For all tracers used, the highest subsurface concentrations were found in the confined sand aquifer most down-gradient in the catchment (G12a). The lowest tracer concentrations in the sand aquifer were in G11, which most likely has rapid input from rainwater because of the thin unsaturated layer (Fig. 19).



**Fig. 19.** pH and environmental tracers ( $\text{SiO}_2$ ,  $\text{Ca}^{2+}$  and EC) sampled from boreholes, streams and precipitation in June 2010, plotted as the function of horizontal distance from the first sample. Black columns are samples from the sand aquifer, white columns represent the stream concentration at different locations and the grey column is the groundwater in peat soil. Reprinted with permission from Elsevier (Paper II).

### 5.1.3 Airborne thermal infrared imaging (IV)

The areal thermal imaging provided a spatially extensive snapshot of the GW-lake exchange processes at the study site. Groundwater discharge to lakes in the Rokua area was evident in the TIR data, since locations where water surface temperature was notably cooler (10–15 °C) than the background temperature (~20 °C) were abundant (Fig. 20). The data showed both diffuse groundwater inflow along long sections of the shoreline and focused inflow coming from a more constrained area. Groundwater inflow was observed in lakes throughout the aquifer recharge area and drainage lakes with a stream outlet stood out, with a high number of groundwater inflow observations.



**Fig. 20. Spatial distribution of diffuse and concentrated groundwater discharge locations in lakes in the Rokua aquifer recharge area.**

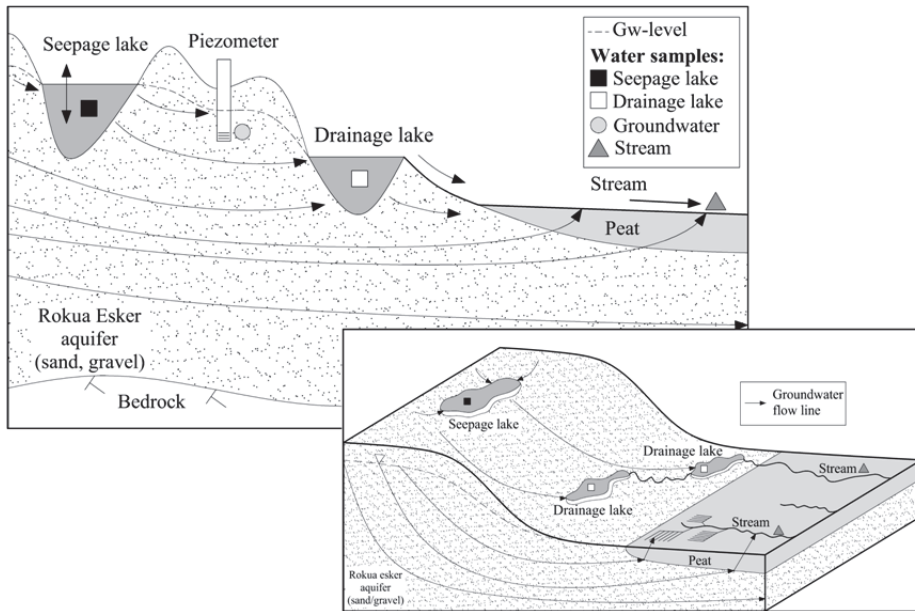
#### **5.1.4 Conceptual model for GW-SW interactions**

Based on the results from field studies, the conceptual model of the aquifer hydrology (Fig. 21) was verified for some parts (occurrence of GW-SW interaction) and refined for other parts (spatial variability of GW-SW exchange and understanding of groundwater flow systems). The field-based methods showed that:

- Groundwater-surface water interaction is unambiguously present between the esker aquifer and related surface water bodies (Figs. 13 and 16)
- The interaction is highly variable in space in both lakes (Figs. 11 and 20) and drainage channels (Fig. 16).

Use of environmental tracers:

- Further verified the small-scale GW-SW exchange processes (Table 7 and Fig. 19)
- Facilitated generalisation of the small-scale exchange processes identified to aquifer scale (Fig. 17)
- Showed that silica is a good tracer for groundwater influence in surface water bodies for the given geology.



**Fig. 21. Conceptual model of the Rokua esker aquifer explaining water level fluctuations in some lakes and the eutrophic state of others. The hypothesis was that seepage lakes receive most of their water from precipitation or local groundwater flow systems, so their levels are more sensitive to climate variations. Drainage lakes are more eutrophic and have more stable levels, because they receive constant, nutrient-rich groundwater inflow. Reprinted with permission from Elsevier (Paper I).**

According to the results from the environmental tracer analysis, water in the seepage lakes with periodically declining water table is poor in solutes and closer to precipitation in composition rather than to the high solute concentrations of drainage lakes. Nevertheless, TIR imaging, measured in seepage for one such lake, and solute concentrations higher than in precipitation provided evidence that closed basin lakes are not hydraulically isolated, but rather interact with the groundwater system. Low solute concentrations in the seepage lakes in comparison with drainage lakes could be explained by:

1. Lower concentrations of solutes in the groundwater in seepage because of shorter subsurface flow paths.
2. A smaller contribution of groundwater to the closed basin lake water balance.
3. Both of the above, acting simultaneously.

Environmental tracers were present in similar concentrations in eutrophic drainage lakes and in groundwater, implying nutrient and cation input to certain lakes from groundwater discharge. Surface or near surface runoff is often considered an important transport route for nutrients to surface water bodies, but at the study site highly permeable soils and a lichen layer covering the soils make the surface runoff in the area negligible. Among possible anthropogenic sources, agriculture in the aquifer recharge area is non-existent. Forestry activities, which have been shown to be a potential source of e.g. phosphate to groundwater (Devito *et al.* 2000), are practised in the area. However, fertilisation in the forestry has been minimal and the nutrient leaching from the forestry is estimated to be at the level of natural background loading (Väisänen *et al.* 2007). Because land use practices and habitation in the catchment areas of seepage and drainage lakes are similar and nutrient inputs to the system from precipitation almost non-existent, subsurface origin by leaching, dissolution, weathering or desorption remains the most credible source providing nutrients and cations to the lakes.

A considerable body of research reports similar inputs of dissolution and weathering products to lakes via long, regional groundwater flow paths (Brock *et al.* 1982, Kenoyer & Anderson 1989, Kenoyer & Bowser 1992, Webster *et al.* 1996). In the Rokua aquifer area, stream outlets are a vital component in enabling and sustaining steady, nutrient-rich groundwater inflow to the drainage lakes. This holds true especially for the first lakes in the chain of lakes, which have no inlets but discharge water constantly via outlets. These outlets convey the nutrient-rich water seeping from groundwater through the chain of lakes, affecting the water quality of the whole lake chain. Stets *et al.* (2010) have reported similar settings where a regional groundwater flow system provides inflow to headwater lakes connected with streams.

## **5.2 Spatially and temporally distributed groundwater recharge (III)**

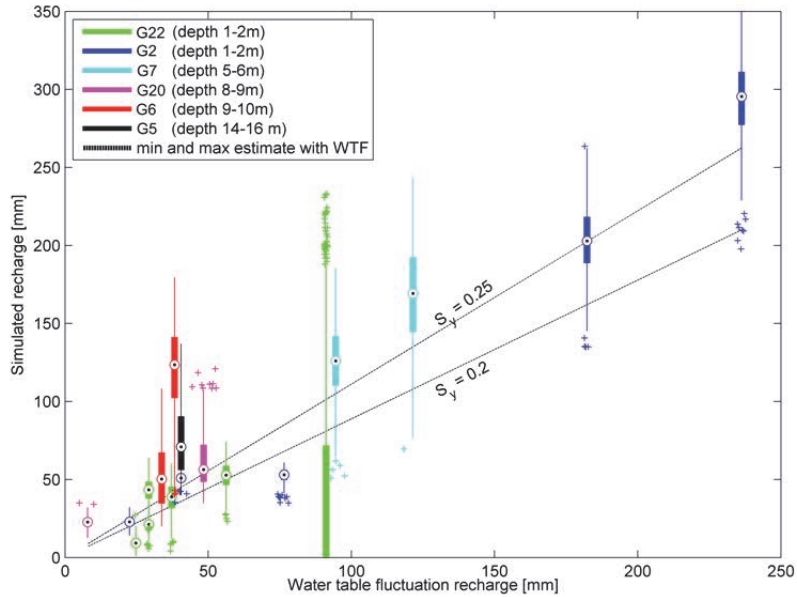
Spatial and temporal variations in groundwater recharge were estimated with a modelling approach developed to utilise forestry inventory data. The Richards equation-based 1-D simulations were spatially distributed using Monte Carlo runs for an unsaturated soil column. Within the Monte Carlo process, residence time in the unsaturated zone and relevant physical characteristics of the system were accounted for, while uncertainty in selected model parameters was propagated to the final recharge time series. The simulations provided a sound estimate for historical time series of groundwater recharge in the Rokua esker aquifer.



### **5.2.1 Model validation**

The model showed reasonable performance and consistency when compared against independent recharge estimates obtained with both WTF and baseflow methods (Fig. 22 and Table 8, respectively). The WTF method agreed well with the simulated values, with overlapping estimates between the methods for all but two boreholes. Moreover, the median value of simulations was close to that obtained with the WTF method, but with some bias towards higher estimates from the simulations.

The discrepancy can be due to different assumptions behind the methods and uncertainty in local parameterisation, in the WTF method for the specific yield and in the simulations mainly for the hydraulic conductivity, which dictates the timing of recharge. However, there were overlapping estimates for almost every recharge event, which shows consistency between the methods. The stream baseflow was lower than the long-term average recharge, which was expected because of the site hydrogeology. All of the outflow from the aquifer was probably not captured by the baseflow measurements, as some of the water discharges to larger streams and lakes outside the stream catchments (as shown in Section 5.3). When simulated recharge was extracted specifically for the baseflow measurement dates, the lower values for simulated recharge were also anticipated because of seasonal variability in recharge but a stabilising effect of the groundwater storage for stream baseflow. In conclusion, the order of magnitude of the regional baseflow estimates and the simulation results was similar. Despite the very different assumptions on which the modelling and field methods were based, all provided similar estimates of groundwater recharge at the study site.



**Fig. 22. Assemblage of simulated recharge for individual recharge events, shown as boxplots where circles represent the median, bold lines 25–75<sup>th</sup> percentiles of the simulations, thin lines the remaining upper and lower 25<sup>th</sup> percentiles and crosses are outliers. The location of the boxplots on the x-axis is the water table fluctuation (WTF) estimate for a given recharge event using a specific yield value of 0.225. The dashed lines indicate the uncertainty in the WTF estimates caused by the selection of specific yield. The two estimates would agree perfectly (given the uncertainty in  $S_y$ ) if all simulations shown as boxplots fell between the dashed lines. CC BY 3.0 (Paper III).**

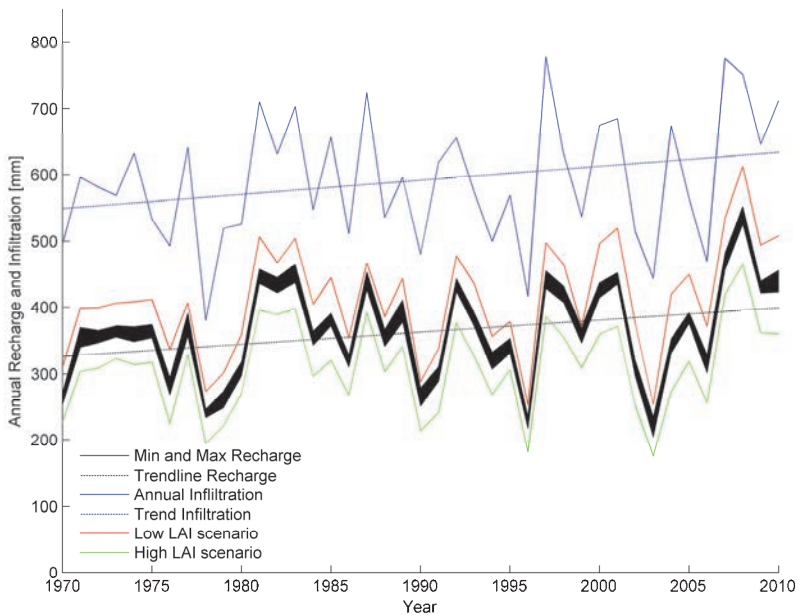
**Table 8. Stream baseflow estimates compared with simulated recharge outputs calculated for different periods**

Baseflow for 9–10 February 2010 [ $\text{mm a}^{-1}$ ]	Long-term average recharge [ $\text{mm a}^{-1}$ ]	Recharge for preceding year 2009 [ $\text{mm a}^{-1}$ ]	Simulated recharge for 9–10 February 2010
312.7	362.8	421.8 (min)	110.0 (min)
		439.5 (max)	135.8 (max)

### **5.2.2 Spatially and temporally distributed recharge time series**

Annual recharge (Fig. 23) was strongly correlated with annual sum of precipitation (linear correlation coefficient 0.89), as expected based on previous work in a humid climate and sandy soils (Keese *et al.* 2005, Lemmelä 1990,

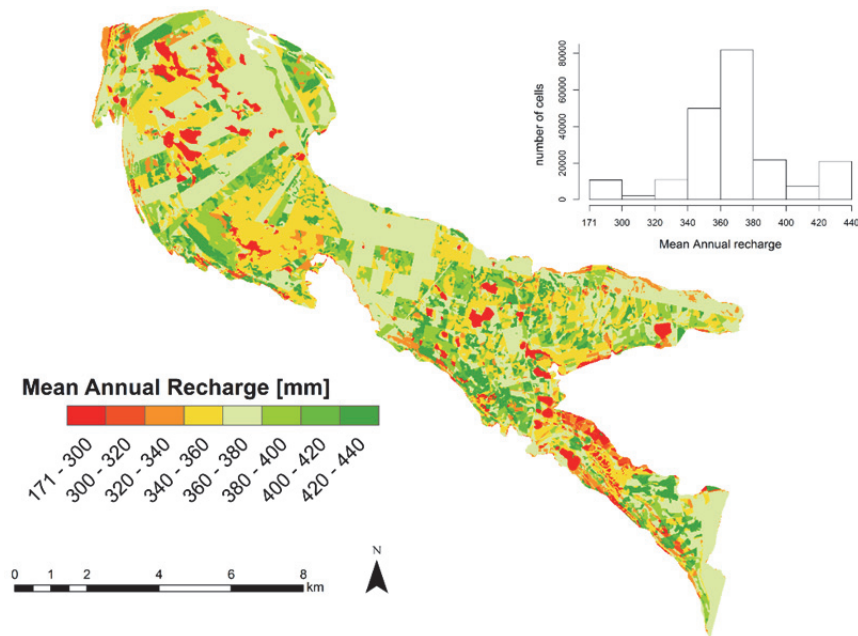
Okkonen & Kløve 2011). According to the simulations, the average groundwater recharge was  $362.8 \text{ mm year}^{-1}$ , and the effective rainfall, i.e. the percentage of rainfall resulting in groundwater recharge annually, was on average 59.3%. This is in agreement with previous studies on unconfined esker aquifers at northerly latitudes, in which the proportion of annual precipitation percolating to recharge is reported to be 50–70% (71% by Zaitsoff (1984), 54% by Lemmelä and Tattari (1986) and 56% by Lemmelä (1990)).



**Fig. 23. Annual recharge time series from simulations, where the black area covers the minimum and maximum values for different recharge samples. The annual recharge pattern closely followed trends in infiltration. Effects of different land use management practices over time on annual recharge rates are shown as high and low leaf area index (LAI) scenarios. CC BY 3.0 (Paper III).**

The method used here to estimate LAI from forestry inventories introduces a new approach for incorporating large spatial coverage of detailed conifer canopy data into groundwater recharge estimations. The spatial distribution of groundwater recharge was indeed mostly due to variations in LAI originating from forestry data, distance to water table and distribution of lakes (Fig. 24). Higher evaporation rates from lakes led

to lower recharge in lakes (see red spots in Fig. 24). Similarly, high LAI led to high ET and resulted in low recharge. Other areas of low recharge, although not as obvious at the larger spatial scales shown in Fig. 24, were cells with a shallow water table. The effect of high ET at locations with a shallow water table can best be seen in south-east parts of the aquifer.



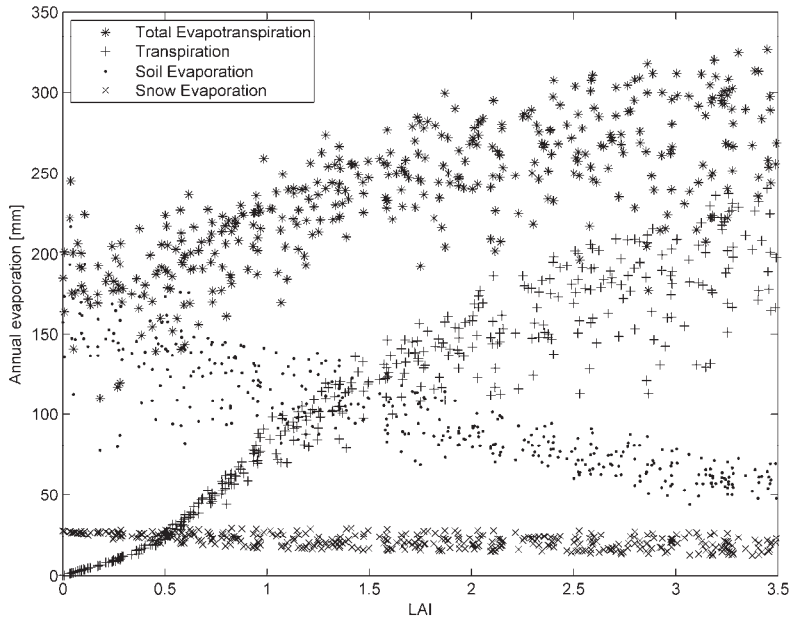
**Fig. 24. Spatial distribution of mean annual recharge, which was influenced mainly by the Scots pine canopy (leaf area index, LAI), the presence of lakes and, to some extent, areas with a shallow water table. CC BY 3.0 (Paper III)**

Estimated evaporation from the land surface (mean 237.6 mm) was somewhat lower than previous regional estimates of total ET (300 mm; Mustonen 1986). Kelliher *et al.* (1998) found that ET from boreal conifer forests is around 2 mm d<sup>-1</sup> during the growing season, which is again slightly higher than our average value of 1.6 mm d<sup>-1</sup> for the period 1 May–31 Oct. The differences may have been caused by the permeable sandy soil type at the study site. Conifer forests in the boreal zone are usually dominated by less permeable glacial till soils, allowing

more time for evaporation before percolating below root zone. More details about the allocation of evaporation to different components are given in Paper III.

### **5.2.3 Impact of LAI on groundwater recharge**

Plant cover, represented as LAI, proved to be the most important model parameter determining the total recharge amount (Fig. 25). This has been reported in earlier simulation studies estimating groundwater recharge (Dripps 2012, Keese *et al.* 2005, Sophocleous 2000), but here the vegetation was represented with more spatially detailed patterns and a field data-based approach for LAI. However, some earlier field studies have claimed that the influence of LAI on total ET rates from boreal conifer canopies is minor (Kelliher *et al.* 1993, Ohta *et al.* 2001, Vesala *et al.* 2005). There appears to be a disagreement in the literature, with field studies suggesting that total ET is not much influenced by canopy LAI, whereas modelling studies such as the present thesis demonstrate a clear increase in ET with increasing LAI. Therefore more work is needed in matching the model estimates and field data for conifer ET. While soil (and snow) evaporation partly compensated for the lower transpiration for LAI values up to around 1.0, the total annual ET values progressively increased as a function of LAI (Fig. 25). Interestingly, the simulations suggested that ET remains constant in the LAI range 0–1, potentially due to the sparse canopy changing the aerodynamic resistance and partitioning of radiation limiting soil evaporation, while still not contributing much to transpiration in total ET. This suggests that the maximum groundwater recharge for boreal Scots pine remains rather constant up to a threshold LAI value of around 1. This knowledge can be used when co-managing forest and groundwater resources in order to optimise both.



**Fig. 25. Example of scatter plots with the mean annual evapotranspiration (ET) components are plotted as a function of the variable leaf area index (LAI), showing clear dependence of all ET components on LAI. CC BY 3.0 (Paper III).**

LAI values reported for conifer forests in Nordic conditions similar to the study site are in the range 1–3, depending on canopy density and other attributes (Koivusalo *et al.* 2008, Rautiainen *et al.* 2012, Vincke & Thiry 2008, Wang *et al.* 2004). The LAI values obtained for the study site (mean 1.25) were at the lower end of this range. Furthermore, the data showed a bimodal distribution, with many model cells with low LAI (<0.4) lowering the mean LAI (Fig. 12). The low LAI values were not considered to be an error in data or calculations, but were in fact expected because of active logging and clear-cutting in the study area. Although the equations to estimate LAI are empirical in nature and based on simplified assumptions, the method can outline spatial differences in canopy structure. However, the LAI estimation method could be further validated with field measurements or LiDAR techniques (Chasmer *et al.* 2012, Riaño *et al.* 2004).

The method allowed different land use scenarios in forestry management to be tested. The simulations showed that variable intensity of forestry, from low canopy coverage (LAI = 0–0.2) to dense coverage (LAI = 3.2–3.5), resulted in an average difference of 101.7 mm in annual recharge (Fig. 24). It can be argued that the

scenarios are unrealistic, because high LAI values, covering the whole study site, may not be achieved even with a complete absence of forestry operations. Nevertheless, the results demonstrate a substantial impact of forestry operations on esker aquifer groundwater resources. Previous work on the subject focused on changes in groundwater quality (Kubin 1998, Mannerkoski *et al.* 2005, Rusanen *et al.* 2004), whereas our simulations also have quantitative implications. However, more work should be done on comparing field and model estimates for conifer stand ET fluxes.

### **5.3 Surface-subsurface flow modelling of GW-lake interactions (IV)**

A fully integrated surface-subsurface groundwater model was established to simulate the transient hydrological processes in the esker aquifer, with particular emphasis on the fluxes at the GW-SW interface. The model successfully reproduced the hydrological processes of a complex esker aquifer with seepage and drainage lakes and interconnected streams in both steady state and transient mode. The simulation results provided information on GW-lake interactions which were validated with field measurements.

Water balance over the 13-year simulation period was distributed between: (1) Water input as rainfall and snowmelt (632 mm year<sup>-1</sup>), (2) evapotranspiration (297 mm year<sup>-1</sup>), (3) surface water outflow from the critical depth boundary condition (251 mm year<sup>-1</sup>), (4) subsurface outflow from the specified head boundary condition (79 mm year<sup>-1</sup>), and (5) net accumulation of water in the model domain (5 mm year<sup>-1</sup>). The values for annual precipitation and ET are typical for the study site area (Mustonen 1986). The model provided novel estimates of the amount of aquifer groundwater discharge from a complex shallow aquifer to regional surface water bodies. The River Oulujoki (Fig. 3) receives the majority (69.6 mm year<sup>-1</sup>) of the subsurface discharge, which was expected because of steepest gradients and deepest overburden layers at the boundary. Water accumulation in the model domain reflected the increase in storage due to elevated groundwater levels during the simulation period.

The model successfully reproduced the main dynamics in hydraulic head and stream flow in both transient and steady state mode. A detailed comparison of simulations and observations is given in Paper IV. Of the alternatives given in Table 3, hydraulic conductivity of  $2 \times 10^{-5} \text{ m s}^{-1}$  and an anisotropy ratio of 1:2 gave the best agreement between GW and lake head and stream outflow. Absolute mean error for simulated and observed GW and lake head was 2.38 m and 2.94 m, respectively. Errors of similar magnitude have been reported in earlier catchment-

scale surface-subsurface modelling studies (Goderniaux *et al.* 2009, Jones *et al.* 2008, Sudicky *et al.* 2008). The simulated head values were positively biased (simulated higher than measured) above 130 m asl. For all other calibration alternatives (Table 3), the GW and lake levels were underestimated, whereas the selected combination led to a slight general overestimation. Thus the most representative value for hydraulic conductivity and anisotropy was found in the lower end of the calibration range. A better fit could be obtained by adjusting the K value in the range  $6.5 \times 10^{-5} - 2 \times 10^{-5} \text{ m s}^{-1}$ , while keeping the anisotropy at 1:2. The simplifying assumption of homogeneous K throughout the aquifer inevitably introduced error into the simulations. Local-scale heterogeneities in the subsurface are undoubtedly present and could be captured by automated model calibration schemes, as done in another modelling study of the area (Rossi *et al.* 2014).

This thesis demonstrates the ability of the fully integrated hydrological simulation code HydroGeoSphere to represent the study site hydrological system at aquifer scale, while maintaining detailed simulations of GW-SW interactions in the model set-up. Previous fully integrated modelling studies have focused mainly on simulating domains delineated by surface water catchments (Goderniaux *et al.* 2009, Jones *et al.* 2008, Li *et al.* 2008). When modelling work has focused on lake systems, the models rarely cover the full extent of an aquifer (Kidmose *et al.* 2013, Smerdon *et al.* 2007, Viridi *et al.* 2013). The surface water bodies here were defined in the model only as topographical features derived from DEM and bathymetric maps, and the model routed water into lakes and streams in accordance with field measurements. The good level of general model performance provides more confidence about using fully integrated surface-subsurface models as a tool to simulate esker aquifers with interconnected lakes, streams and wetlands.

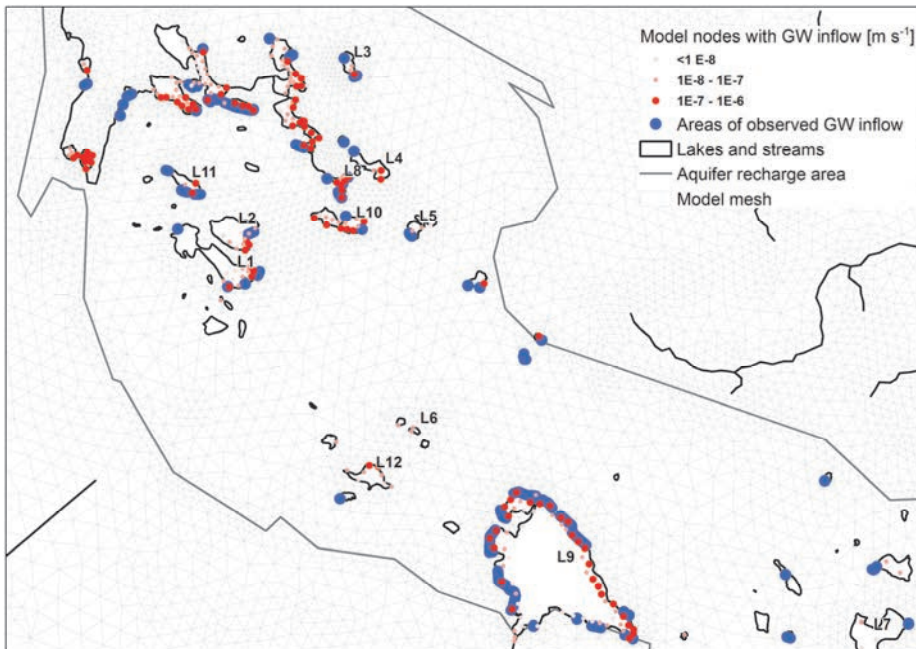
### **5.3.1 GW-lake interaction: discharge locations and fluxes**

#### ***Spatially distributed groundwater inflow to lakes***

To the best of my knowledge, this is the first study to compare the results of airborne thermal imaging with those of numerical simulations in a system of lakes. The general pattern of groundwater inflow locations to lakes, interpreted from areal thermal imaging, was captured by the simulations (Fig. 26). In most areas where TIR data showed groundwater discharge, there were also model nodes showing positive exchange flux between subsurface and surface domains. For example, in lake L9,



which continuously drains the aquifer, both observations and simulations showed groundwater discharge almost throughout the lake perimeter. The same was true for L8, although not apparent in detail because of smaller lake size. Only a few locations of groundwater inflow were missed by the simulations, for example in the north-east part of lakes L3, L4 and L11. The inability of thermal imaging to capture all groundwater discharge locations is best seen in lake L12, for which both simulations and isotope methods showed a clear signal of groundwater inflow (Fig. 27), but the TIR data did not reveal inflow locations to the lake (Fig. 26).



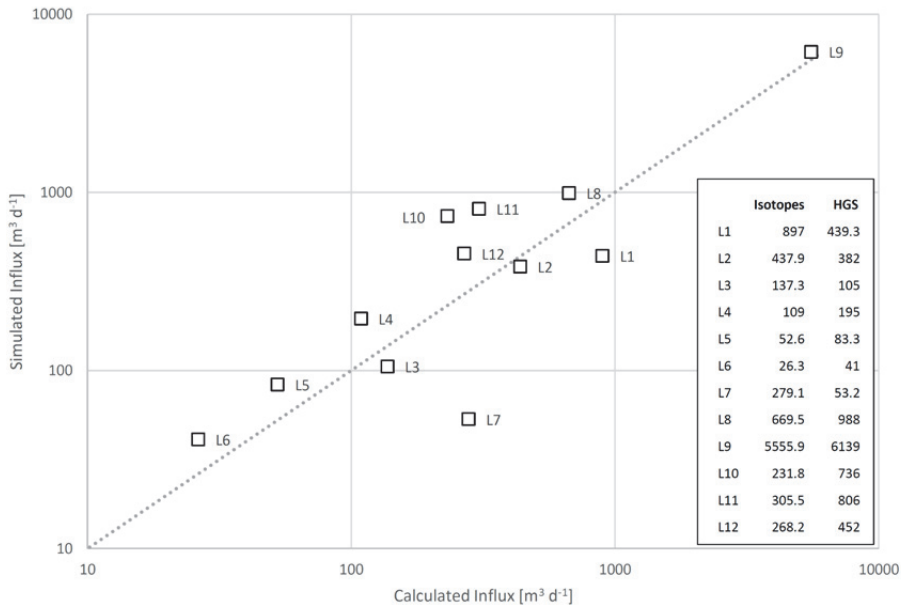
**Fig. 26. Locations of observed groundwater inflow from areal thermal imaging, which compared well with model cells where groundwater inflow was simulated.**

The differences between simulated and observed groundwater inflow locations are mainly attributable to difficulties in observing groundwater inflow in thermal imaging data (see Section 4.1.4), model mesh resolution, simplified geological model and model overestimation of groundwater head. Model mesh resolution was refined for the lakes with monitoring, but the topographical relief surrounding the lakes was still not fully captured. Therefore some local groundwater mounds around lakes may not be adequately represented in the

model, and some observed localised groundwater inflow may not be reproduced. In addition, some of the lake beds consisted of only a couple of cells (e.g. L4, L5, L6, L11) and the model resolution was too coarse to simulate the groundwater inflow focused near the lake shoreline in those cases. Finally, local subsurface heterogeneities and the distribution of lake bed sediments can have a great effect on GW-SW exchange locations (Kidmose *et al.* 2013, Smerdon *et al.* 2005). Because soil and lake bed were represented with uniform hydraulic parameterisation, GW-SW exchange hotspots due to local heterogeneities were overlooked by the simulations.

### *Comparison of simulated and calculated groundwater influxes to lakes*

In addition to similarity in spatial distribution, the magnitude of simulated groundwater inflow flux showed agreement with the inflow determined using stable isotope methods (Fig. 27). The magnitude of inflow ranged from tens to thousands of  $\text{m}^3 \text{s}^{-1}$ , the highest inflow being in L9 constantly draining via outlet S3. The simulations gave a good estimate of the order of magnitude in groundwater inflow, although some mismatches occurred in the absolute values. A better match between simulated and observed hydraulic head would probably bring the values even closer together. This result is promising, because total groundwater inflow is a difficult variable to estimate in a lake water balance. In the absence of surface runoff and stream inlets in particular, groundwater inflow can be the main source of nutrients in the lake water balance (Holman *et al.* 2010, Kidmose *et al.* 2013, Winter *et al.* 1998). Therefore a valid model-based estimate of the magnitude and spatial distribution of the groundwater influx, along with information on groundwater quality, can provide crucial information on ecologically relevant fluxes needed in current water resources management.



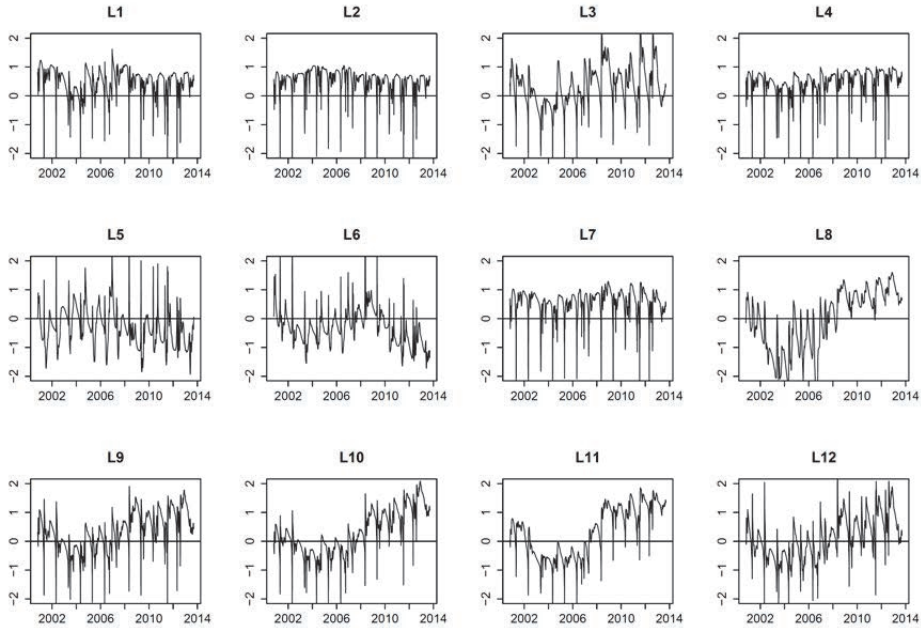
**Fig. 27. Calculated groundwater influx to various lakes in August 2013 using the stable isotope method (Isokangas *et al.* 2014) and the corresponding simulated groundwater influx values.**

The overall overestimation of groundwater head above 130 m asl can be seen as biased results in several GW-SW exchange outputs. Higher than observed head can be expected to provide excess groundwater discharge to lakes, especially drainage lakes. Because the outlet elevation is defined from the DEM draining the lake above the defined altitude, the increased hydraulic gradient due to head overestimation leads to increased groundwater influx. In the spatial distribution of groundwater discharge, this conclusion is supported by the most northerly lakes connected by a stream starting at L8. There, simulations showed extensive groundwater discharge to south-east parts of the lakes, whereas only little inflow was seen in areal thermal imaging (Fig. 26). Similar overestimation can be inferred for drainage lakes L8, L9 and L10 in terms of total influx (Fig. 27), where the simulations showed consistent overestimation. In reality, lake L10 did not have an outlet during the observation period (see Fig. 26), but closer examination of the simulation outputs showed an ephemeral surface flow connection emerging from lake L10 to L8. Thus the fully integrated modelling approach created a lake outlet in a physically based manner, where the

groundwater level reached the ground surface. The emerging outlet allowed seasonal draining of the lake, and thereby excess groundwater discharge. Finally, excess groundwater influx could be seen to some extent in stream flow, as flow rate overestimation for some of the streams which act as lake outlets (S3, S18 and S19).

### **5.3.2 Simulated transient variability in the GW-lake interaction**

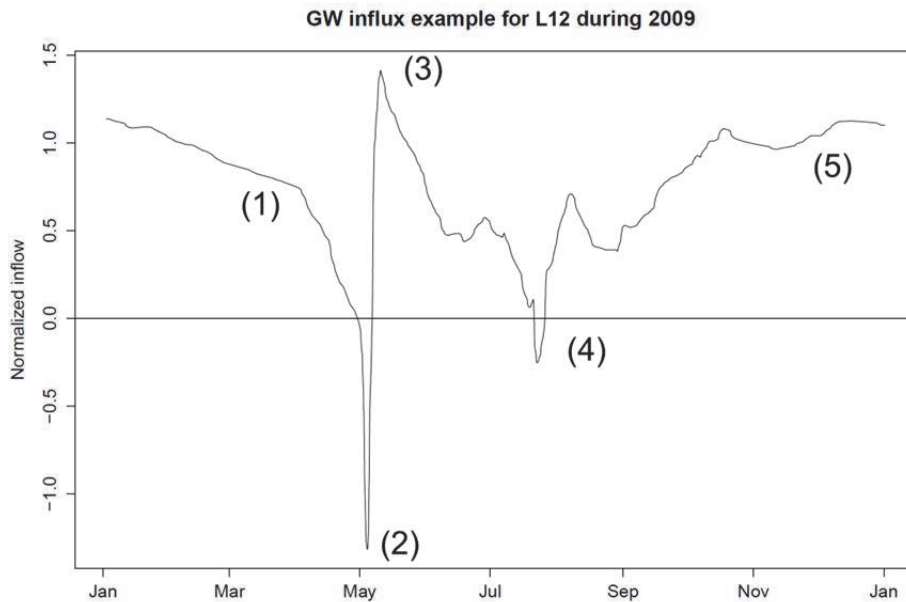
The fully integrated modelling approach enabled extraction of influx time series between lakes and groundwater. The time series of groundwater inflow showed both annual (seasonal) and interannual (long term) variability, which appeared to be different among lakes in the area (Fig. 28). Drainage lakes (L8, L9, and L10) exhibited different dynamics for groundwater inflow than seepage lakes. The level of seepage lakes followed the groundwater level, showing a similar decreasing trend until 2004 with a following rise until the end of simulations (see Fig. 4 in Paper IV). These changes can be attributed to natural climate variability, with drier conditions at the beginning of the simulation period. The water levels in drainage lakes, on the other hand, were kept relatively constant by the base of the outlet, as discussed earlier. This made the hydraulic gradient between lakes and groundwater decrease and increase according to the position of the groundwater table, creating interannual variability in groundwater inflow. For the seepage lakes, the lake water levels rose at approximately same rate as the groundwater level, therefore keeping the hydraulic gradient and influx more stable in the long term. Groundwater inflow trends are much more variable in closed basin lakes, with an increasing trend in some (L3, L11, L12) and a declining trend in others (L5, L6). Hunt *et al.* (2013) reported similar differences in transient lake inflow response between drainage and seepage lakes in their lake system modelling study.



**Fig. 28. Transient groundwater inflow to lakes, showing both seasonal and interannual variability. The time series are plotted as standardised values to facilitate comparison between different lakes (L1–L12).**

Several field methods enable the estimation of groundwater inflow time series on a small scale (Kalbus *et al.* 2006, Rosenberry & LaBaugh 2008), but studying and comparing transient influxes for a lake system would be highly laborious, if possible at all, with current techniques. Given that the model reproduced the spatial locations and flow volumes with acceptable accuracy, the transient variability in groundwater inflow can be studied in a meaningful way. However, it should be noted that the flux time series plotted in Fig. 28 were extracted from cells which exhibited groundwater inflow on 1 Aug 2013, to facilitate prior comparison with thermal imaging and stable isotope data. Some of the selected cells may seasonally shift in flow direction from in-seepage to out-seepage, whereas other cells showing out-seepage on 1 Aug 2013 may seasonally become in-seepage cells at other times. Therefore the time series most likely did not capture the full amplitude of the annual variability. However, closer examination of the shifting cells in model output showed that flux in those was generally some orders of magnitude lower than in cells of permanent high in-seepage selected for output (see red dots in Fig. 26). Thus Fig. 28 gives a good indication of the overall dynamics of the groundwater inflow into lakes at the study site.

Groundwater influx appeared to follow the groundwater table hydrograph typically found at latitudes with seasonal snow cover, such as the study site, except for the distinct and sudden decline in inflow at the onset of snowmelt (Fig. 29). This sudden decline appears to be physically unrealistic, but can be explained by how the model surface boundary conditions were executed. Water input from the snowmelt was simulated in Coup Model (Section 5.2) and acted as input to the current HGS model application. The input was defined as specified flux to the entire model top domain, including lakes. Therefore the free water surface at inundated lake nodes received the snowmelt water immediately, with perhaps some additional contribution from overland flow, whereas the response of the groundwater level was delayed due to the unsaturated layer. In reality, lake snow and ice cover is readily included in total hydraulic head for a given point, because the snow and ice are primarily ‘floating’ on the lake. The sudden increase in simulated lake head presumably levelled out the difference between the upgradient groundwater table and lake momentarily, ‘pushing back’ the groundwater inflow. After the sudden shock, the head stabilised and snowmelt reached the groundwater level, resulting in the expected increase in groundwater influx.



**Fig. 29.** Annual cycle for lake groundwater inflow, resembling a typical groundwater (GW) hydrograph and starting with declining inflow rates for Jan-April (1). At the onset of snowmelt, typically in early May (2), GW inflow decreased rapidly and quickly turned to elevated inflow (3); the amplitude of these shifts varied for different lakes (Fig. 8). Inflow started to decrease towards summer, with flow minima typically found in July (4). Inflow started to increase towards autumn (5), because of lower evapotranspiration and higher precipitation leading to rising GW levels.

When simulated GW-SW exchange flux was compared with the seepage meter measurements in L3 (Section 5.1.1), the latter showed a very similar distribution of groundwater inflow and outflow locations as simulated in the present thesis. The measured groundwater inflows were also of the same order of magnitude as the simulations. For example, the largest measured average inflow at the south-east corner of the lake during summer 2010 was  $5.7 \times 10^{-7} \text{ m s}^{-1}$ , while the simulations for the same period gave an average positive exchange flux of  $3.3 \times 10^{-7} \text{ m s}^{-1}$ . As a peculiarity, a preliminary round of seepage measurements in 2009 showed groundwater inflow from the north-west part of the lake. The later seepage meter measurements in slightly different locations during 2010 did not confirm the 2009 results, and the simulations did not result in inflow for the northern parts of the lake. Nonetheless, the areal thermal imaging interestingly showed a spot of groundwater

inflow at approximately the same location as measured in 2009. This demonstrates that exchange fluxes between GW and SW are highly variable in space and time and very difficult to characterise unambiguously, even by using several independent methods.



## 6 Conclusions and future recommendations

This thesis combined multiple field investigations and state-of-the-art numerical groundwater modelling methods to study hydrological processes in a complex esker aquifer. The research focused on the largely unknown interaction between the Rokua esker aquifer and lakes and streams located in the area. In addition to providing information on GW-SW exchange, the thesis enhanced the understanding of esker aquifer hydrology in terms of water quality and water budgets for both whole aquifer and single water body scale.

Paper I verified GW-lake interactions in the area with seepage meters and used environmental tracers to show the variable presence of groundwater in other lakes and streams in the area. Paper II studied GW-peatland interaction and demonstrated the role of peatland drainage in amplifying groundwater outflow from the aquifer. Paper III used numerical simulations to establish the influence of forestry land use and aquifer geometry on groundwater recharge. Paper IV merged the established process understanding and collected field data into a fully-integrated surface-subsurface flow model, which was used to simulate spatial variability, total inflow fluxes and transient changes in GW-lake interaction.

Both field and numerical studies highlighted that the GW-SW interactions in Rokua esker aquifer were highly variable in space for both lakes and streams. The groundwater discharged into lakes (in the groundwater recharge area) and peatland drainage ditches (in the groundwater discharge area) in very complex patterns. Discharge occurred both as focused flow in specific, spring-like locations and diffuse seepage covering a larger areal extent in both lakes and streams. Because of process complexity, investigations to understand detailed patterns of groundwater exfiltration into surface water bodies will remain a laborious task in esker aquifers.

At the Rokua esker, the GW-SW exchange process appeared to be more stable in time than in space. Therefore tools that can integrate the observed sporadic spatial variability into total fluxes over a larger spatial extent have great potential in studying the influence of groundwater on surface water bodies. The most prominent tool used in this thesis was fully integrated surface-subsurface flow modelling. The method provided estimates of the strength of groundwater inflow to surface water bodies which were consistent with field observations. However, all the field and modeling methods used in this thesis were helpful in establishing the conceptual process understanding needed in the integrated flow modelling. Therefore use of multiple methods for GW-SW interaction studies in esker aquifers is strongly recommended.

This thesis provides new information on the site-specific problems in the Rokua esker aquifer. Seepage lakes (lakes without outlets) have suffered periodically declining water levels, whereas the drainage lakes (lakes with outlets) have shown eutrophic water quality. Both these phenomena negatively affect the recreational use of the lakes, but they are also considered a threat to lake ecosystems. Water level variability in the transient surface-subsurface flow simulations agreed relatively well with the observed lake level changes. Therefore at least the most recent lake level decline (during the early 2000s) can be explained by climate variability, because no land use changes were included in the simulations. Rossi (2014) reached a similar conclusion, that the majority of the lake level variability can be explained by climate factors. However, peatland ditches may have a long-term draining effect on the aquifer, but this could not be verified in this thesis.

The role of groundwater as a nutrient source for Rokua's lakes was clarified in this thesis. The eutrophic status of drainage lakes is most likely related to nutrient-rich groundwater discharging to the lakes. The drainage lakes and groundwater are similarly enriched not only in nutrients (phosphate), but also in soil weathering products (silica, major cations), indicating groundwater input into the lakes. Notable groundwater inflow to the drainage lakes was also shown by the numerical modelling. The subsurface loading of nutrients carried by groundwater is nearly impossible to prevent, which has implications for surface water management practices. The results presented in this thesis suggest that groundwater inflow results in naturally eutrophic lakes in Rokua. This emphasises the need for integrated groundwater-surface water management, because neglecting the groundwater as a source of phosphorus influx to lakes would lead to misinformed management decisions. This thesis provides new knowledge on the potential role of groundwater on lake water quality when the lake is a part of complex esker aquifer system. However, the role of groundwater in surface water bodies will be different in other esker aquifers, both qualitatively and quantitatively, and therefore the results presented here cannot be generalised directly to other esker environments. Nevertheless, the methods applied in this work can be used to study site-specific hydrology in esker aquifers and address local management issues.

This thesis produced new information on how forestry land use can influence hydrological processes in esker aquifers. Forestry was found to affect the aquifer water storage in two opposing ways. Open drainage channels, excavated to drain the peat soil, have the unintended potential to also drain the underlying confined aquifer in groundwater discharge areas. In groundwater recharge areas, on the other hand, the main forestry operation is forestry logging. The simulations in this thesis suggest that

thinning or removing the tree canopy can result in an increase of 100 mm (30%) in groundwater recharge. Therefore land use actions can both decrease and increase groundwater storage. This adds to the previous statement that esker aquifers should be understood and managed as a single unit.

### *Proposals for future studies*

Based on the results presented in this thesis, the following research topics would further increase the understanding of esker aquifer hydrology:

- Changes in GW-SW interaction fluxes due to water abstraction should be tested with integrated surface-subsurface modelling methods. Such work would be beneficial in water resources management, where the impacts of water abstraction on the GW-SW interface are poorly understood and quantified.
- Rigorous automated model calibration and uncertainty estimation schemes need to be implemented in surface-subsurface models to understand the impact of model parameter uncertainty on the GW-SW exchange fluxes. Groundwater model calibration efforts usually focus on matching groundwater head and stream hydrographs, but novel methods, such as TIR and stable water isotopes, would enable the actual exchange fluxes to be used as a calibration objective.
- More attention should be paid to mechanisms of groundwater exfiltration to peatlands, where the groundwater discharge via preferential flowpaths in particular is poorly understood. Detailed field investigations in other aquifers would be needed to quantify the relevance of the phenomena shown here for esker aquifer management in general.
- More work should be done on comparing model and field-based ET estimates for boreal conifer canopies. The coupling of the vegetation-atmosphere boundary to the otherwise well-integrated surface-subsurface simulations could also be further developed.

This thesis provides an example of successful combination of field techniques and a fully integrated surface-subsurface model (HGS) application in a water resource problem. These numerical modelling techniques can provide data-based estimates on spatially and temporally variable fluxes of water, heat and nutrients, which determine the environmental conditions for ecological communities. This information will be increasingly called for in future water resources management, as the importance of

groundwater-dependent ecology is stressed in European Union and Finnish water legislation. The work presented in this thesis will hopefully promote the use of novel numerical simulation methods in studying esker aquifer hydrology. To fully exploit the potential of the methods presented here, more interdisciplinary research involving hydrology and ecology is needed for combined management of ecology and water resources. Future research efforts in esker aquifer hydrology should focus on establishing the role of groundwater in ecology related to esker aquifers.

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# Appendix 1

Borehole	"Alias"	Installed by	fully penetrating	Particle size analysis	Levelloggers	Monitoring started	Paper 1	Paper 2	Paper 3	Paper 4
G1	MEA106	ELY			x	2006	S			L
G2	MEA206	ELY			x	2006	S		L	L
G3	MEA1106	ELY			x	2006	S			L
G4	ROK2	ELY			x	2007				L
G5	ROK1	ELY			x	2006			L	L
G6	MEA506	ELY			x	2006	S,L		L	L
G7	MEA606	ELY			x	2006			L	L
G8	MEA706	ELY			x	2006	S			L
G9	ROK3	ELY			x	2004				L
G10	S1H	OY	x	x	x	2009	S	S,L		L
G11	S1R	OY			x	2009	S	S,L		L
G12 a&b	S1Hk/S1Tv	OY			x	2009		S,L		L
G13	S2H	OY	x	x	x	2009				L
G14	MEA2110	OY	x	x						
G15	Leväs.	OY		x						
G16	Vedeno.	OY	x	x						
G17	MEA2010	OY		x	x	2010	S			
G18	Ahmast.	OY	x	x						
G19	Vasikkak.	OY	x	x						
G20	MEA1907	ELY			x	2007	S,L		L	
G21	MEA1807	ELY			x	2007	S,L			
G22	S2R	OY			x	2009			L	

Alias: name of the borehole in other publications/databases

OY: installation by the University of Oulu

ELY: installation by the ELY Centre

S: borehole used in water sampling,

L: borehole used in level monitoring

## Appendix 2

Institution	Location WGS 84 coordinates (distance from site)	Variable	Resolutio n	Timespan	Comments
FMI	Oulunsalo airport 64.93; 25.36 (60 km)	T	3h	1960 – 2009	Daily data until 1960
		P	3h	1960 – 2009	
		W	3h	1960 – 2009	
		RH	3h	1960 – 2009	
		C	3h	1960 - 2009	
	Kajaani airport 64.28; 27.68 (60 km)	T	day/3h	1903 – 2009	
		P	day	1903 – 2009	
		W	3h	1960 – 2009	
		RH	3h	1960 - 2009	
		C	3h	1960 - 2009	
	Pelso climate station 64.46; 26.46 (5 km)	T	day/3h	1959 – 2014	
		P	day/3h	1959 – 2014	
		RH	6h/3h	1969 – 2014	
		W	6h/3h	1970 – 2014	
		interpolation grid 64.58;26.47 (0 km)	T	day/3h	
P			day	1961 – 2014	
W			day/3h	1961 – 2010	
UOULU	Rokua climate station 64.59; 26.50 (0 km)	RH	day/3h	1961 – 2010	
		RAD	day	1961 – 2014	
		T	30min	2009 ->	
		P	30min	2009 ->	
		W	30min	2009 ->	
		RH	30 min	2009 ->	
		RAD	30 min	2009 ->	
SYKE	Vaala snow line 64.58; 26.79 (5 km)	AP	30min	2009 ->	
		S	30min	2009 ->	
		S	three weeks	1950 – 2010	
	Lake Oulujärvi 22 km	T	daily (during open water)	1970 – 2014	Water surface temperature

## Original publications

- I Ala-aho P, Rossi, PM & Kløve, B (2013) Interaction of esker groundwater with headwater lakes and streams. *Journal of Hydrology* 500(2013): 144-156.
- II Rossi PM, Ala-aho P, Ronkanen A-K & Kløve B (2012) Groundwater-surface water interaction between an esker aquifer and a drained fen. *Journal of Hydrology* 432-433 (2012): 52-60.
- III Ala-aho P, Rossi, PM & Kløve, B (2014) Estimation of temporal and spatial variations in groundwater recharge in unconfined sand aquifers using scots pine inventories. *Hydrology and Earth System Sciences Discussions* 11: 7773-7826. (*Manuscript*)
- IV Ala-aho P, Rossi, PM, Isokangas E & Kløve, B (2014) Fully integrated surface-subsurface flow modelling of groundwater-lake interaction in an esker aquifer: Model verification with stable isotopes and airborne thermal imaging. (*Manuscript*)

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ISBN 978-952-62-0657-8 (Paperback)

ISBN 978-952-62-0658-5 (PDF)

ISSN 0355-3213 (Print)

ISSN 1796-2226 (Online)

