

PLANE-WAVE SCATTERING OF A PERIODIC CORRUGATED CYLINDER

by

Samuel Garcia

A Dissertation Submitted to the Faculty of

College of Engineering & Computer Science

In Partial Fulfillment of the Requirements for the Degree of

Doctor of Philosophy

Florida Atlantic University

Boca Raton, FL

May 2017

ProQuest Number: 10610475

All rights reserved

INFORMATION TO ALL USERS

The quality of this reproduction is dependent upon the quality of the copy submitted.

In the unlikely event that the author did not send a complete manuscript and there are missing pages, these will be noted. Also, if material had to be removed, a note will indicate the deletion.



ProQuest 10610475

Published by ProQuest LLC (2017). Copyright of the Dissertation is held by the Author.

All rights reserved.

This work is protected against unauthorized copying under Title 17, United States Code
Microform Edition © ProQuest LLC.

ProQuest LLC.
789 East Eisenhower Parkway
P.O. Box 1346
Ann Arbor, MI 48106 – 1346

Copyright 2017 by Samuel Garcia

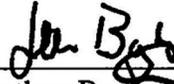
PLANE-WAVE SCATTERING OF A PERIODIC CORRUGATED CYLINDER

by

Samuel Garcia

This dissertation was prepared under the direction of the candidate's dissertation advisor, Dr. Jonathan Bagby, Department of Computer & Electrical Engineering and Computer Science, and has been approved by the members of his supervisory committee. It was submitted to the faculty of the College of Engineering & Computer Science and was accepted in partial fulfillment of the requirements for the degree of Doctor of Philosophy.

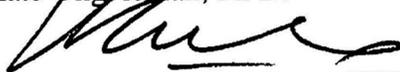
SUPERVISORY COMMITTEE:



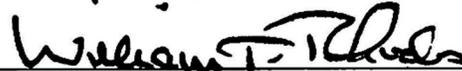
Jonathan Bagby, Ph D.
Dissertation Advisor



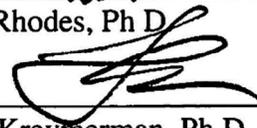
Vichate Ungvichian, Ph D.



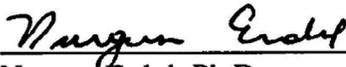
Valentine Aalo, Ph D.



William Rhodes, Ph D.



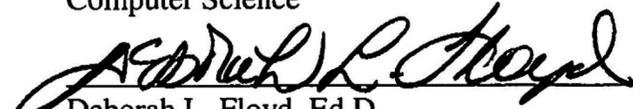
Grigoriy Kreymerman, Ph D.



Nurgun Erdol, Ph.D.
Chair, Department of Computer &
Electrical Engineering & Computer
Science



Mohammad Ilyas, Ph.D.
Dean, College of Engineering &
Computer Science



Deborah L. Floyd, Ed.D.
Dean, Graduate College

April 12, 2017

Date

ACKNOWLEDGEMENTS

This dissertation could not have been accomplished without the supervision and guidance of Dr. Jonathan Bagby, the Committee Chairperson and dissertation advisor. I would like to thank Dr. Bagby for his continued support throughout my PhD. His vast knowledge on this research material is something I admire. My sincere gratitude goes out to him for the guidance and advice he has given me.

I wish to thank the Committee Members, Dr. Valentine Aalo, Dr. Grigoriy Kreymerman, Dr. William Rhodes and Dr. Vichate Ungvichian for their time serving as members of the committee and providing their educated assessment to this dissertation. I would like to give an extra thanks Dr. Vichate Ungvichian, who stepped in to advise me for a semester. I owe him a debt of gratitude for that time and for his guidance and support.

I want to give a special thanks to my girlfriend, Ivette Morazzani, who's pushed me and advised me along this journey. She gave me constant encouragement and has shown an enormous amount of patience with me. She has also directly contributed to my success in helping me develop and learn the coding language used, along with running and reviewing countless simulations, lines of code, formulas and this dissertation itself.

I'm also greatly thankful for my family in supporting me through this journey. Their strength and support in me encouraged me to push through and achieve this goal of completing my dissertation.

ABSTRACT

Author: Samuel Garcia
Thesis: Plane-Wave Scattering of a Periodic Corrugated Cylinder
Institution: Florida Atlantic University
Dissertation Advisor: Dr. Jonathan Bagby
Degree: Doctorate of Philosophy
Year: 2016

In this dissertation, a novel approach to modeling the scattered field of a periodic corrugated cylinder, from an oblique incident planewave, is presented. The approach utilizes radial waveguide approximations for fields within the corrugations, which are point matched to approximated scattered fields outside of the corrugation to solve for the expansion coefficients. The point matching is done with TM_z and TE_z modes simultaneously, allowing for hybrid modes to exist.

The derivation of the fields and boundary conditions used are discussed in detail. Axial and radial propagating modes for the scattered fields are derived and discussed. Close treatment is given to field equations summation truncation and conversion to matrix form, for numerical computing. A detailed account of the modeling approach using Mathematica® and NCAIgebra for the noncommutative algebra, involved in solving for the expansion coefficients, are also given.

The modeling techniques offered provide a full description and prediction of the scattered field of a periodic corrugated cylinder. The model is configured to approximate a smooth cylinder, which is then compared against that of a textbook standard smooth cylinder. The methodology and analysis applied in this research provide a solution for computational electromagnetics, RF communications, Radar systems and the like, for the design, development, and analysis of such systems. Through the rapid modeling techniques developed in this research, early knowledge discovery can be made allowing for better more effective decision making to be made early in the design and investigation process of an RF project.

DEDICATION

First and foremost, this manuscript is dedicated to my late father. It's because of him I had any interest in becoming an electrical engineering. He always encouraged me to study and work hard. Growing up, he always gave me electrical projects to work on and challenge me. He started this PhD journey with me, but now, wherever he is, I know he'd be proud.

I also dedicated this to my girlfriend, Ivette Morazzani, who not only spent many years putting up with my research, she's also spent a lot of time reviewing my work and helping me code my work.

I would also like to dedicate this to my mom Mayte, my brother Carlos, my sister-in-law Paula and my nephews Carlos and Bryan. They have all supported me through this journey and have brought me joy in my toughest moments.

PLANE-WAVE SCATTERING OF A PERIODIC CORRUGATED CYLINDER

LIST OF TABLES	XII
LIST OF FIGURES	XIV
CHAPTER 1 INTRODUCTION	1
1.1 Objective.....	1
1.2 Background.....	2
1.3 Chapter-Wise Organization	3
CHAPTER 2 PERIODIC CORRUGATED CYLINDER: PHYSICAL DESCRIPTION AND ELECTROMAGNETIC APPLICATION.....	6
2.1 Physical Description	6
2.2 Infinite Length Approximation.....	7
2.3 Problem Space	8
2.4 Solution Approach	9
CHAPTER 3 INCIDENT FIELD	11
3.1 Incident Field TM_z mode	13
3.2 Incident Field TE_z mode	14
3.3 Total Incident Field.....	15

CHAPTER 4 REGION I – RADIAL WAVEGUIDE FIELD EQUATIONS	16
4.1 TM_z Mode Equations for Region I	17
4.1.1 Deriving $R_z(\rho)$ of E_z in Region I	19
4.1.2 Deriving $\Phi_z(\varphi)$ of E_z in Region I	19
4.1.3 Deriving $Z_z(z)$ of E_z in Region I	19
4.1.4 Deriving TM_z Mode Equations for Region I	22
4.2 TE_z Mode Equations for Region I	22
4.2.1 Deriving $R_z(\rho)$ of H_z in Region I	23
4.2.2 Deriving $\Phi_z(\varphi)$ of H_z in Region I	24
4.2.3 Deriving $Z_z(z)$ of H_z in Region I	24
4.2.4 Deriving TE_z Mode Equations for Region I	25
CHAPTER 5 REGION II – SCATTERED FIELD EQUATIONS	28
5.1 Equations for the TM_z Mode Scattered Field of Region II	29
5.2 Equations for the TE_z Mode Scattered Field of Region II	32
CHAPTER 6 BOUNDARY CONDITIONS & POINT MATCHING METHOD	33
6.1 General Boundary Conditions	33
6.2 Matrix Form of Field Equations	35
6.2.1 Matrix form of Region I Equations	36
6.2.2 Matrix form of Region II Equations	38
6.2.3 Matrix Equation Matches for Point Matching	40
6.3 Summation Truncation	42
6.4 Numeric Computation Techniques and Tool Methodology	44

6.4.1	Tool Selection and Use	44
6.4.2	Ill-Conditioned Matrices	46
6.4.3	Tool Methodology.....	46
CHAPTER 7 RESULTS, COMPARISONS AND FUTURE RESEARCH.....		50
7.1	Model Configuration and Parameters	50
7.1.1	Parameters Relative to Lambda.....	50
7.1.2	Incident Field Parameters.....	52
7.1.3	Point Matching Selection	52
7.1.4	Total E-Field Calculation	53
7.1.5	Reconciliation of Boundary 'a' and Boundary 'b'	53
7.2	RCS Computation	54
7.3	Smooth Cylinder Comparison Model	56
7.4	Alternate Corrugated Cylinder Method Comparison.....	58
7.5	Results.....	58
7.5.1	Run a.20.0.0 (b=20 λ , a=b*.001, $\rho_2=20\lambda$, m=0)	64
7.5.2	Run a.2.0.0 (b=2 λ , a=b*.001, $\rho_2=2\lambda$, m=0)	73
7.5.3	Run a.0.1.0.0 (b=0.1 λ , a=b*.001, $\rho_2=0.1\lambda$, m=0)	83
7.5.4	Run b.20.0.0 (b=20 λ , a=b*.001, $\rho_2=20\lambda$, m=0).....	92
7.5.5	Run b.2.0.0 (b=2 λ , a=b*.001, $\rho_2=2\lambda$, m=0).....	102
7.5.6	Run b.0.1.0.0 (b=0.1 λ , a=b*.001, $\rho_2=0.1\lambda$, m=0).....	112
7.5.7	Run a_plus_b.20.0.0 (b=20 λ , a=b*.001, $\rho_2=20\lambda$, m=0)	121
7.5.8	Run a_plus_b.2.0.0 (b=2 λ , a=b*.001, $\rho_2=2\lambda$, m=0)	131

7.5.9	Run a_plus_b.0.1.0.0 ($b=0.1\lambda$, $a=b*.001$, $\rho_2=0.1\lambda$, $m=0$)	141
7.5.10	Comparison to Other Corrugated Cylinder Methods	150
7.5.11	Varied Dielectric Constant with Comparisons	151
7.6	Conclusions.....	152
7.7	Open Questions for Future Research	154
APPENDICES	155
APPENDIX A	156
APPENDIX B	208

LIST OF TABLES

Table 1 Summary of boundary ‘a’ simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models	63
Table 2 Summary of boundary ‘b’ simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models	64
Table 3 Summary of boundary ‘a+b’ simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models	64
Table 4 Detailed parameters summary for changing ϕ plots of Run a.20.0.0	64
Table 5 Detailed parameters summary for changing ρ plots of Run a.20.0.0	69
Table 6 Detailed parameters summary for changing ϕ plots of Run a.2.0.0	73
Table 7 Detailed parameters summary for changing ρ plots of Run a.2.0.0	78
Table 8 Detailed parameters summary for changing ϕ plots of Run a.0.1.0.0	83
Table 9 Detailed parameters summary for changing ρ plots of Run a.0.1.0.0	88
Table 10 Detailed parameters summary for changing ϕ plots of Run b.20.0.0	92
Table 11 Detailed parameters summary for changing ρ plots of Run b.20.0.0	97
Table 12 Detailed parameters summary for changing ϕ plots of Run b.2.0.0	102
Table 13 Detailed parameters summary for changing ρ plots of Run b.2.0.0	107
Table 14 Detailed parameters summary for changing ϕ plots of Run b.0.1.0.0	112
Table 15 Detailed parameters summary for changing ρ plots of Run b.0.1.0.0	117
Table 16 Detailed parameters summary for changing ϕ plots of Run a_plus_b.20.0.0	121

Table 17 Detailed parameters summary for changing ρ plots of Run	
a_plus_b.20.0.0	126
Table 18 Detailed parameters summary for changing ϕ plots of Run	
a_plus_b.2.0.0	131
Table 19 Detailed parameters summary for changing ρ plots of Run	
a_plus_b.2.0.0	136
Table 20 Detailed parameters summary for changing ϕ plots of Run	
a_plus_b.0.1.0.0	141
Table 21 Detailed parameters summary for changing ρ plots of Run	
a_plus_b.0.1.0.0	146
Table 22 Detailed parameters summary for changing ϕ plots of Run	
a_plus_b.compare	150

LIST OF FIGURES

Figure 1-1 Example of a parabolic dish used in communications	3
Figure 2-1 Representation of a Segment of a Periodic Corrugated Cylinder: (a) 3D view of the Periodic Corrugated Cylinder (b) Cross-sectional view of the Periodic Corrugated Cylinder with Referenced Dimensions.....	7
Figure 2-2 PEC periodic corrugated cylinder of infinite length, radiated by incident planewave.....	8
Figure 3-1 Incident field shown with respect to corrugated cylinder for TM_z mode (a) and TE_z mode (b).....	12
Figure 4-1 Standing wave depicted in region I along the z-axis.....	18
Figure 4-2 Cross-sectional view of corrugated cylinder with multiple boundaries identified	20
Figure 5-1 A depiction of the vector decomposition of the wavenumber in region II.....	30
Figure 5-2 A depiction of constructive interference for a propagating wave along a periodic surface	30
Figure 6-1 A depiction for the general boundary conditions utilized to solve for the unknown coefficients	35
Figure 6-2 Software Process Workflow.....	48
Figure 6-3 Solving for Boundary ‘b’ Unknown Coefficients Flow Chart.....	48
Figure 6-4 Solving for Boundary ‘a’ Unknown Coefficients Flow Chart	49

Figure 7-1 Relative relationship of target size to illuminated wavelength with associated regions of scattering approximation, courtesy of Wikipedia [24].....	51
Figure 7-2 A run title example describing each component of the title and how it relates to the run's configuration	59
Figure 7-3 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'a'	61
Figure 7-4 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'b'	61
Figure 7-5 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'a+b'	62
Figure 7-6 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	65
Figure 7-7 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	65
Figure 7-8 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	66
Figure 7-9 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	66
Figure 7-10 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	67
Figure 7-11 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	67

Figure 7-12 XY Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	68
Figure 7-13 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	68
Figure 7-14 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	69
Figure 7-15 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	70
Figure 7-16 XY Plot of Scattered Field Amplitude Only, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	70
Figure 7-17 XY Plot of Scattered + Incident Field Amplitude, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	71
Figure 7-18 XY Plot of Scattered Field Amplitude Only, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	71
Figure 7-19 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	72

Figure 7-20 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0.....	72
Figure 7-21 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0	73
Figure 7-22 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	74
Figure 7-23 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	74
Figure 7-24 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	75
Figure 7-25 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0	75
Figure 7-26 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0	76
Figure 7-27 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0	76
Figure 7-28 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0	77
Figure 7-29 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	77

Figure 7-30 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	78
Figure 7-31 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	79
Figure 7-32 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	79
Figure 7-33 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	80
Figure 7-34 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	80
Figure 7-35 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	81
Figure 7-36 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	81

Figure 7-37 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0.....	82
Figure 7-38 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	83
Figure 7-39 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	84
Figure 7-40 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	84
Figure 7-41 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	85
Figure 7-42 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	85
Figure 7-43 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	86
Figure 7-44 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	86
Figure 7-45 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0.....	87
Figure 7-46 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0.....	88

Figure 7-47 XY Plot of Scattered + Incident Field Amplitude Only, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0	89
Figure 7-48 XY Plot of Scattered Field Amplitude Only, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0.....	89
Figure 7-49 XY Plot of Scattered + Incident Field Amplitude Only, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0	90
Figure 7-50 XY Plot of Scattered Field Amplitude Only, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0.....	90
Figure 7-51 XY Plot of Scattered + Incident Field Amplitude Only, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0	91
Figure 7-52 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0.....	91
Figure 7-53 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0	92
Figure 7-54 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	93

Figure 7-55 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	93
Figure 7-56 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	94
Figure 7-57 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0	94
Figure 7-58 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0	95
Figure 7-59 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0	95
Figure 7-60 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0	96
Figure 7-61 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0	96
Figure 7-62 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	97
Figure 7-63 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	98
Figure 7-64 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	98

Figure 7-65 XY Plot of Scattered + Incident Field Amplitude, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	99
Figure 7-66 XY Plot of Scattered Field Amplitude Only, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	99
Figure 7-67 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	100
Figure 7-68 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	100
Figure 7-69 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0.....	101
Figure 7-70 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	102
Figure 7-71 Polar Plot form of RCS dBsm for E_{ρ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	103
Figure 7-72 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	103
Figure 7-73 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	104

Figure 7-74 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0	104
Figure 7-75 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0	105
Figure 7-76 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0	105
Figure 7-77 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0	106
Figure 7-78 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	107
Figure 7-79 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	108
Figure 7-80 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	108
Figure 7-81 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	109
Figure 7-82 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	109

Figure 7-83 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	110
Figure 7-84 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	110
Figure 7-85 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0.....	111
Figure 7-86 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	112
Figure 7-87 Polar Plot form of RCS dBsm for E_{ρ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	113
Figure 7-88 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	113
Figure 7-89 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	114
Figure 7-90 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	114
Figure 7-91 XY Plot form of RCS dBsm for E_{ρ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	115
Figure 7-92 XY Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0.....	115

Figure 7-93 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0	116
Figure 7-94 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	117
Figure 7-95 XY Plot of Scattered + Incident Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	118
Figure 7-96 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	118
Figure 7-97 XY Plot of Scattered + Incident Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	119
Figure 7-98 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	119
Figure 7-99 XY Plot of Scattered + Incident Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	120
Figure 7-100 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0.....	120

Figure 7-101 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0	121
Figure 7-102 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	122
Figure 7-103 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	122
Figure 7-104 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	123
Figure 7-105 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0.....	123
Figure 7-106 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0.....	124
Figure 7-107 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0.....	124
Figure 7-108 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0.....	125
Figure 7-109 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0.....	125
Figure 7-110 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	126

Figure 7-111 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	127
Figure 7-112 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	127
Figure 7-113 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	128
Figure 7-114 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	128
Figure 7-115 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	129
Figure 7-116 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	129
Figure 7-117 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0	130
Figure 7-118 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	131

Figure 7-119 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	132
Figure 7-120 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	132
Figure 7-121 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0.....	133
Figure 7-122 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0.....	133
Figure 7-123 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0.....	134
Figure 7-124 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0.....	134
Figure 7-125 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0.....	135
Figure 7-126 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	136
Figure 7-127 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	137
Figure 7-128 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	137

Figure 7-129 XY Plot of Scattered + Incident Field Amplitude, for E_{ρ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	138
Figure 7-130 XY Plot of Scattered Field Amplitude Only, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	138
Figure 7-131 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	139
Figure 7-132 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	139
Figure 7-133 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0	140
Figure 7-134 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0	141
Figure 7-135 Polar Plot form of RCS dBsm for E_{ρ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0	142
Figure 7-136 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0	142

Figure 7-137 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0.....	143
Figure 7-138 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0.....	143
Figure 7-139 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0.....	144
Figure 7-140 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0.....	144
Figure 7-141 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0.....	145
Figure 7-142 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	146
Figure 7-143 XY Plot of Scattered + Incident Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	147
Figure 7-144 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	147
Figure 7-145 XY Plot of Scattered + Incident Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	148

Figure 7-146 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	148
Figure 7-147 XY Plot of Scattered + Incident Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	149
Figure 7-148 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	149
Figure 7-149 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0.....	150
Figure 7-150 XY Plot form of Cross-Polar Corrugated Cylinder $\sigma_{\phi\theta}/\lambda_0$ (dB) for Run a_plus_b. Compared with results of the finite element method (FEM) and method of moments (MoM) from [27]	151
Figure 7-151 Comparison of scattered axial fields of a smooth cylinder (solid line) with the corrugated cylinder (dotted line) with lossless dielectric loading of dielectric constant: $\epsilon_r=1$ a) $\epsilon_r=4$; b) $\epsilon_r=9$; c)	151
Figure 7-152 Axial scattered fields of a smooth cylinder (solid line) and corrugated cylinder (dotted line) with lossy dielectric loading. Dielectric constants: a) $\epsilon_r=4 - j1$; b) $\epsilon_r=6.29$; c) $\epsilon_r=6.29 - j1.73$	152

CHAPTER 1 INTRODUCTION

1.1 Objective

The scattered field due to a large periodic corrugated cylinder of quasi-infinite length is formulated and numerically determined in this dissertation. It is assumed that the boundaries and structure of the corrugated cylinder are constructed of Perfect Electrical Conductors (PECs). The present research provides an alternate technique for evaluating near-field scattering of a corrugated cylinder due to an incident plane wave while improving the computational efficiency of infinite array scattering using Floquet modes. The effect on the total electric field from variations of relative dimensions of the corrugated cylinder is also investigated.

Problems of scattering from periodic corrugated cylinders have been treated in the past. There has been investigation into the use of radial waveguide representation of the corrugated region [1] [2], asymptotic corrugation boundary conditions [3] [4], metallic ring representation [5], tensor permeability and tensor permittivity [6], and surface roughness function for corrugation representation [7]. However, treatment of this problem utilizing radial waveguide representation for the region within the corrugations and simultaneously working with Transverse Magnetic (TM) and Transverse Electric (TE) modes appears to be a new contribution to the field of computational electromagnetics, specifically with regards to scattering structures.

1.2 Background

In today's modern era of increasingly use of high-tech radio frequency (RF) communications and radar systems, it has become increasingly important to understand and mitigate the effects of RF or electromagnetic field scattering from common objects and geometries involved in those systems. That's because the more bandwidth and the greater sensitivity these instruments require, the more impactful inadvertent scattering off of nearby objects can be. The effect would cause an increase to the noise floor and distortion of intended signals, which reduces the overall quality and bandwidth of the data sent through the system. In the case of a 'stealth' type aircraft, unintended scattering would increase the aircraft's Radar Cross Section (RCS) which would improve an adversarial radar system's ability to detect that aircraft.

A common shape seen across all these systems is the cylinder. The fuselage of an aircraft and many external payloads are approximately cylindrical. The supporting struts for the transmitter/receiver on parabolic dishes (Figure 1-1), as such used in satellite communication, radio astronomy, etc. also tend to be cylindrical in shape. The present research provides a method of analysis for a modified geometry of these cylindrical structures, utilizing a periodic corrugation, in effect to optimize the design of them through assessment of their scattering.



Figure 1-1 Example of a parabolic dish used in communications

1.3 Chapter-Wise Organization

In order to provide a coherent and orderly research documentation, this dissertation has been organized categorically into chapters, which are summarized here:

- Chapter 1 Introduction

This chapter (current) is an introduction to the present research. It provides context and motivation for the field of research. It also provides a summary for the structure of the dissertation.

- Chapter 2 Periodic Corrugated Cylinder: Physical Description And Electromagnetic Application

This chapter describes the problem space in which the research is set. A detailed description of the geometry and electromagnetic treatment are discussed. The characteristics of the problem space that are varied are also

described. Floquet modes are invoked to represent the phase shift of the fields due to the periodicity of the structure. The nomenclature for the components, regions and other aspects of the problem space are established. Also, well established electromagnetic waveguide equations are represented and discussed. The overall approach for achieving solutions is also discussed as well as its validity.

□ Chapter 3 Incident Field

The incident plane-wave for TM & TE modes is described. The fields are further derived into their respective cylindrical coordinate components for both E-fields and H-fields.

□ Chapter 4 Region I – Radial Waveguide Field Equations

The fields between the corrugations are examined. Radial waveguide field equations were derived, based on Maxwell's equations. Boundary conditions are established as part of the derivation and further reduction of the equations. Finally, equations are developed for each respective cylindrical coordinate component for both E-fields and H-fields. Unknown coefficients are identified for solving in subsequent chapters.

□ Chapter 5 Region II – Scattered Field Equations

The scattered fields are derived and boundary conditions are established. Equations are developed for each respective cylindrical coordinate component for both E-fields and H-fields. Unknown coefficients are identified for solving in the subsequent chapter.

□ Chapter 6 Boundary Conditions & Point Matching Method

A point matching method is established for solving all the unknown coefficients. Equation sets are established for boundary conditions intended for point matching. All the field equations' summations are truncated from $+\infty$ and $-\infty$, to integers.

□ Chapter 7 Results, Comparisons and Future Research

Results are presented and discussed. General description of mathematical software tool and use are provided. Expressions identified for full description of solution space. A description of future research is also discussed.

CHAPTER 2 PERIODIC CORRUGATED CYLINDER: PHYSICAL DESCRIPTION AND ELECTROMAGNETIC APPLICATION

2.1 Physical Description

The subject of this paper is on the scatterer shown in Figure 2-1. It is a periodic corrugated cylinder of approximately infinite length, discussed further in the following section. The different dimensions of its components are referenced in Figure 2-1(b) with letter reference designators.

The corrugated cylinder is lined vertically with its center axis being on the z-axis. The inner radius of the corrugation is ρ_1 and the outer radius is ρ_2 along the ρ axis. The corrugated cylinder is symmetrical all along the ϕ axis. These corrugation pieces, also referred to here as discs, have a thickness (height in z direction) of b. The spacing between the corrugation (or discs) have a dimension of a. The values of these dimensions are discussed further in later chapters and will be described in terms of λ , wavelength of the incident plane-wave.

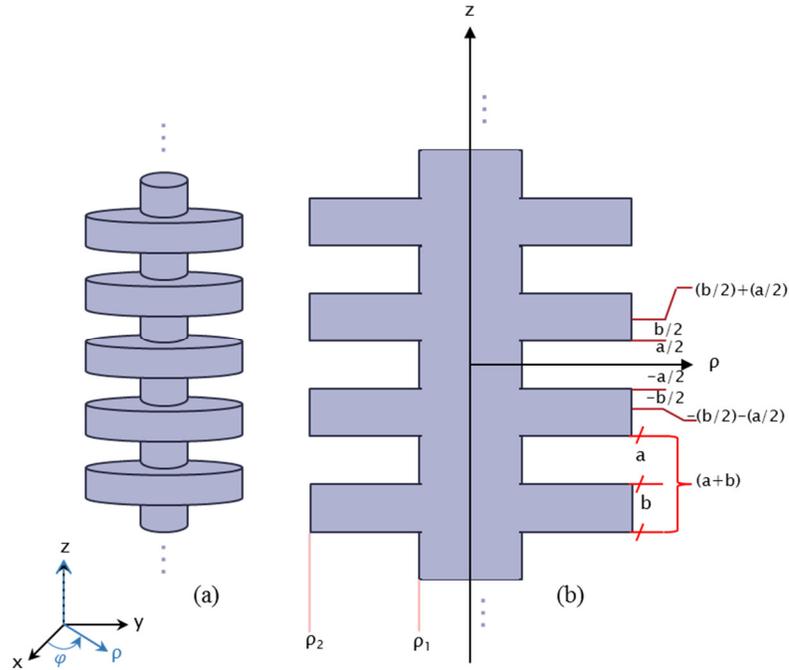


Figure 2-1 Representation of a Segment of a Periodic Corrugated Cylinder: (a) 3D view of the Periodic Corrugated Cylinder (b) Cross-sectional view of the Periodic Corrugated Cylinder with Referenced Dimensions

2.2 Infinite Length Approximation

When a periodic structure of infinite length, in this case a corrugated cylinder, is radiated by an incident field, the scattered field produced will contain multiple modes or space harmonics, which are coupled to the boundary conditions in which they must satisfy [8, p. 625]. These spatially periodic fields can be represented through Floquet modes. Floquet modes are modes of propagating waves that take on the symmetry of the periodic structure that wave has interfaced with. This is based on Floquet theory, in which a single period of the periodic structure is used to define the wave and accounting for the phase shift along the axis of propagation, which is also the axis of periodicity of the structure. A further description of Floquet modes and Floquet theory can be found in [9, pp. 264-266] and [8, pp. 605-608].

Practically, one works with smaller and finite length periodic structures and not infinitely long ones. However, sufficiently long periodic scatterers can be approximated as infinitely long allowing for simplification for mathematical models of the scattering fields [10], [11].

2.3 Problem Space

Consider a PEC periodic corrugated cylinder of infinite length as shown in Figure 2-2. Now consider that same corrugated cylinder in the presence of an incident planewave. That corrugated cylinder will perturb the incident planewave by behaving as a scatterer. Many have approached the problem of calculating the scattered field, such as Manara [1] [2], Kishk [4], Freni [5] and Hillion [7].

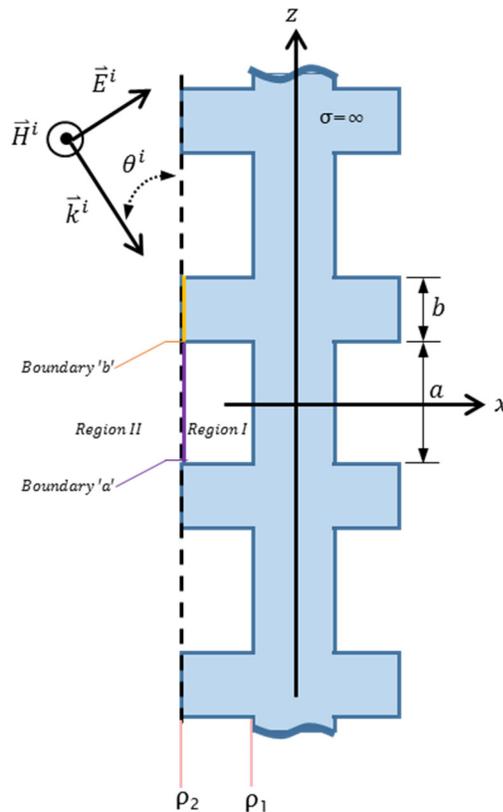


Figure 2-2 PEC periodic corrugated cylinder of infinite length, radiated by incident planewave

However, the method proposed in this paper describes the simultaneous use of the Transverse Magnetic (TM_z) and the Transverse Electric (TE_z) field modes, with respect to the z-axis, to solve the problem of predicting the scattered fields. As implied by Constantine A. Balanis in his work on describing scattering by a conducting circular cylinder of an oblique planewave, a cylinder structure that deviates from a smooth cylinder can experience depolarizations of the fields due to the scattering [12, p. 615]. Based on this statement, this work makes the assumption of a hybrid mode when scattering from a corrugated cylinder. Therefore, the TM_z and the TE_z modes shall be accounted for simultaneously and depolarization of the fields from one mode to another can occur.

Along with TM_z and the TE_z modes, this approach also utilizes a radial waveguide representation of the fields within the corrugations (region I) which the full solution for is formulated in conjunction with the fields outside of the corrugations (region II). The radial waveguide method has been investigated by Manara [1]. The combination of TM_z and the TE_z modes with the radial waveguide representation provides a more complete description of the scattered field from a periodic corrugated cylinder, that is novel and has not been observed by the author in previous literature.

2.4 Solution Approach

Having been presented with a description of the problem space, the reader can now follow along with the solution approach, a step-by-step guide on how to utilize the problem space components provided in order to solve the problem (predicting the scattered fields) of a known PEC periodic corrugated cylinder.

Step 1: Identify the incident planewaves

Step 2: Derive solutions to Helmholtz equations for the fields in region I

Step 3: Derive solutions to Helmholtz equations for the scattered fields in region II

Step 4: Truncate all summation equations to finite ranges and represent in matrix form

Step 5: Apply boundary conditions for fields in region I and region II to solve for unknown coefficients

Step 6: Symbolically and numerically compute solutions for unknown coefficients

This is the solution approach that is represented in this paper. Steps 1, 2 and 3 are described in chapters 3, 4 and 5 respectively. Steps 4, 5 and 6 are covered in chapter 6. Step 6 is where a great deal of time and effort was spent by the author in developing the appropriate numerical computing approach.

In this paper, the fields and incident planewaves are considered to be time harmonic, as shown in equations (2-1) and (2-2). Only the vector phasor component, $\vec{E}(x, y, z)$, will be considered and the $e^{j\omega t}$ will be omitted for simplification.

$$\vec{E}(x, y, z, t) = \text{Re}[\vec{E}(x, y, z)]e^{j\omega t} \quad (2-1)$$

$$\vec{H}(x, y, z, t) = \text{Re}[\vec{H}(x, y, z)]e^{j\omega t}. \quad (2-2)$$

The field equations and solutions to them, presented in this paper will be in the cylindrical coordinate form (i.e. $\hat{\rho}$, $\hat{\phi}$, and \hat{z} axes), with the exception of the introduction of the incident field in Chapter 3.

CHAPTER 3 INCIDENT FIELD

Now consider an unbounded medium, referred to here as region II, which is a near infinite media and void of any scatterers. This description allows for the easy modeling of a propagating incident planewave. An idealistic view as such is incomplete, with regards to the scattered field, in the presence of a scatterer (as in the case of the periodic corrugated cylinder). In order to appropriately describe the total fields (E^t , H^t), superposition can be used, as shown in equations (3.1) and (3.2), in which the incident field (E^i , H^i) is added to the scattered field (E^s & H^s , field created by a scatterer in the presence of a propagating field) in order to get the total field. Deriving the scattered field is the subject of chapter 5. This chapter will focus on the incident field.

$$E^t = E^i + E^s \quad (3-1)$$

$$H^t = H^i + H^s. \quad (3-2)$$

The problem space and solution approach require that the solution set be driven by two sets of modes, the TM and TE modes. Separate treatment will be given to these modes when describing the field components. However, when solving for boundary conditions at the point matching phase, these modes will be combined through invoking superposition. For now, the driving incident field will be separated in its TM and TE modes. It's also important to note here that the present work is done on oblique incident planewaves and not normal incident planewaves.

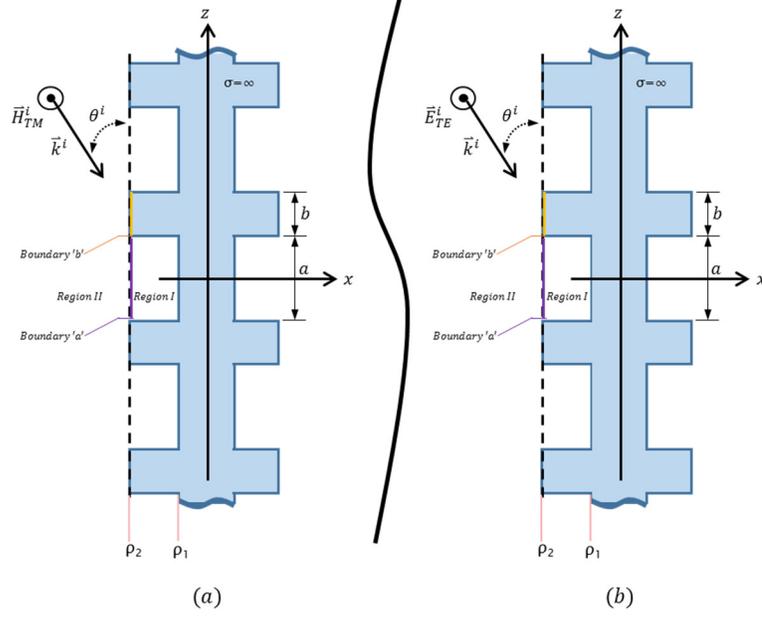


Figure 3-1 Incident field shown with respect to corrugated cylinder for TM_z mode (a) and TE_z mode (b)

Depicted in Figure 3-1(a) is a TM_z mode planewave, in region II, which is incident to a periodic corrugated cylinder. In Figure 3-1(b), the same structure is shown only now with a TE_z mode planewave that's incident. In both scenarios, the planewave is traveling in the same direction, as indicated by θ^i (angle of incidence) and the wave vector \vec{k}^i , which is given by

$$\vec{k}^i = k[\hat{x} \sin \theta^i - \hat{z} \cos \theta^i] \quad (3-3)$$

where $k = \omega\sqrt{\mu\varepsilon}$ is the wavenumber. In region II, as is the case for the incident field, $k = \omega\sqrt{\mu_{II}\varepsilon_{II}}$ where $\mu = \mu_{II}$ and $\varepsilon = \varepsilon_{II}$. In region I, covered in detail in Chapter 4, $k = \omega\sqrt{\mu_I\varepsilon_I}$ where $\mu = \mu_I$ and $\varepsilon = \varepsilon_I$.

Here is a brief description of TM_z and TE_z modes of a propagating wave, to aid the reader through this paper. A transverse magnetic mode, with respect to the z -axis (TM_z), of a propagating wave, is that of a wave that has its magnetic field components in

a plane that is perpendicular (transverse) to the z-axis. Therefore, there is no magnetic field component on the z-axis, or $H_z=0$, for a TM_z mode.

A transverse electric mode, with respect to the z-axis (TE_z), of a propagating wave, follows the same logic as that of the transverse magnetic, but rather now it's the electric field component that is perpendicular (transverse) to the z-axis. In this case of a TE_z mode, there is no electric field component on the z-axis, or $E_z=0$.

3.1 Incident Field TM_z mode

In the case of the TM_z incidence, the equation for the electric field is given by equation (3.4) for rectangular coordinates and (3.5) for cylindrical coordinates. The component $Z = \sqrt{\frac{\mu_{II}}{\epsilon_{II}}}$ is intrinsic impedance of region II. Conversion of a vector field between coordinate system types can be found in [12, pp. 920-923] .

$$\vec{E}^i = E_0[\hat{x} \cos \theta^i + \hat{z} \sin \theta^i]e^{-jk[x \sin \theta^i - z \cos \theta^i]} \quad (3-4)$$

$$\vec{E}^i = E_0[\hat{\rho} \cos \varphi \cos \theta^i - \hat{\phi} \sin \varphi \cos \theta^i + \hat{z} \sin \theta^i]e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-5)$$

The corresponding magnetic fields are given using and expanding on Maxwell's curl equations, which a full example can be found in [12, pp. 616-618] to get equations (3-6) for rectangular coordinates and (3-7) for cylindrical coordinates.

$$\begin{aligned} \vec{H}^i &= \frac{1}{Z} \hat{k} \times \vec{E}^i = \frac{E_0}{Z} [\hat{x} \sin \theta^i - \hat{z} \cos \theta^i] \times [\hat{x} \cos \theta^i + \hat{z} \sin \theta^i] e^{-jk[x \sin \theta^i - z \cos \theta^i]} \\ &= -\hat{y} \frac{E_0}{Z} e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \end{aligned} \quad (3-6)$$

$$\vec{H}^i = \frac{E_0}{Z} [-\hat{\rho} \sin \varphi - \hat{\phi} \cos \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-7)$$

Further breaking down the electric and magnetic field equations into their coordinate constituents, we get equations

$$E_{z^{II}}^i = E_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-8)$$

$$E_{\rho_{TM^{II}}}^i = E_0 \cos \varphi \cos \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-9)$$

$$E_{\varphi_{TM^{II}}}^i = -E_0 \sin \varphi \cos \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-10)$$

$$H_{\rho_{TM^{II}}}^i = -\frac{E_0}{Z} \sin \varphi e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-11)$$

$$H_{\varphi_{TM^{II}}}^i = -\frac{E_0}{Z} \cos \varphi e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-12)$$

which now provides a more manageable description of the TM_z mode incident field as will be seen in the later chapters.

3.2 Incident Field TE_z mode

In the case of the TE_z incidence, the equation for the magnetic field is given by equation (3-13) for rectangular coordinates and (3-14) for cylindrical coordinates.

$$\vec{H}^i = H_0 [\hat{x} \cos \theta^i + \hat{z} \sin \theta^i] e^{-jk[x \sin \theta^i - z \cos \theta^i]} \quad (3-13)$$

$$\vec{H}^i = H_0 [\hat{\rho} \cos \varphi \cos \theta^i - \hat{\varphi} \sin \varphi \cos \theta^i + \hat{z} \sin \theta^i] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi}. \quad (3-14)$$

The corresponding electric fields are given by (3-15) for rectangular coordinates and (3-16) for cylindrical coordinates.

$$\vec{E}^i = Z\vec{H}^i \times \hat{k} = ZH_0 [\hat{x} \cos \theta^i + \hat{z} \sin \theta^i] \times [\hat{x} \sin \theta^i - \hat{z} \cos \theta^i] e^{-jk[x \sin \theta^i - z \cos \theta^i]} = \hat{y} ZH_0 e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-15)$$

$$\vec{E}^i = ZH_0 [\hat{\rho} \sin \varphi + \hat{\varphi} \cos \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-16)$$

As was done in the incident Field TM_z mode section, a further breakdown of the TE_z mode field equations into their coordinate constituents gives

$$H_{zII}^i = H_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-17)$$

$$E_{\rho_{TEII}}^i = ZH_0 \sin \varphi e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-18)$$

$$E_{\varphi_{TEII}}^i = ZH_0 \cos \varphi e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-19)$$

$$H_{\rho_{TEII}}^i = H_0 \cos \varphi \cos \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-20)$$

$$H_{\varphi_{TEII}}^i = -H_0 \sin \varphi \cos \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-21)$$

completing the full component breakdown description of the incident field.

3.3 Total Incident Field

Due to the hybrid nature of the corrugated cylinder, both TM_z and TE_z modes will be used simultaneously. Therefore, the TM_z and TE_z mode fields in the cylindrical coordinate orientation will be combined to form

$$E_{zII}^i = E_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-22)$$

$$E_{\rho II}^i = [E_0 \cos \varphi \cos \theta^i + ZH_0 \sin \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-23)$$

$$E_{\varphi II}^i = [-E_0 \sin \varphi \cos \theta^i + ZH_0 \cos \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-24)$$

$$H_{zII}^i = H_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-25)$$

$$H_{\rho II}^i = \left[-\frac{E_0}{Z} \sin \varphi + H_0 \cos \varphi \cos \theta^i \right] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-26)$$

$$H_{\varphi II}^i = \left[-\frac{E_0}{Z} \cos \varphi - H_0 \sin \varphi \cos \theta^i \right] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \quad (3-27)$$

CHAPTER 4 REGION I – RADIAL WAVEGUIDE FIELD EQUATIONS

This chapter will focus on deriving the field equations for region I, the region between the corrugations as can be seen in Figure 3-1. The approach to deriving the equations shown is to start with the Fundamental Equations of Guided Waves (FEGW) in cylindrical form, given by

$$E_\rho = \frac{-j}{k_\rho^2} \left[k_z \frac{\partial E_z}{\partial \rho} + \frac{\omega \mu}{\rho} \frac{\partial H_z}{\partial \varphi} \right] \quad (4-1)$$

$$E_\varphi = \frac{-j}{k_\rho^2} \left[k_z \frac{\partial E_z}{\partial \varphi} - \omega \mu \frac{\partial H_z}{\partial \rho} \right] \quad (4-2)$$

$$H_\rho = \frac{j}{k_\rho^2} \left[\frac{\omega \varepsilon}{\rho} \frac{\partial E_z}{\partial \varphi} - k_z \frac{\partial H_z}{\partial \rho} \right] \quad (4-3)$$

$$H_\varphi = \frac{-j}{k_\rho^2} \left[\omega \varepsilon \frac{\partial E_z}{\partial \rho} + \frac{k_z}{\rho} \frac{\partial H_z}{\partial \varphi} \right] \quad (4-4)$$

where

$$k_\rho = \sqrt{k^2 - k_z^2} \quad (4-5)$$

and as mentioned in Chapter 3, $k = \omega \sqrt{\mu_I \varepsilon_I}$, when referring to the wavenumber k in equations from region I. These equations are derived from Maxwell's equations and can be found in any electromagnetic textbook [13, p. 118].

Note that these FEGWs are in terms of H_z and E_z . When utilizing these equations for TM_z or TE_z modes, H_z or E_z respectively can be set to zero further simplifying the equations. This will be useful in the subsequent sections, in order to derive the appropriate form for many of the equations.

4.1 TM_z Mode Equations for Region I

For the TM_z mode, the FEGWs can be rewritten as

$$E_{\rho} = \frac{-j}{k_{\rho}^2} \left[k_z \frac{\partial E_z}{\partial \rho} \right] \quad (4-6)$$

$$E_{\varphi} = \frac{-j}{k_{\rho}^2} \left[\frac{k_z}{\rho} \frac{\partial E_z}{\partial \varphi} \right] \quad (4-7)$$

$$H_{\rho} = \frac{j}{k_{\rho}^2} \left[\frac{\omega \varepsilon}{\rho} \frac{\partial E_z}{\partial \varphi} \right] \quad (4-8)$$

$$H_{\varphi} = \frac{-j}{k_{\rho}^2} \left[\omega \varepsilon \frac{\partial E_z}{\partial \rho} \right] \quad (4-9)$$

by substituting in $H_z=0$.

It is now apparent that all the FEGWs equations are in terms of E_z . The only term now left to develop an equation for is E_z . In order to derive a vector field wave equation for E_z , region I will be assumed to be lossless and source free, in order to simplify the mathematics. This will allow for the use of the Helmholtz vector wave equation in the form

$$\nabla^2 E_z + k^2 E_z = 0 \quad (4-10)$$

which can be used to derive an equation for E_z . Further detail and derivation of the Helmholtz equations can be found in [13, p. 116].

The other assumption is that E_z , being composed of all the cylindrical field components, or $E_z = E_z(\rho, \varphi, z)$, is separable into its constituent components, such that

$$E_z = R_z(\rho) \phi_z(\varphi) Z_z(z) . \quad (4-11)$$

Now, substituting equation (4-11) into equation (4-10) yields 3 sets of differential second order equations, one for each coordinate component. Since this is a common process in the field of electromagnets, details of these steps are will not be shown here but can be found in [13, p. 118]. However, solutions to these second order homogenous differential equations take the form of

$$R_z(\rho) = \begin{cases} A_1 J_n(k_\rho \rho) + B_1 Y_n(k_\rho \rho) \leftarrow \text{Standing Wave} \\ C_1 H_n^{(1)}(k_\rho \rho) + D_1 H_n^{(2)}(k_\rho \rho) \leftarrow \text{Traveling Wave} \end{cases} \quad (4-12)$$

$$\phi_z(\varphi) = \begin{cases} A_2 \cos n\varphi + B_2 \sin n\varphi \leftarrow \text{Standing Wave} \\ C_2 e^{-jn\varphi} + D_2 e^{jn\varphi} \leftarrow \text{Traveling Wave} \end{cases} \quad (4-13)$$

$$Z_z(z) = \begin{cases} A_3 \cos k_z z + B_3 \sin k_z z \leftarrow \text{Standing Wave} \\ C_3 e^{-jk_z z} + D_3 e^{jk_z z} \leftarrow \text{Traveling Wave} \end{cases} \quad (4-14)$$

It is important to note the geometry of the structure of region I, which behaves as a radial waveguide, in order to appropriately select the standing wave or traveling wave solution for each of the E_z subcomponents. The structure allows for traveling waves in the ρ and φ direction. However, in the z direction, only a standing wave can exist as depicted in Figure 4-1. Therefore, the solutions for each of the E_z subcomponents will be selected as

$$R_z(\rho) = C_1 H_n^{(1)}(k_\rho \rho) + D_1 H_n^{(2)}(k_\rho \rho) \leftarrow \text{Traveling Wave} \quad (4-15)$$

$$\phi_z(\varphi) = C_2 e^{-jn\varphi} + D_2 e^{jn\varphi} \leftarrow \text{Traveling Wave} \quad (4-16)$$

$$Z_z(z) = A_3 \cos k_z z + B_3 \sin k_z z \leftarrow \text{Standing Wave} \quad (4-17)$$

which leads to

$$E_z = \left(C_1 H_n^{(1)}(k_\rho \rho) + D_1 H_n^{(2)}(k_\rho \rho) \right) (C_2 e^{-jn\varphi} + D_2 e^{jn\varphi}) (A_3 \cos k_z z + B_3 \sin k_z z) . \quad (4-18)$$

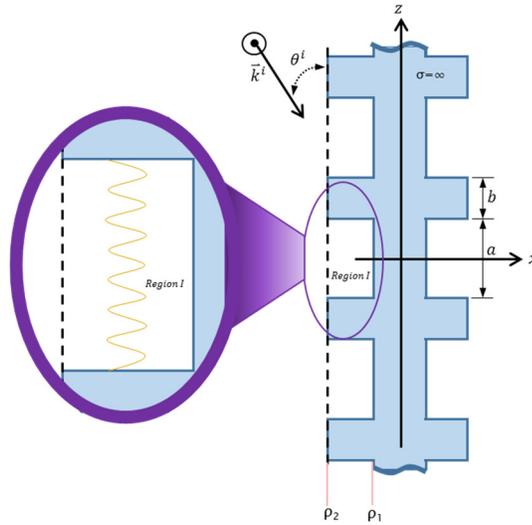


Figure 4-1 Standing wave depicted in region I along the z -axis

4.1.1 Deriving $R_z(\rho)$ of E_z in Region I

From here, the next step is to reduce each E_z subcomponents starting with $R_z(\rho)$.

This can be done with using the using boundary condition $\rho=\rho_1$ where $R_z(\rho) = 0$ or

$$C_1 H_n^{(1)}(k_\rho \rho_1) + D_1 H_n^{(2)}(k_\rho \rho_1) = 0 \quad (4-19)$$

Now solve for D_1 which will give

$$D_1 = -C_1 \frac{H_n^{(1)}(k_\rho \rho_1)}{H_n^{(2)}(k_\rho \rho_1)}. \quad (4-20)$$

Plug D_1 back into equation (4-15) to give

$$C_1 H_n^{(1)}(k_\rho \rho) - C_1 \frac{H_n^{(1)}(k_\rho \rho_1)}{H_n^{(2)}(k_\rho \rho_1)} H_n^{(2)}(k_\rho \rho) = C_1 \left(H_n^{(1)}(k_\rho \rho) - \frac{H_n^{(1)}(k_\rho \rho_1)}{H_n^{(2)}(k_\rho \rho_1)} H_n^{(2)}(k_\rho \rho) \right). \quad (4-21)$$

4.1.2 Deriving $\Phi_z(\varphi)$ of E_z in Region I

Simplifying $\Phi_z(\varphi)$ is a little bit easier, as it requires very little manipulation.

Since the two terms are exponentials each multiplied by a coefficient, have the same exponents but just with opposite signs, and will be incorporated into a summation that has 'n' going from $-\infty$ to $+\infty$, the two terms can be written as a single term inside a summation. Doing so yields

$$\sum_{n=-\infty}^{\infty} A_n e^{jn\varphi} \quad (4-22)$$

where A_n is the coefficient with an 'n' subscript representing the index where, 'n' represents the circumferential (φ) variations.

4.1.3 Deriving $Z_z(z)$ of E_z in Region I

The remaining term (z), for E_z , Z_z , can be simplified using the boundary condition of $z=\pm a/2$ where $\frac{\partial Z_z(z)}{\partial z}$ is set equal to 0. This is possible due to the boundary condition of E_ρ and E_φ being equal to zero at $z=\pm a/2$ and both having components of $\partial E_z / \partial z$ as shown by

$$E_\varphi \sim E_\rho \sim \frac{\partial Z_z(z)}{\partial z} = \frac{\partial(A_3 \cos k_z z + B_3 \sin k_z z)}{\partial z} = Z'_z(z) = -A_3 k_z \sin k_z z + k_z B_3 \cos k_z z \quad (4-23)$$

which will need to be set to zero for this boundary condition. As shown in Figure 4-2, E_φ and E_ρ are tangential to the PEC at $z=\pm a/2$ and therefore equal to zero, leading to

$$\begin{cases} -A_3 k_z \sin k_z z + k_z B_3 \cos k_z z = 0 = \\ -A_3 k_z \sin\left(k_z \frac{a}{2}\right) + B_3 k_z \cos\left(k_z \frac{a}{2}\right) = 0 & , z = \frac{a}{2} \\ -A_3 k_z \sin\left(-k_z \frac{a}{2}\right) + B_3 k_z \cos\left(-k_z \frac{a}{2}\right) = 0 & , z = -\frac{a}{2} \end{cases} \quad (4-24)$$

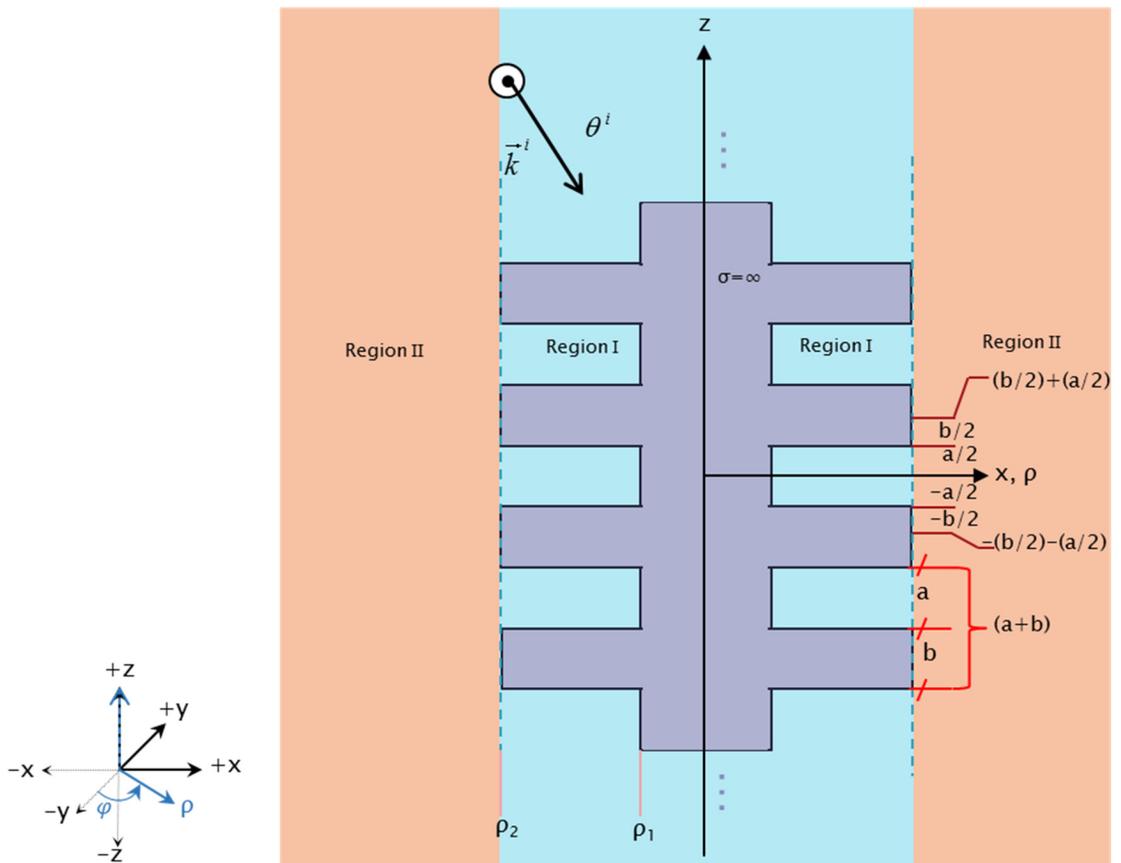


Figure 4-2 Cross-sectional view of corrugated cylinder with multiple boundaries identified

Choosing the equation form where $z = \frac{a}{2}$, the coefficient A_3 can be solved for, which yields

$$A_3 = \frac{B_3 k_z \cos\left(k_z \frac{a}{2}\right)}{k_z \sin\left(k_z \frac{a}{2}\right)}. \quad (4-25)$$

Plug A_3 back into the $Z_z(z)$ equation to get

$$Z_z(z) = \frac{B_3 k_z \cos\left(k_z \frac{a}{2}\right)}{k_z \sin\left(k_z \frac{a}{2}\right)} \cos k_z z + B_3 \sin k_z z = B_3 \left(\sin k_z z + \frac{\cos\left(k_z \frac{a}{2}\right)}{\sin\left(k_z \frac{a}{2}\right)} \cos k_z z \right). \quad (4-26)$$

Since k_z is anticipated to be a constant, a new constant $B'_3 = B_3 / \sin k_z \frac{a}{2}$ can be defined and plugged back into $Z_z(z)$ equation giving

$$Z_z(z) = B'_3 \left(\sin k_z \frac{a}{2} \sin k_z z + \cos k_z \frac{a}{2} \cos k_z z \right). \quad (4-27)$$

This expression can be simplified further using the trigonometric identity

$$\cos(x - y) = (\sin x \sin y + \cos x \cos y) \quad (4-28)$$

which gives

$$Z_z(z) = B'_3 \cos\left(k_z z - k_z \frac{a}{2}\right) \quad (4-29)$$

$$\frac{\partial Z_z(z)}{\partial z} = Z'_z(z) = -B'_3 k_z \sin\left(k_z z - k_z \frac{a}{2}\right). \quad (4-30)$$

Up to this point in region I, the k_z has been left in its general form. Now, k_z needs to be defined so that $\frac{\partial Z_z(z)}{\partial z}$ equals zero whenever $z = \pm \frac{a}{2}$, which leads to

$$k_{z_m} \left(z - \frac{a}{2} \right) = k_{z_m} \left(\pm \frac{a}{2} - \frac{a}{2} \right) = -k_{z_m} a = 0 \quad (4-31)$$

$$0 = m\pi \rightarrow k_{z_m} a = -m\pi \rightarrow k_{z_m} = \frac{-m\pi}{a} \quad (4-32)$$

and therefore, provides the final form of the $Z_z(z)$ equation as

$$Z_z(z) = B'_3 \cos k_{z_m} \left(z - \frac{a}{2} \right) \quad (4-33)$$

Note that axial wavenumber k_z is now k_{z_m} where the 'm' sub-subscript identifies propagating mode for region I in integer intervals, much the way a classic waveguide does. This will be used in the TE_z mode as well.

4.1.4 Deriving TM_z Mode Equations for Region I

Now that the subcomponents to E_z have been defined, they can come together into a summation as given by

$$E_z^I = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \left(A_{nm} \cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \quad (4-34)$$

where A_{nm} is the combined coefficients and $k_z = k_{z_m}$, $k_\rho = k_{\rho_m}$ and the radial wavenumber,

k_{ρ_m} , is derived as $k_{\rho_m} = \sqrt{k^2 - k_{z_m}^2}$. From here, E_z is plugged into the modified FEGWs

given by equations (4-6) through (4-9) to yield

$$E_{\rho_TM}^I = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(A_{nm} \cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho) \right) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} \left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho) \right) \right) \quad (4-35)$$

$$E_{\varphi_TM}^I = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(A_{nm} \cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \quad (4-36)$$

$$H_{\rho_TM}^I = -\frac{\omega \varepsilon}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(A_{nm} \cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \quad (4-37)$$

$$H_{\varphi_TM}^I = -j \omega \varepsilon \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(A_{nm} \cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho) \right) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} \left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho) \right) \right) \quad (4-38)$$

4.2 TE_z Mode Equations for Region I

The TE_z mode will follow the same approach as with the TM_z mode starting with rewriting the FEGWs as

$$E_\rho = \frac{-j}{k_\rho^2} \left[\omega\mu \frac{\partial H_z}{\partial \varphi} \right] \quad (4-39)$$

$$E_\varphi = \frac{-j}{k_\rho^2} \left[-\omega\mu \frac{\partial H_z}{\partial \rho} \right] \quad (4-40)$$

$$H_\rho = \frac{j}{k_\rho^2} \left[-k_z \frac{\partial H_z}{\partial \rho} \right] \quad (4-41)$$

$$H_\varphi = \frac{-j}{k_\rho^2} \left[k_z \frac{\partial H_z}{\partial \varphi} \right] \quad (4-42)$$

by substituting in $E_z=0$.

In the case of the TM_z mode, the FEGWs were in terms of E_z . For the TE_z case, they're in terms of H_z . Just as in the TM_z mode, the Helmholtz vector wave equation will be used, but in the form

$$\nabla^2 H_z + k^2 H_z = 0 \quad (4-43)$$

along with the assumption of $H_z = H_z(\rho, \varphi, z)$, and that it is separable into its constituent components, such that

$$H_z = R_z(\rho)\phi_z(\varphi)Z_z(z). \quad (4-44)$$

Using the same solutions from equations (4-15) through (4-17), H_z can be found to be

$$H_z = \left(C_1 H_n^{(1)}(k_\rho \rho) + D_1 H_n^{(2)}(k_\rho \rho) \right) (C_2 e^{-jn\varphi} + D_2 e^{jn\varphi}) (A_3 \cos k_z z + B_3 \sin k_z z). \quad (4-45)$$

4.2.1 Deriving $R_z(\rho)$ of H_z in Region I

Now, the next step is to reduce each H_z subcomponents starting with $R_z(\rho)$. This approach is similar to the approach taking for E_z . However, a boundary condition for H_z

is not directly available but one can be derived from the relationship $E_\varphi \sim \frac{\partial H_z}{\partial \rho} \sim \frac{\partial R_z(\rho)}{\partial \rho} =$

0 at the boundary $\rho=\rho_1$, which is given by

$$\frac{\partial R_z(\rho)}{\partial \rho} = C_1 \left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho) \right) + D_1 \left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho) \right) = 0. \quad (4-46)$$

This equation can be rearranged to become

$$D_1 = -C_1 \frac{\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)\right)}{\left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)\right)} \quad (4-47)$$

which can be plugged into $R_z(\rho)$ to give

$$R_z(\rho) = C_1 H_n^{(1)}(k_{\rho_m} \rho) - C_1 \frac{\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)\right)}{\left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)\right)} H_n^{(2)}(k_{\rho_m} \rho) =$$

$$C_1 \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)\right)}{\left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)\right)} H_n^{(2)}(k_{\rho_m} \rho) \right). \quad (4-48)$$

4.2.2 Deriving $\Phi_z(\varphi)$ of H_z in Region I

Deriving $\Phi_z(\varphi)$ H_z follows the same process as E_z . Both terms can be combined within a summation forming

$$\sum_{n=-\infty}^{\infty} B_n e^{jn\varphi}. \quad (4-49)$$

4.2.3 Deriving $Z_z(z)$ of H_z in Region I

The last term for H_z , $Z_z(z)$, will require a boundary condition in order for it to be simplified. $Z_z(z)$ is found to have a relationship with $E_\varphi \sim Z_z(z)$, and E_φ is equal to zero at the boundary where $z = \pm a/2$. This boundary condition will be sufficient to simplify $Z_z(z)$. First, the relationship of $E_\varphi \sim Z_z(z)$ needs to be established by using the definitions of E_ρ from equation (4-39) and

$$H_\varphi = \frac{1}{k_{\rho_m}^2 \rho} \frac{\partial^2 H_z}{\partial \varphi \partial z} \quad (4-50)$$

which is an alternate form of a FEGW as described in [14, p. 202]. E_ρ and H_φ can be related as

$$\frac{\partial E_\rho}{\partial z} = -j\omega\mu H_\varphi \quad (4-51)$$

and therefore $\frac{\partial E_\rho}{\partial z} \sim \frac{\partial H_z}{\partial z}$ and $E_\rho \sim H_z$.

Now $Z_z(z)$, which takes the form of equation (4-17), can be equated to zero at the prescribed boundary condition yielding

$$A_3 \cos k_z z + B_3 \sin k_z z = 0 = \begin{cases} A_3 \cos \left(k_z \frac{a}{2} \right) + B_3 \sin \left(k_z \frac{a}{2} \right) = 0 & , \quad z = \frac{a}{2} \\ A_3 \cos \left(-k_z \frac{a}{2} \right) + B_3 \sin \left(-k_z \frac{a}{2} \right) = 0 & , \quad z = -\frac{a}{2} \end{cases} \quad (4-52)$$

which can now be solved for A_3 in the form

$$A_3 = \frac{-B_3 \sin \left(k_z \frac{a}{2} \right)}{\cos \left(k_z \frac{a}{2} \right)}, z = \frac{a}{2}. \quad (4-53)$$

Plugging A_3 back into $Z_z(z)$ yields

$$Z_z(z) = \frac{-B_3 \sin \left(k_z \frac{a}{2} \right)}{\cos \left(k_z \frac{a}{2} \right)} \cos k_z z + B_3 \sin k_z z = B_3 \left(\sin k_z z - \frac{\sin \left(k_z \frac{a}{2} \right)}{\cos \left(k_z \frac{a}{2} \right)} \cos k_z z \right). \quad (4-54)$$

Since k_z is anticipated to be a constant as was in the derivation for E_z , a new constant

$B'_3 = B_3 / \sin k_z \frac{a}{2}$ can be defined and plugged back into $Z_z(z)$ equation giving

$$Z_z(z) = B'_3 \left(\cos \left(k_z \frac{a}{2} \right) \sin k_z z - \sin \left(k_z \frac{a}{2} \right) \cos k_z z \right). \quad (4-55)$$

The trigonometric identity

$$\sin(x - y) = (\sin x \cos y - \cos x \sin y) \quad (4-56)$$

is then used to simplify the $Z_z(z)$ to give the form

$$Z_z(z) = B'_3 \sin \left(k_z z - k_z \frac{a}{2} \right) = B'_3 \sin k_z \left(z - \frac{a}{2} \right) \quad (4-57)$$

and since $k_z = k_{z_m}$

$$Z_z(z) = B'_3 \sin k_{z_m} \left(z - \frac{a}{2} \right). \quad (4-58)$$

4.2.4 Deriving TE_z Mode Equations for Region I

The subcomponents for H_z have been defined and are combined as

$$H_z^I = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \left(B_{nm} \sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \quad (4-59)$$

within summation form. Just as in the TM_z mode, B_{nm} is the combined coefficients and

$$k_z = k_{z_m}, k_\rho = k_{\rho_m} \text{ and } k_{\rho_m} = \sqrt{k^2 - k_{z_m}^2}.$$

Following the same steps as in the TM_z mode, H_z is plugged into the modified FEGWs given by equations (4-39) through (4-42) to yield

$$E_{\rho_{TE}}^I = \frac{\omega\mu}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(B_{nm} \sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \quad (4-60)$$

$$E_{\varphi_{TE}}^I = j\omega\mu \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(B_{nm} \sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho) \right) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} \left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho) \right) \right) \quad (4-61)$$

$$H_{\rho_{TE}}^I = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(B_{nm} \sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(\left(k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho) \right) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} \left(k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho) \right) \right) \quad (4-62)$$

$$H_{\varphi_{TE}}^I = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{zm}}{k_{\rho m}^2} \left(B_{nm} \sin k_{zm} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho m} \rho) - \frac{k_{\rho m} H_{n-1}^{(1)}(k_{\rho m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho m} \rho_1)}{k_{\rho m} H_{n-1}^{(2)}(k_{\rho m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho m} \rho_1)} H_n^{(2)}(k_{\rho m} \rho) \right). \quad (4-63)$$

CHAPTER 5 REGION II – SCATTERED FIELD EQUATIONS

This chapter will focus on the derivation of the scattered field in region II. This is the same region in which the incident fields were described in Chapter 3. By the end of this chapter, all the fields in region II would will be covered.

According to [12, p. 615], a perfectly smooth cylinder that is infinitely long and a PEC does not depolarize an incident wave. Balanis continues on to describe that deviations from this can cause depolarization of the incident wave [12, p. 615]. Though not explicitly stated by Balanis, his statement can be interpreted to be applied to that of the periodic corrugated cylinder which would depolarize an incident plane wave. Therefore, as stated in section 2.3 , a hybrid mode of TM_z and TE_z can exist for the periodic corrugated cylinder and will be examined as such. The field equations for the TM_z and TE_z modes will be derived separately, but through the principle of superposition will be combined in Chapter 5 when finding solutions for the fields.

When deriving the field equations for the scattered field, the FEGWs presented in Chapter 4, equations (4-1) through (4-4), will be made much use of. Also from Chapter 4, deriving the E_z and H_z scattered fields will use the same Helmholtz equation representation from (4-10) and (4-43) respectively, as well as the same coordinate constituent separable equations from (4-11) and (4-44) respectively. Use of the known solutions for the Helmholtz equation described in equations (4-12) through (4-14) will also be made in this chapter.

5.1 Equations for the TM_z Mode Scattered Field of Region II

The steps to derive the equations representing the TM_z mode of the scattered field in region II will be the same as that for the TM_z mode in region I. This starts with choosing the appropriate field representation from equations (4-12) through (4-14) based on geometry and expected behavior in order to describe E_z. Since there are no restrictive boundaries in region II, the traveling wave representation is chosen for each constituent and replaced into (4-11) to give

$$E_z = \left(C_1 H_n^{(1)}(k_\rho \rho) + D_1 H_n^{(2)}(k_\rho \rho) \right) (C_2 e^{-jn\varphi} + D_2 e^{+jn\varphi}) (C_3 e^{-jk_z z} + C_3 e^{jk_z z}). \quad (5-1)$$

Now, the first and second term of E_z, which make up R_z(ρ) represent inward and outward traveling waves respectively. Since at the boundary of region II, whether with the conductive surface or with region I, there is no scattered field expected, the inward traveling wave portion (the first term) can be eliminated leaving

$$E_z = D_1 H_n^{(2)}(k_\rho \rho) (C_2 e^{-jn\varphi} + D_2 e^{+jn\varphi}) (C_3 e^{-jk_z z} + C_3 e^{jk_z z}). \quad (5-2)$$

This equation can be further simplified by bringing it into summation terms as was done in Chapter 4 yielding

$$E_{zII}^S = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} C_{nl} e^{-jk_{z_l} z} H_n^{(2)}(k_{\rho_l} \rho). \quad (5-3)$$

Note that axial wavenumber k_z has been replaced by k_{z_l} and radial wavenumber k_ρ has been replaced by k_{ρ_l} , where $k_{\rho_l} = \sqrt{k^2 - k_{z_l}^2}$. Here, the sub-subscript 'l' identifies the propagating mode for region II in the same way 'm' is for region I. To understand the relationship of the propagating mode with the geometry, a derivation of k_{z_l} , is required. This is due to the fact that a propagating wave interfacing with a structure, in this case the scattered field with the periodic corrugated cylinder, takes on the symmetry of said structure as depicted in Figure 5-1. This k_{z_l} is known as the Floquet harmonic or Floquet

wavenumber [9, p. 265] or a Bloch wavenumber [15] because of the non-uniqueness and ability to represent a periodic medium.

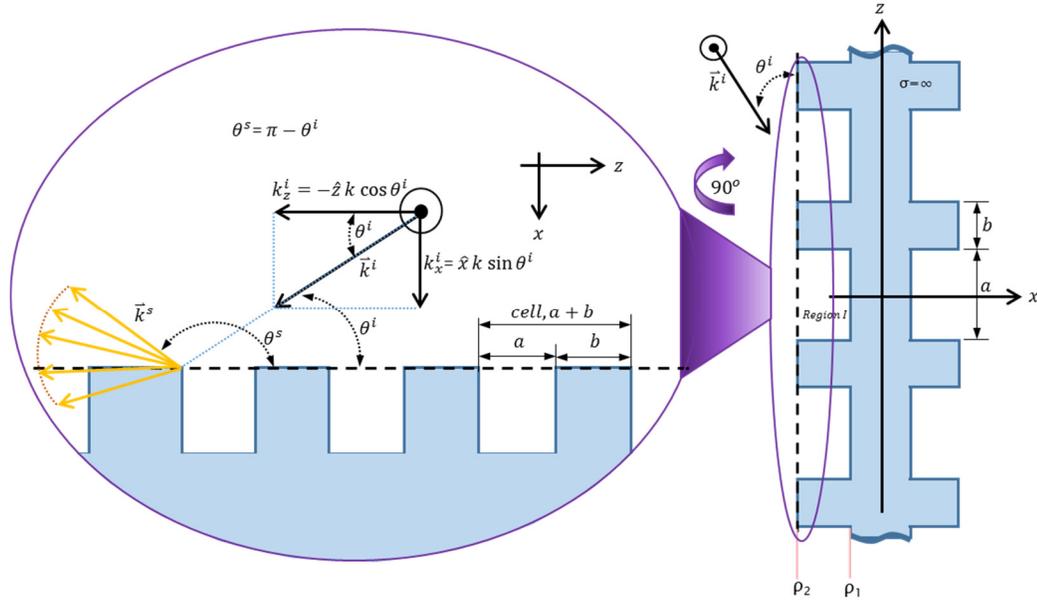


Figure 5-1 A depiction of the vector decomposition of the wavenumber in region II

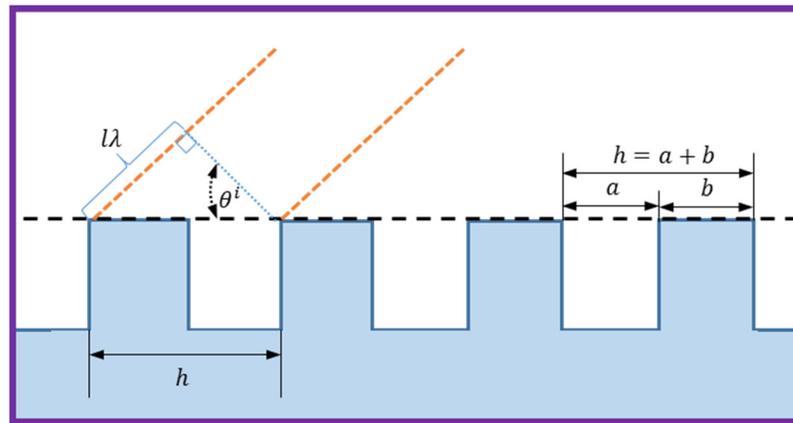


Figure 5-2 A depiction of constructive interference for a propagating wave along a periodic surface

First, for wave modes to exist, a constructive interference relationship needs to be established along the path of propagation. This is how wave modes are established within waveguides and periodic structures. It can be seen from Figure 5-2 that an integer

multiple ‘1’ to the wavelength ‘ λ ’ would provide a description of the propagating modes along the prescribed surface where constructive interface would occur. Also, the relationship

$$l\lambda = (a + b) \sin \theta^i \quad (5-4)$$

is established. The relationship for the scattered field wave vector

$$\vec{k}^s = -\hat{z} k \cos \theta^s + \hat{x} k \sin \theta^s \quad (5-5)$$

is established from Figure 5-1 where the magnitude of \vec{k}^s , which will be referred to as

k_{z_l} , the axial wavenumber in region II, is

$$k_{z_l} = k \cos \theta^i + k \sin \theta^i. \quad (5-6)$$

when substituting in the relationship of $\theta^s = \pi - \theta^i$ as per [12, p. 615]. Substituting in the

definition $k = \frac{2\pi}{\lambda}$ for the second term yields

$$k_{z_l} = k \cos \theta^i + \frac{2\pi}{\lambda} \sin \theta^i \quad (5-7)$$

which can further be reduced by using equation (5-4) to give

$$\frac{l\lambda}{(a + b)} = \sin \theta^i \quad (5-8)$$

$$k_{z_l} = k \cos \theta^i + \frac{2\pi}{\lambda} \frac{l\lambda}{(a + b)} = k \cos \theta^i + \frac{2\pi l}{(a + b)} \quad (5-9)$$

which completes the derivation for k_{z_l} . This also completes the definition for $E_{z_{II}}^s$.

Next, the remaining TM_z mode scattered field equations are derived. This is done by substituting $E_{z_{II}}^s$ into equations (4-6) through (4-9) to produce

$$E_{\rho_{TMII}}^s = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho_l}^2} C_{nl} e^{-jk_{z_l}z} \left(k_{\rho_l} H_{n-1}^{(2)}(k_{\rho_l}\rho) - \frac{nH_n^{(2)}(k_{\rho_l}\rho)}{\rho} \right) \quad (5-10)$$

$$E_{\varphi_{TMII}}^s = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho_l}^2} C_{nl} e^{-jk_{z_l}z} H_n^{(2)}(k_{\rho_l}\rho) \quad (5-11)$$

$$H_{\rho_{TMII}}^s = -\frac{\omega\epsilon}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho_l}^2} C_{nl} e^{-jk_{z_l}z} H_n^{(2)}(k_{\rho_l}\rho) \quad (5-12)$$

$$H_{\varphi_{TM}^{II}}^S = -j\omega\varepsilon \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} C_{nl} e^{-jk_{z l} z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{n H_n^{(2)}(k_{\rho l} \rho)}{\rho} \right). \quad (5-13)$$

5.2 Equations for the TE_z Mode Scattered Field of Region II

For the TE_z mode, H_z is derived much the same way as was in the TE_z mode in region I. Once applying the same assumptions from the geometry and expected field behavior described in section 5.1 for the TM_z mode case, onto the equations (4-12) through (4-14) and to equation (4-44), H_z is defined as

$$H_{zII}^S = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} D_{nl} e^{-jk_{z l} z} H_n^{(2)}(k_{\rho l} \rho). \quad (5-14)$$

where D_{nl} represents the combined coefficients and k_{z l} and k_{ρ l} are the axial and radial wavenumbers defined in section 5.1 respectively.

Now with a fully defined H_{zII}^S, the remaining equations can be found by plugging H_{zII}^S into equations (4-39) through (4-42) to yield

$$E_{\rho_{TE}^{II}}^S = -j\omega\mu * j \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} D_{nl} e^{-jk_{z l} z} H_n^{(2)}(k_{\rho l} \rho) \quad (5-15)$$

$$E_{\varphi_{TE}^{II}}^S = j\omega\mu \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} D_{nl} e^{-jk_{z l} z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{n H_n^{(2)}(k_{\rho l} \rho)}{\rho} \right) \quad (5-16)$$

$$H_{\rho_{TE}^{II}}^S = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z l}}{k_{\rho l}^2} D_{nl} e^{-jk_{z l} z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{n H_n^{(2)}(k_{\rho l} \rho)}{\rho} \right) \quad (5-17)$$

$$H_{\varphi_{TE}^{II}}^S = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z l}}{k_{\rho l}^2} D_{nl} e^{-jk_{z l} z} H_n^{(2)}(k_{\rho l} \rho). \quad (5-18)$$

CHAPTER 6 BOUNDARY CONDITIONS & POINT MATCHING METHOD

At this point, the equations for region I and region II have been defined. However, the equations for region I and the scattered field equations for region II have unknown coefficients that need to be solved for in order to have a complete representation, and therefore to be able to calculate and predict the scattered field. In order to achieve this, boundary conditions need to be established to provide equation sets that allow for algebraic solving of the unknown coefficients. The equation relationships are established by point matching, equating points from different equations, that establishes an equal number of point matches to unknowns.

6.1 General Boundary Conditions

There are two main boundary regions that are utilized in this paper for point matching, as can be observed from Figure 6-1, which are boundary ‘a’ and boundary ‘b’.

Boundary ‘a’:

- Boundary between region I and II at $\rho = \rho_2$ for a z range of $\frac{-a}{2} \leq z \leq \frac{a}{2}$.
- The available matching points, $p_j(\rho, \varphi, z)$, of a quantity ‘j’ are: $\rho = \rho_2$, $\frac{-a}{2} \leq z \leq \frac{a}{2}$ and $0 \leq \varphi \leq 2\pi$.
- Tangential electric fields from region II, E_z^{II} and E_φ^{II} , are equal to tangential electric fields from region I, E_z^I and E_φ^I , hence $E_z^{II}=E_z^I$ and $E_\varphi^{II}=E_\varphi^I$ [16, p. 178].
- Tangential magnetic fields from region II, H_z^{II} and H_φ^{II} , are equal to tangential magnetic fields from region I, H_z^I and H_φ^I , hence $H_z^{II}=H_z^I$ and $H_\varphi^{II}=H_\varphi^I$ when the

conductivity is finite, hence, not a PEC which is the case at this boundary [16, p. 234].

- Used to solve for the unknown expansion coefficients A_{nm} and B_{nm} from region I.
- Used to solve for the unknown expansion coefficients C_{nl} and D_{nl} from region II, which are distinct for each boundary, therefore these will have superscript of (a) to identify them: $C_{nl}^{(a)}$ and $D_{nl}^{(a)}$.

Boundary ‘b’:

- Boundary between region II and outer conducting surface of corrugated cylinder at $\rho = \rho_2$ for a z range of $\frac{a}{2} \leq z \leq \frac{a}{2} + b$.
- The available matching points, $p_j(\rho, \varphi, z)$, of a quantity ‘j’ are: $\rho = \rho_2, \frac{a}{2} \leq z \leq \frac{a}{2} + b$ and $0 \leq \varphi \leq 2\pi$.
- Tangential electric fields from region II are equal to zero based on the Dirichlet boundary condition [9, pp. 97-100]: $E_z^{II} = 0$ and $E_\varphi^{II} = 0$.
- Used to solve for the unknown expansion coefficients C_{nl} and D_{nl} from region II, which are distinct and will have superscript (b) to identify them, $C_{nl}^{(b)}$ and $D_{nl}^{(b)}$.

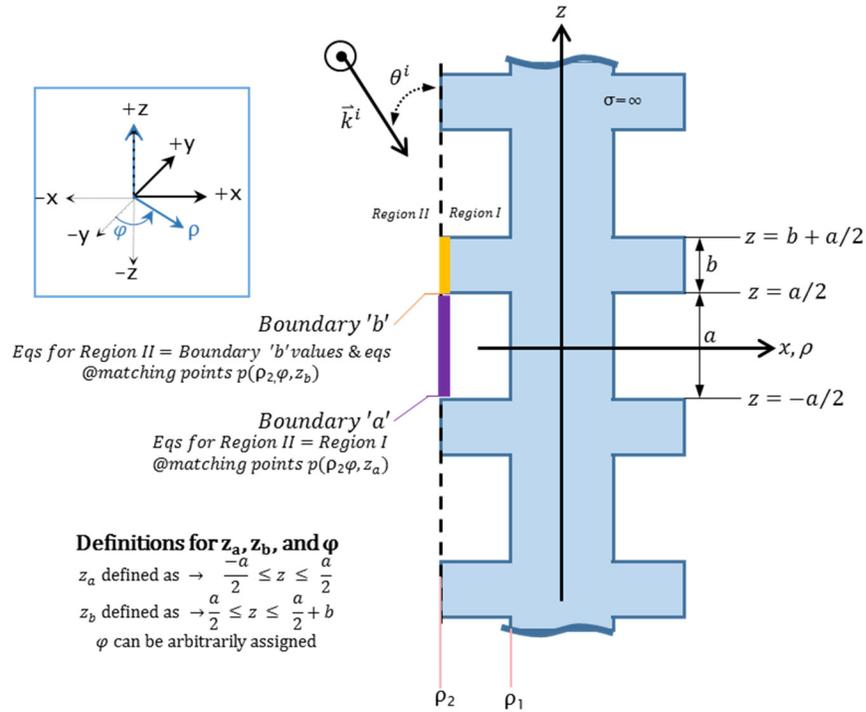


Figure 6-1 A depiction for the general boundary conditions utilized to solve for the unknown coefficients

6.2 Matrix Form of Field Equations

In order to effectively apply the boundary conditions and to solve for the unknown expansion coefficients, the field equations described in Chapter 3, Chapter 4 and Chapter 5 will be represented in matrix form. This will aid in the algebraic manipulation and solving of the coefficients.

There are a few things to note about the matrix form and indices. The expansion coefficients of each region need to have the same shape as each other for point matching, therefore the $n \times m$ size matrices of region I need to match the $n \times l$ matrices of region II. This is accomplished by making “n” of each region equal to each other and having “m” of region I equal to “l” of region II.

The matrices that contain a subscript “j” indicate that there are z’s and φ ’s referenced in them, where ρ is always ρ_2 for point matches. Each “j” is a matching point,

which is provided by z 's and φ 's variation on the specified boundary with a fixed ρ_2 and z range indicated. The number of matching points, which is the number of “j” points, is equal to $n * m$ or $n * l$, thus there's a matching point for every expanded “n” and “m” or “n” and “l”. Also, the number of equation matches equals the number of expansion coefficients. The number of matching points times the number of equation matches equals the total number of unknown expanded coefficients which provides a complete system of equations.

In order to separate the coefficients from the rest of the terms for each equation, the matrices of the unknown expansion coefficients are flattened into an array of a single column with $n * m$ or $n * l$ rows and the remainder of the term can stay in a matrix form of “j” rows and $n * m$ or $n * l$ columns. When multiplied back together, it produces the summation equation. The incident fields are also “j” rows, but of a single column of which each entry is a full summation solution.

6.2.1 Matrix form of Region I Equations

The following are the matrix form of the subcomponents of the region I equations described in Chapter 4. The equations listed below capture the fields E_z^I , H_z^I , E_φ^I , H_φ^I , E_ρ^I and H_ρ^I in matrix form. For each equation in the list, the corresponding matrix form in which it's used is provided. Also, the equation's substituted form is identified and located within the matrix form through the use of highlighting and bolding the font.

$$[h_{nmj}] = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \left(\cos k_{zm} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho m} \rho) - \frac{H_n^{(1)}(k_{\rho m} \rho_1)}{H_n^{(2)}(k_{\rho m} \rho_1)} H_n^{(2)}(k_{\rho m} \rho) \right) \quad (6-1)$$

\leftarrow From $E_z^I = \mathbf{[h_{nmj}] [A_{nm}]}$

$$[i_{nmj}] = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \left(\sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \leftarrow \text{From } H_z^I = [i_{nmj}][B_{nm}] \quad (6-2)$$

$$[k_{nmj}] = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(\cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \leftarrow \text{From } E_\varphi^I = [k_{nmj}][A_{nm}] + [l_{nmj}][B_{nm}] \quad (6-3)$$

$$[l_{nmj}] = j\omega\mu \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(\sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left((k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho)) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} (k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho)) \right) \leftarrow \text{From } E_\varphi^I = [k_{nmj}][A_{nm}] + [l_{nmj}][B_{nm}] \quad (6-4)$$

$$[o_{nmj}] = -j\omega\varepsilon \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(\cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left((k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho)) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} (k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho)) \right) \leftarrow \text{From } H_\varphi^I = [o_{nmj}][A_{nm}] + [p_{nmj}][B_{nm}] \quad (6-5)$$

$$[p_{nmj}] = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(\sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \leftarrow \text{From } H_\varphi^I = [o_{nmj}][A_{nm}] + [p_{nmj}][B_{nm}] \quad (6-6)$$

$$[r_{nmj}] = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho_m}^2} \left(\cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left((k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho_m} \rho)) - \frac{H_n^{(1)}(k_{\rho_m} \rho_1)}{H_n^{(2)}(k_{\rho_m} \rho_1)} (k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho_m} \rho)) \right) \leftarrow \text{From } E_\rho^I = [r_{nmj}][A_{nm}] + [s_{nmj}][B_{nm}] \quad (6-7)$$

$$[s_{nmj}] = \frac{\omega\mu}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho_m}^2} \left(\sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho_m} \rho) - \frac{k_{\rho_m} H_{n-1}^{(1)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho_m} \rho_1)}{k_{\rho_m} H_{n-1}^{(2)}(k_{\rho_m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho_m} \rho_1)} H_n^{(2)}(k_{\rho_m} \rho) \right) \leftarrow \text{From } E_\rho^I = [r_{nmj}][A_{nm}] + [s_{nmj}][B_{nm}] \quad (6-8)$$

$$[t_{nmj}] = -\frac{\omega\varepsilon}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{1}{k_{\rho m}^2} \left(\cos k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(H_n^{(1)}(k_{\rho m} \rho) - \frac{H_n^{(1)}(k_{\rho m} \rho_1)}{H_n^{(2)}(k_{\rho m} \rho_1)} H_n^{(2)}(k_{\rho m} \rho) \right) \leftarrow \text{From } H_{\rho}^I = [t_{nmj}] [A_{nm}] + [u_{nmj}] [B_{nm}] \quad (6-9)$$

$$[u_{nmj}] = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{m=-\infty}^{\infty} \frac{k_{z_m}}{k_{\rho m}^2} \left(\sin k_{z_m} \left(z - \frac{a}{2} \right) \right) \left(\left(k_{\rho m} H_{n-1}^{(1)}(k_{\rho m} \rho) - \frac{n}{\rho} H_n^{(1)}(k_{\rho m} \rho) \right) - \frac{k_{\rho m} H_{n-1}^{(1)}(k_{\rho m} \rho_1) - \frac{n}{\rho_1} H_n^{(1)}(k_{\rho m} \rho_1)}{k_{\rho m} H_{n-1}^{(2)}(k_{\rho m} \rho_1) - \frac{n}{\rho_1} H_n^{(2)}(k_{\rho m} \rho_1)} \left(k_{\rho m} H_{n-1}^{(2)}(k_{\rho m} \rho) - \frac{n}{\rho} H_n^{(2)}(k_{\rho m} \rho) \right) \right) \leftarrow \text{From } H_{\rho}^I = [t_{nmj}] [A_{nm}] + [u_{nmj}] [B_{nm}] \quad (6-10)$$

The TM_z mode region I field expansion coefficient is represented by $[A_{nm}]$ and the TE_z mode region I field expansion coefficient is represented by $[B_{nm}]$. The remaining are region I field components of the respective mode to the coefficient it's a product with.

6.2.2 Matrix form of Region II Equations

The following are the matrix form of the subcomponents of the region II equations described in Chapter 3 and Chapter 5. This includes the superposition of all the region II fields within the same coordinate axis, including TM_z and TE_z modes for both the scattered and incident field. Hence, the total field for each axis is summarized as

$$E_z^{II} = E_{z^{II}}^i + E_{z_{TM}^{II}}^s \quad (6-11)$$

$$E_{\rho}^{II} = E_{\rho^{II}}^i + E_{\rho_{TM}^{II}}^s + E_{\rho_{TE}^{II}}^s \quad (6-12)$$

$$E_{\varphi}^{II} = E_{\varphi^{II}}^i + E_{\varphi_{TM}^{II}}^s + E_{\varphi_{TE}^{II}}^s \quad (6-13)$$

$$H_z^{II} = H_{z^{II}}^i + H_{z_{TE}^{II}}^s \quad (6-14)$$

$$H_{\rho}^{II} = H_{\rho^{II}}^i + H_{\rho_{TM}^{II}}^s + H_{\rho_{TE}^{II}}^s \quad (6-15)$$

$$H_{\varphi}^{II} = H_{\varphi^{II}}^i + H_{\varphi_{TM}^{II}}^s + H_{\varphi_{TE}^{II}}^s \quad (6-16)$$

Below are the field components of E_z^{II} , H_z^{II} , E_{φ}^{II} , H_{φ}^{II} , E_{ρ}^{II} and H_{ρ}^{II} in matrix form. Just as in section 6.2.1, the equation's substituted form is identified and located within the matrix form through the use of highlighting and bolding the font.

$$[b_{nj}] = E_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } E_z^{II} = [\mathbf{b}_{nj}] + [a_{nl}][C_{nl}] \quad (6-17)$$

$$[a_{nlj}] = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } E_z^{II} = [b_{nj}] + [\mathbf{a}_{nlj}][C_{nl}] \quad (6-18)$$

$$[f_{nj}] = H_0 \sin \theta^i e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } H_z^{II} = [\mathbf{f}_{nj}] + [g_{nl}][D_{nl}] \quad (6-19)$$

$$[g_{nlj}] = \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } H_z^{II} = [f_{nj}] + [\mathbf{g}_{nlj}][D_{nl}] \quad (6-20)$$

$$[d_{nj}] = [-E_0 \sin \varphi \cos \theta^i + ZH_0 \cos \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } E_{\varphi}^{II} = [\mathbf{d}_{nj}] + ([c_{nlj}][C_{nl}] + [e_{nlj}][D_{nl}]) \quad (6-21)$$

$$[c_{nlj}] = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho l}^2} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } E_{\varphi}^{II} = [d_{nj}] + ([\mathbf{c}_{nlj}][C_{nl}] + [e_{nlj}][D_{nl}]) \quad (6-22)$$

$$[e_{nlj}] = j\omega\mu \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} e^{-jkz_l z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{nH_n^{(2)}(k_{\rho l} \rho)}{\rho} \right) \leftarrow \text{From } E_{\varphi}^{II} = [d_{nj}] + ([c_{nlj}][C_{nl}] + [\mathbf{e}_{nlj}][D_{nl}]) \quad (6-23)$$

$$[m_{nj}] = \left[-\frac{E_0}{Z} \cos \varphi - H_0 \sin \varphi \cos \theta^i \right] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } H_{\varphi}^{II} = [\mathbf{m}_{nj}] + ([n_{nlj}][C_{nl}] + [q_{nlj}][D_{nl}]) \quad (6-24)$$

$$[n_{nlj}] = -j\omega\varepsilon \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} e^{-jkz_l z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{nH_n^{(2)}(k_{\rho l} \rho)}{\rho} \right) \leftarrow \text{From } H_{\varphi}^{II} = [m_{nj}] + ([\mathbf{n}_{nlj}][C_{nl}] + [q_{nlj}][D_{nl}]) \quad (6-25)$$

$$[q_{nlj}] = \frac{1}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho l}^2} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } H_{\varphi}^{II} = [m_{nj}] + ([n_{nlj}][C_{nl}] + [\mathbf{q}_{nlj}][D_{nl}]) \quad (6-26)$$

$$[\gamma_{nj}] = [E_0 \cos \varphi \cos \theta^i + ZH_0 \sin \varphi] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } E_{\rho}^{II} = [\mathbf{\gamma}_{nj}] + ([v_{nlj}][C_{nl}] + [w_{nlj}][D_{nl}]) \quad (6-27)$$

$$[v_{nlj}] = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho l}^2} e^{-jkz_l z} \left(k_{\rho l} H_{n-1}^{(2)}(k_{\rho l} \rho) - \frac{nH_n^{(2)}(k_{\rho l} \rho)}{\rho} \right) \leftarrow \text{From } E_{\rho}^{II} = [\gamma_{nj}] + ([\mathbf{v}_{nlj}][C_{nl}] + [w_{nlj}][D_{nl}]) \quad (6-28)$$

$$[w_{nlj}] = \frac{\omega\mu}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } E_{\rho}^{II} = [\gamma_{nj}] + ([v_{nlj}][C_{nl}] + [\mathbf{w}_{nlj}][D_{nl}]) \quad (6-29)$$

$$[\delta_{nj}] = \left[-\frac{E_0}{Z} \sin \varphi + H_0 \cos \varphi \cos \theta^i \right] e^{jkz \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta^i) e^{jn\varphi} \leftarrow \text{From } H_{\rho}^{II} = [\mathbf{\delta}_{nj}] + ([x_{nlj}][C_{nl}] + [y_{nlj}][D_{nl}]) \quad (6-30)$$

$$[x_{nlj}] = -\frac{\omega\varepsilon}{\rho} \sum_{n=-\infty}^{\infty} n e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{1}{k_{\rho l}^2} e^{-jkz_l z} H_n^{(2)}(k_{\rho l} \rho) \leftarrow \text{From } H_{\rho}^{II} = [\delta_{nj}] + ([\mathbf{x}_{nlj}][C_{nl}] + [y_{nlj}][D_{nl}]) \quad (6-31)$$

$$[y_{nlj}] = -j \sum_{n=-\infty}^{\infty} e^{jn\varphi} \sum_{l=-\infty}^{\infty} \frac{k_{z_l}}{k_{\rho_l}^2} e^{-jk_{z_l}z} \left(k_{\rho_l} H_{n-1}^{(2)}(k_{\rho_l}\rho) - \frac{nH_n^{(2)}(k_{\rho_l}\rho)}{\rho} \right) \leftarrow \text{From } H_{\rho}^{II} = \quad (6-32)$$

$$[\delta_{nj}] + ([x_{nlj}][C_{nl}] + [y_{nlj}][D_{nl}])$$

The components $[b_{nj}]$, $[f_{nj}]$, $[d_{nj}]$, $[m_{nj}]$, $[y_{nj}]$ and $[\delta_{nj}]$ represent the incident field of the corresponding cylindrical orientation with both TM_z and TE_z mode combined. The TM_z mode scattered field expansion coefficient is represented by $[C_{nl}]$ and the TE_z mode scattered field expansion coefficient is represented by $[D_{nl}]$. The remaining are scattered field components of the respective mode to the coefficient it's a product with.

6.2.3 Matrix Equation Matches for Point Matching

There are 6 unknown expansion coefficients, each of which expand out to either $n * m$ or $n * l$ quantities of unknowns. This means that there needs to be at least 6 matrix equation matches in order to solve for the unknowns. Based on the boundary conditions discussed in section 6.1 the following 6 equations will provide a system of equations to solve for the unknowns.

For boundary 'a':

$$[E_z^I] = [E_z^{II(a)}] \rightarrow [h_{nmj}][A_{nm}] = [b_{nj}] + [a_{nlj}][C_{nl}^{(a)}] \quad (6-33)$$

$$[E_{\varphi}^I] = [E_{\varphi}^{II(b)}] \rightarrow [k_{nmj}][A_{nm}] + [l_{nmj}][B_{nm}] = [d_{nj}] + ([c_{nlj}][C_{nl}^{(a)}] + [e_{nlj}][D_{nl}^{(a)}]) \quad (6-34)$$

$$[H_z^I] = [H_z^{II(a)}] \rightarrow [i_{nmj}][B_{nm}] = [f_{nj}] + [g_{nlj}][D_{nl}^{(a)}] \quad (6-35)$$

$$[H_{\varphi}^I] = [H_{\varphi}^{II(a)}] \rightarrow [o_{nmj}][A_{nm}] + [p_{nmj}][B_{nm}] = [m_{nj}] + ([n_{nlj}][C_{nl}^{(a)}] + [q_{nlj}][D_{nl}^{(a)}]) \quad (6-36)$$

For boundary 'b':

$$0 = [E_z^{II(b)}] \rightarrow 0 = [b_{nj}] + [a_{nlj}][C_{nl}^{(b)}] \quad (6-37)$$

$$0 = [E_{\varphi}^{II(b)}] \rightarrow 0 = [d_{nj}] + ([c_{nlj}][C_{nl}^{(b)}] + [e_{nlj}][D_{nl}^{(b)}]) \quad (6-38)$$

A partially expanded matrix form provides a good aid of the matrix form which is represented here as well. Subscripts within the matrices will be further observable and the

matrix shape made obvious. Though, a few notes on the sub-subscripts need to be made.

A sub-subscript of 1 on the subscript “n”, “m”, and “l” signifies the first increment of that index. A sub-subscript of “n_max”, “m_max”, or “l_max” signifies the last increment of that index, which are on “n”, “m”, or “l” respectively.

For boundary ‘a’:

$$\begin{aligned}
 [E_z^l] = [E_z^{II(a)}] &\rightarrow \begin{bmatrix} h_{n_1 m_1 j_1} & \cdots & h_{n_{n_{\max}} m_{m_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ h_{n_1 m_1 j_{j_{\max}}} & \cdots & h_{n_{n_{\max}} m_{m_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} A_{n_1 m_1} \\ \vdots \\ A_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
 &= \begin{bmatrix} b_{n j_1} \\ \vdots \\ b_{n j_{j_{\max}}} \end{bmatrix} + \begin{bmatrix} a_{j_1 n_1 l_1} & \cdots & a_{j_1 n_{n_{\max}} l_{l_{\max}}} \\ \vdots & \ddots & \vdots \\ a_{n_1 l_1 j_{j_{\max}}} & \cdots & a_{n_{n_{\max}} l_{l_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} C_{n_1 l_1}^{(b)} \\ \vdots \\ C_{n_{n_{\max}} l_{l_{\max}}}^{(b)} \end{bmatrix}
 \end{aligned} \tag{6-39}$$

$$\begin{aligned}
 [E_\varphi^l] = [E_\varphi^{II(a)}] &\rightarrow \begin{bmatrix} k_{n_1 m_1 j_1} & \cdots & k_{j_1 n_{n_{\max}} m_{m_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ k_{n_1 m_1 j_{j_{\max}}} & \cdots & k_{n_{n_{\max}} m_{m_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} A_{n_1 m_1} \\ \vdots \\ A_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
 &+ \begin{bmatrix} l_{n_1 m_1 j_1} & \cdots & l_{n_{n_{\max}} m_{m_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ l_{n_1 m_1 j_{j_{\max}}} & \cdots & l_{n_{n_{\max}} m_{m_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} B_{n_1 m_1} \\ \vdots \\ B_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
 &= \begin{bmatrix} d_{n j_1} \\ \vdots \\ d_{n j_{j_{\max}}} \end{bmatrix} \\
 &+ \left(\begin{bmatrix} c_{n_1 l_1 j_1} & \cdots & c_{n_{n_{\max}} l_{l_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ c_{n_1 l_1 j_{j_{\max}}} & \cdots & c_{n_{n_{\max}} l_{l_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} C_{n_1 l_1}^{(a)} \\ \vdots \\ C_{n_{n_{\max}} l_{l_{\max}}}^{(a)} \end{bmatrix} \right. \\
 &\left. + \begin{bmatrix} e_{n_1 l_1 j_1} & \cdots & e_{n_{n_{\max}} l_{l_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ e_{n_1 l_1 j_{j_{\max}}} & \cdots & e_{n_{n_{\max}} l_{l_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} D_{n_1 l_1}^{(a)} \\ \vdots \\ D_{n_{n_{\max}} l_{l_{\max}}}^{(a)} \end{bmatrix} \right)
 \end{aligned} \tag{6-40}$$

$$\begin{aligned}
 [H_z^l] = [H_z^{II(a)}] &\rightarrow \begin{bmatrix} i_{n_1 m_1 j_1} & \cdots & i_{n_{n_{\max}} m_{m_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ i_{n_1 m_1 j_{j_{\max}}} & \cdots & i_{n_{n_{\max}} m_{m_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} B_{n_1 m_1} \\ \vdots \\ B_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
 &= \begin{bmatrix} f_{n j_1} \\ \vdots \\ f_{n j_{j_{\max}}} \end{bmatrix} + \begin{bmatrix} g_{j_1 n_1 l_1} & \cdots & g_{n_{n_{\max}} l_{l_{\max}} j_1} \\ \vdots & \ddots & \vdots \\ g_{n_1 l_1 j_{j_{\max}}} & \cdots & g_{n_{n_{\max}} l_{l_{\max}} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} D_{n_1 l_1}^{(a)} \\ \vdots \\ D_{n_{n_{\max}} l_{l_{\max}}}^{(a)} \end{bmatrix}
 \end{aligned} \tag{6-41}$$

$$\begin{aligned}
[H_\phi^a] = [H_\phi^{II(a)}] &\rightarrow \begin{bmatrix} o_{n_1 l_1 j_1} & \cdots & o_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ o_{n_1 l_1 j_{j_{\max}}} & \cdots & o_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} A_{n_1 m_1} \\ \vdots \\ A_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
&+ \begin{bmatrix} p_{n_1 l_1 j_1} & \cdots & p_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ p_{n_1 l_1 j_{j_{\max}}} & \cdots & p_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} B_{n_1 m_1} \\ \vdots \\ B_{n_{n_{\max}} m_{m_{\max}}} \end{bmatrix} \\
&= \begin{bmatrix} m_{n_{j_1}} \\ \vdots \\ m_{n_{j_{j_{\max}}}} \end{bmatrix} \\
&+ \left(\begin{bmatrix} n_{n_1 l_1 j_1} & \cdots & n_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ n_{n_1 l_1 j_{j_{\max}}} & \cdots & n_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} C_{n_1 l_1}^{(a)} \\ \vdots \\ C_{n_{n_{\max}} l_{\max}}^{(a)} \end{bmatrix} \right. \\
&+ \left. \begin{bmatrix} q_{n_1 l_1 j_1} & \cdots & q_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ q_{n_1 l_1 j_{j_{\max}}} & \cdots & q_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} D_{n_1 l_1}^{(a)} \\ \vdots \\ D_{n_{n_{\max}} l_{\max}}^{(a)} \end{bmatrix} \right)
\end{aligned} \tag{6-42}$$

For boundary ‘b’:

$$0 = [E_z^{II(b)}] \rightarrow 0 = \begin{bmatrix} b_{n_{j_1}} \\ \vdots \\ b_{n_{j_{j_{\max}}}} \end{bmatrix} + \begin{bmatrix} a_{n_1 l_1 j_1} & \cdots & a_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ a_{n_1 l_1 j_{j_{\max}}} & \cdots & a_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} C_{n_1 l_1}^{(b)} \\ \vdots \\ C_{n_{n_{\max}} l_{\max}}^{(b)} \end{bmatrix} \tag{6-43}$$

$$\begin{aligned}
0 = [E_\phi^{II(b)}] &\rightarrow 0 \\
&= \begin{bmatrix} d_{n_{j_1}} \\ \vdots \\ d_{n_{j_{j_{\max}}}} \end{bmatrix} \\
&+ \left(\begin{bmatrix} c_{n_1 l_1 j_1} & \cdots & c_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ c_{n_1 l_1 j_{j_{\max}}} & \cdots & c_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} C_{n_1 l_1}^{(b)} \\ \vdots \\ C_{n_{n_{\max}} l_{\max}}^{(b)} \end{bmatrix} \right. \\
&+ \left. \begin{bmatrix} e_{n_1 l_1 j_1} & \cdots & e_{n_{n_{\max}} l_{\max} j_1} \\ \vdots & \ddots & \vdots \\ e_{n_1 l_1 j_{j_{\max}}} & \cdots & e_{n_{n_{\max}} l_{\max} j_{j_{\max}}} \end{bmatrix} \begin{bmatrix} D_{n_1 l_1}^{(b)} \\ \vdots \\ D_{n_{n_{\max}} l_{\max}}^{(b)} \end{bmatrix} \right)
\end{aligned} \tag{6-44}$$

6.3 Summation Truncation

It’s also important to note that the summations for all the equations, and therefore the matrices, need to be truncated from an infinite to a finite length indices. This is required prior to numerical computation. Truncation can reduce accuracy, so it follows that smaller truncated values can be less accurate than when truncated to higher values. However, it is a fair trade off between computer computational power and available processing time versus accuracy. That’s due to the fact that the higher “n”, “m”, and “l”

indices represent higher orders and wave numbers of waves that either don't propagate because they're evanescent or contribute very little overall amplitude and can be neglected. Also, computing solutions that contribute little to the final solution can be computationally burdensome. A result of this trade ultimately leads to the truncated size selection for the summation ranges and matrix sizes.

An example for finding evanescent modes of higher order “m” can be seen when examining equation (4-32) with $k_{\rho_m} = \sqrt{k^2 - k_{z_m}^2}$. At larger values of “m”, it can be seen that $k^2 < k_{z_m}^2$ which makes k_{ρ_m} imaginary, representing evanescent radial wave modes. When $k = \omega\sqrt{\mu_I \epsilon_I}$ and (4-32) are substituted into $k^2 > k_{z_m}^2$, where k_{ρ_m} is still real, the relationship

$$\omega^2 \mu_I \epsilon_I > \frac{m^2 \pi^2}{a^2} \rightarrow \frac{a^2 \omega^2 \mu_I \epsilon_I}{\pi^2} > m^2 \rightarrow \frac{a * \omega \sqrt{\mu_I \epsilon_I}}{\pi} > \pm m \quad (6-45)$$

can be established, setting the upper limit for “m”. The same can be done for k_{ρ_l} and k_{z_l} . Following the same approach but using equations $k = \omega\sqrt{\mu_{II} \epsilon_{II}}$ and (5-9), the relationship

$$\begin{aligned} \omega^2 \mu_{II} \epsilon_{II} > \left(k \cos \theta^i + \frac{2\pi l}{(a+b)} \right)^2 &\rightarrow \omega \sqrt{\mu_{II} \epsilon_{II}} > k \cos \theta^i + \frac{2\pi l}{(a+b)} \rightarrow \\ \frac{(a+b)(\omega \sqrt{\mu_{II} \epsilon_{II}} - k \cos \theta^i)}{2\pi} > l &\rightarrow \frac{(a+b)k(1 - \cos \theta^i)}{2\pi} > l \end{aligned} \quad (6-46)$$

will provide an upper limit for “l”. These equations are implemented in the code, which will be discussed in the following sections, as checks for the user to compare his or her inputs. Violating these limits can prove challenging for the code to find solutions to the field equations, producing nonsensical, erroneous results with values of orders of magnitudes 10's to 100's of times greater than expected.

In summary, the “m” and “l” max values are selected in order to restrict the values of both k_{ρ_l} and k_{ρ_m} to the real domain, which also drives the size of the matrices, for the following reasons:

- Imaginary of k_{ρ_l} and k_{ρ_m} produce rapidly decaying evanescent fields that contribute little to the overall amplitude
- Computationally it can be burdensome to compute and in some cases challenging to find a solution.

It’s also important to note here that this restriction is acceptable to the author. In any approximation technique, there will be areas where computations are truncated and simplification assumptions are made. The results and comparisons in Chapter 7 will provide a guide for when the approach presented by this paper is most valid, with respect to the dimensions of the corrugated cylinder structure when compared to the wavelength of the incident plane-wave. It will be left for a future endeavor to stress the model approach presented in this research, to determine the exact limitations of specific assumptions (e.g. under what conditions can the restricting of k_{ρ_l} and k_{ρ_m} being real be considered unacceptable).

6.4 Numeric Computation Techniques and Tool Methodology

6.4.1 Tool Selection and Use

This next stage requires that of all the equations get implemented into a computational tool. There are many computational tools to choose from, however this author chose to use Mathematica® [17] based on its ability to handle math symbolically. Also, another significant driver for the selection of Mathematica® is the availability of a

free toolbox add-on to Mathematica®, available online from UC San Diego known as NCAIgebra [18], which can handle noncommutative algebra.

NCAIgebra makes it easy in manipulating matrices and vectors algebraically and symbolically. Its key use in this paper was to solve for each of the unknown expansion coefficients in terms of known terms, using the matching equations from (6-33) to (6-38). Essentially, a solve function native to the tool is used, which, once that is done, numeric values for each of terms are computed, plugged in, computed again and the coefficients would be solved for.

However, there were some convergence issues in the results. The issue was not fully identified but at this point, it is important to mention that when NCAIgebra produces solutions, it checks and validates it. This validation check produced a warning describing that the solution may be prone to error for certain circumstances, not described, since it could not guarantee the solution's accuracy. Based on the results and the NCAIgebra warning, the fully derived NCAIgebra method was commented out of the code. It was replaced by a loop solve algorithm developed for this research. However, NCAIgebra was still used to derive some of the unknown expansion coefficient equations where the solution check was validated, and were also used to spot check solutions from the loop solve algorithm used to replace it.

The loop solve algorithm was used to solve partially solved unknown coefficients. The solve function in Mathematica® was used within a loop to solve for the large matrix system of equations. As the loop solve algorithm increments, it solves an equation in terms of an unknown, then plugs that unknown into the equation of the next loop solve iteration. This process eliminates an unknown with each step. At the last step, the

unknown is found to have a value. At this point, another loop is implemented working backwards and plugging in values until all the unknowns are known.

During the numerical computational effort, there were issues that arose in solving for the unknown coefficients. They were attributed to ill-conditioned matrices which will be described in the next section.

6.4.2 Ill-Conditioned Matrices

It turned out that during the computation iterations in the process of this work, the computational tool would produce errors indicating ill-conditioned matrices. This was found during the inversion process of many of the matrices.

There has been much work behind ill-conditioned matrices, particularly in such a case as this one, where an ill-conditioned system of linear equations is involved in an engineering problem. The driving source is from an ill-posed problem, which does not necessarily stem from an ill-conceived design, but rather a fundamental physical limitation to the data at hand [19]. Described in such work, are suggestions for the use of the Moore–Penrose pseudoinverse, which relates to the least squares regression method in finding the shortest length solution to a problem [20]. Both the pseudoinverse and least squares method are made use of in the code, in order to eliminate the ill-conditioned errors and solve for the unknown expansion coefficients.

6.4.3 Tool Methodology

The following section will describe the high-level workflow on how the computational tools are used. It will show how the tools mentioned in section 6.4.1 are used in conjunction with the solving methods mentioned in section 6.4.2 . The workflow

below will describe the code in an already existing state and therefore the workflow steps describe the sequential flow of data, and not the creation of code.

Step 1: The boundary ‘b’ equations, (6-37) and (6-38), are used to solve for $C_{nl}^{(b)}$ and $D_{nl}^{(b)}$ using the least squares method with tool’s built-in least squares solver function. Equations were rearranged to solve for the specified expansion coefficient per the least squares solver function required arrangement [21]. See Figure 6-3 for pictorial form.

Step 2: The boundary ‘a’ equations (6-33) and (6-35) are used to solve for A_{nm} and B_{nm} . They are rearranged using manual matrix manipulation method with noncommutative algebra and solve for A_{nm} and B_{nm} in terms of known of field components, $C_{nl}^{(a)}$ and $D_{nl}^{(a)}$

Step 3: The boundary ‘a’ equation (6-34) is now used to solve for $C_{nl}^{(a)}$ in terms of $D_{nl}^{(a)}$ using the same method as in step 2.

Step 4: The new form of $C_{nl}^{(a)}$ (in terms of $D_{nl}^{(a)}$) is plugged into the new form of A_{nm} (in terms of $C_{nl}^{(a)}$) in order to put A_{nm} in terms of $D_{nl}^{(a)}$

Step 5: The boundary ‘a’ equation (6-36) is now used to solve for $D_{nl}^{(a)}$ in terms of known of field components, A_{nm} , and B_{nm} , where A_{nm} , and B_{nm} are substituted by the solutions in the previous step.

Step 6: $D_{nl}^{(a)}$ is now expanded and solved for all the expanded coefficients within the loop algorithm referenced earlier as the loop solve algorithm. Once complete, $D_{nl}^{(a)}$ is fully solved for numerically.

Step 7: $D_{nl}(a)$ is plugged into $C_{nl}^{(a)}$ and solved for. Both of which are now plugged into A_{nm} and B_{nm} , which are solved for as well, completing the numerical solving of the expansion coefficients. Steps 2 – 7 can be seen in Figure 6-4.

A pictorial overview of this workflow can be seen in Figure 6-2. It includes additional steps required for configuration and result generation.

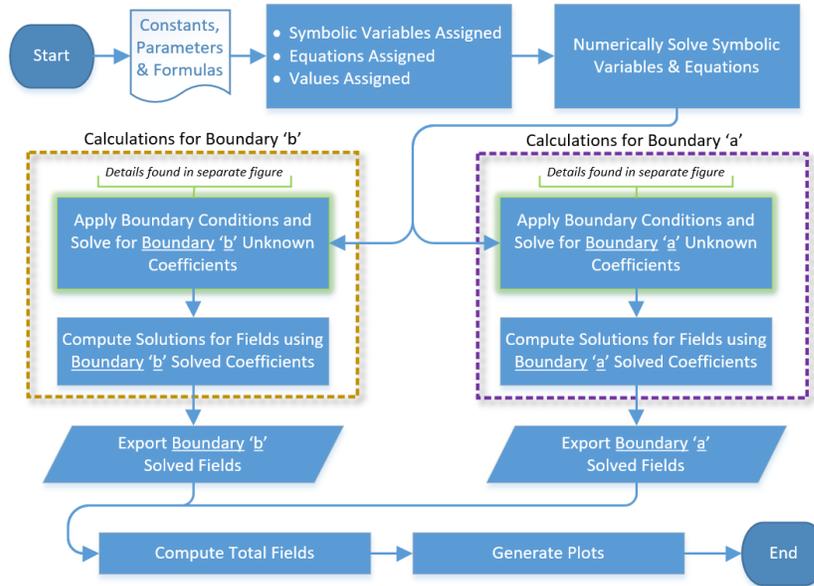


Figure 6-2 Software Process Workflow

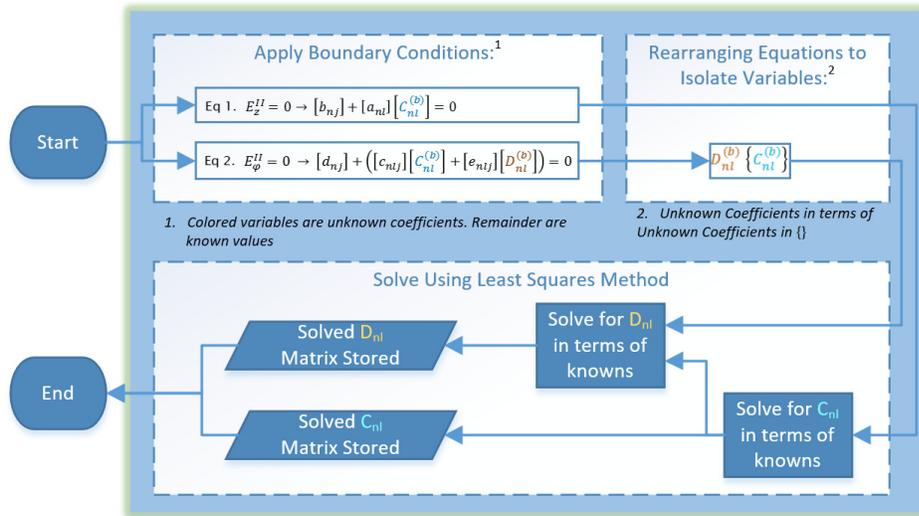


Figure 6-3 Solving for Boundary 'b' Unknown Coefficients Flow Chart

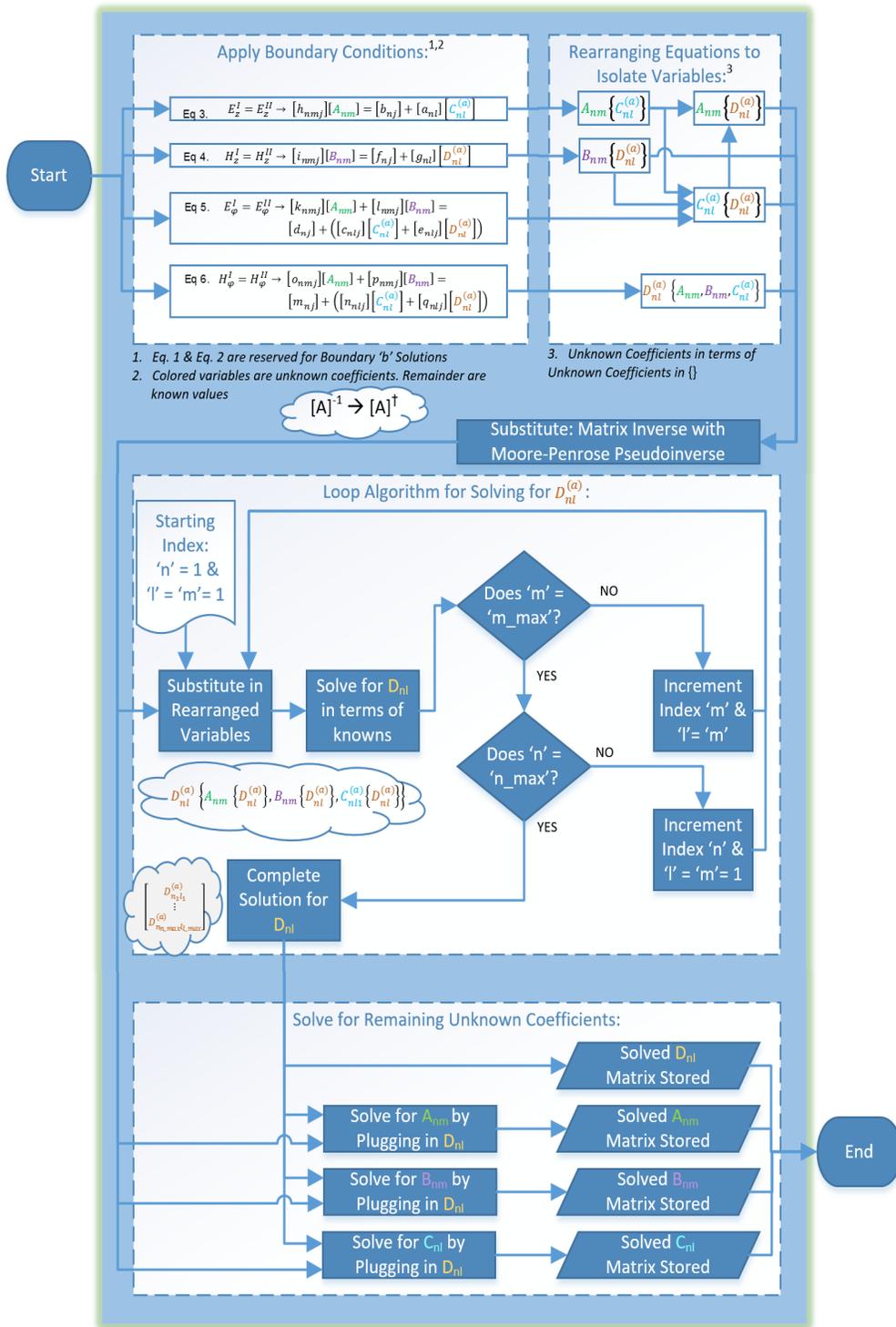


Figure 6-4 Solving for Boundary 'a' Unknown Coefficients Flow Chart

CHAPTER 7 RESULTS, COMPARISONS AND FUTURE RESEARCH

7.1 Model Configuration and Parameters

Many configurations and parameters were set up to support the research in this paper. This section will attempt to describe the key configurations and parameters in order to facilitate understanding of the results. Note, this model is composed of multiple smaller models, most centered on the periodic corrugated cylinder. However, there's also a smooth cylinder model incorporated, which will be discussed in section 7.3 .

7.1.1 Parameters Relative to Lambda

The model computes and displays many of the results in terms of the wavelength λ , where $\lambda = \frac{c}{f}$, where 'f' is the frequency of the incident field and 'c' is the speed of light. Also, the dimensions of the corrugated cylinder are described in units of λ , which include the corrugation opening denoted by 'a', thickness of the metallic corrugation portion denoted by 'b', the inner corrugation radius ρ_1 and the exterior corrugation radius ρ_2 . Note that the period of the corrugation is equal to 'a + b'. This includes the plots displayed later in this chapter, which vary in ρ and have an axis in units of λ , displayed as ρ/λ . This allows the model to display results that are independent of a specified frequency/wavelength. However, parameters do have values thus a λ is chosen and can be varied while fixing the geometry, if so desired. For the purpose of this paper, λ is fixed and the geometry and other parameters are varied.

In the results section, multiple scenarios were run with different parameter changes. One such parameter was labeled ‘d’ which signifies a relative ‘dimension’ to λ , which the physical dimension parameters of the corrugated and smooth cylinders are linked to. For example, the dimension ‘b’, the thickness of the protruding part of the corrugation, is always set equal to ‘d’ in all the scenarios, unless explicitly stated otherwise. The parameter ‘d’ allows for the description of 3 different groupings of relative physical dimensions which are $d \gg \lambda$ by setting $d = 20\lambda$, $d \approx \lambda$ by setting $d = 2\lambda$, and $d \ll \lambda$ by setting $d = 0.1\lambda$. This was done in order to more clearly gauge the performance of the model relative to the different scattering regimes laid out by the figure, as per described in [22]. Also, according to Fuhs [23, p. 18], when in the Rayleigh scattering region ($d \gg \lambda$), polarization is not important for the magnitude of RCS.

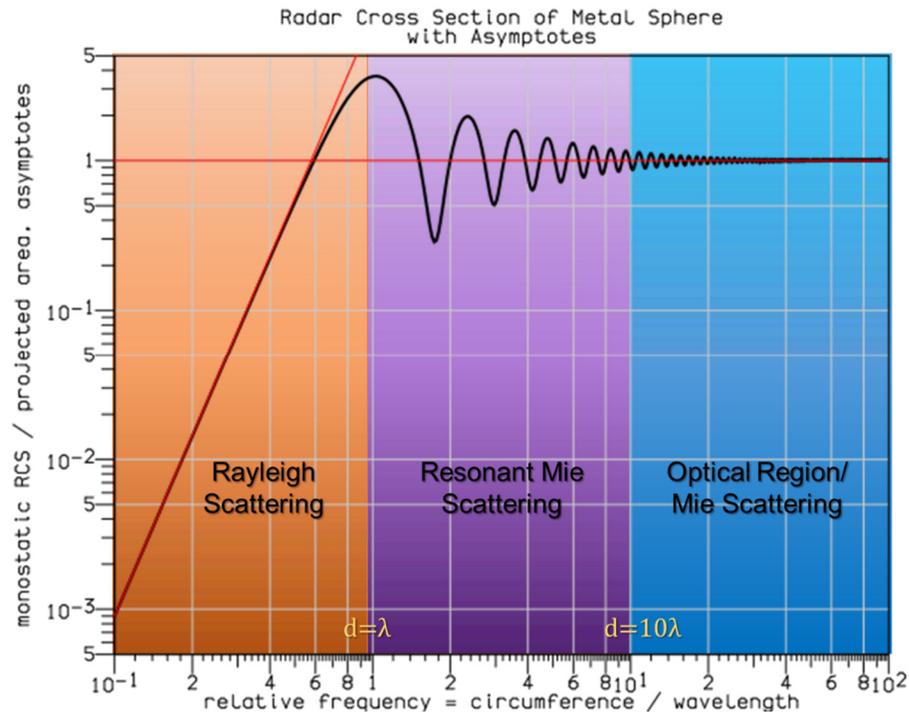


Figure 7-1 Relative relationship of target size to illuminated wavelength with associated regions of scattering approximation, courtesy of Wikipedia [24]

7.1.2 Incident Field Parameters

The incident field amplitudes are driven by the E_0 value for the TM_z mode and the H_0 value for the TE_z mode. Since these modes are independent of each other, E_0 and H_0 values can be selected independent of each other. It is important to note at this point, that the H-fields amplitudes in the TM_z mode are driven by the E_0 , where the H-field amplitude is equal to $\frac{E_0}{Z}$, where $Z = \sqrt{\frac{\mu_{II}}{\epsilon_{II}}}$ and is the impedance of the medium in which the incident field is in. The same holds true for the E-fields in the TE_z mode, in that it's dependent on the H_0 value, where the E-field amplitude is equal to ZH_0 .

7.1.3 Point Matching Selection

As discussed in Chapter 6, point matching is required for the numerical solution of the unknown expansion coefficients. There are various points that could be selected with the prescribed range for that boundary condition, with ρ always being equal to ρ_2 . The type and quantity of matching points can worsen or improve the numerical results, though a minimum of 'j' quantity, expansion number of the coefficients, is required.

Different matching point techniques were attempted during the development of the model. When the NCAIgebra method was first utilized, it allowed for an overdetermined solution where there were more equations (or 'j' points), than unknowns, (or expansion count of coefficients). That's because it was fully defined in the pseudoinverse and least squares method. However, due to its limitations as described in section 6.4.1, the NCAIgebra method was abandoned and the new technique did not allow for an overdetermined solution in its current form.

Two main matching point techniques were maintained in the model. One was fixing ϕ to an arbitrary ϕ value from 0 to 2π while varying z 'j' times, evenly spaced

spanning the distance of the boundary, being ‘a’ or ‘b’ depending on that boundary. The other was to fix z to an arbitrary z value within the boundary, while varying ϕ ‘j’ times evenly from 0 to 2π .

The results computed were done fixing z and varying ϕ . This produces more accurate results, which is due to the fact that the computed comparison results did not vary z values, but did vary ϕ in the changing ϕ results. Therefore, the selection in matching points that is best suited is the matching points that would reinforce the intended computational analysis, which was to vary ϕ .

7.1.4 Total E-Field Calculation

The total E-field calculation finds the magnitude of the combined fields. The method is fairly straight forward. The fields are converted from cylindrical coordinates to rectangular coordinates, which can be found in [12, p. 923] to form

$$E_x = E_\rho \cos \phi + E_\phi \sin \phi \quad (7-1)$$

$$E_y = E_\rho \sin \phi + E_\phi \cos \phi \quad (7-2)$$

$$E_z = E_z \quad (7-3)$$

Then, each of the rectangular coordinate forms of fields are squared, summed together and then the square root of that number is attained.

$$\sqrt{E_x^2 + E_y^2 + E_z^2} = E_{Total} \quad (7-4)$$

This is done for every data point to generate the total E-field data.

7.1.5 Reconciliation of Boundary ‘a’ and Boundary ‘b’

Up to this point, the equations for boundary ‘a’ and boundary ‘b’ have been given separate treatment. However, results were computed for the separate field equations and

results plotted and incorporated into the results section. At the near field, where $\rho \leq \lambda$, the boundaries can be treated separately.

For the far field, $\rho \gg \lambda$, boundary ‘a’ and boundary ‘b’ solutions are examined for their accuracy. Either technique alone should produce a gross representation of the scatter, though within certain regions the approximations of the field amplitudes can be poor. However, the hybrid nature of the problem formulation allows for the depolarization representation of the periodic corrugated cylinder.

A technique described by Kishk et al [25], the asymptotic boundary condition method, utilizes coefficients that vary with the z axis, and are weighted by a ratio factor w/p , where ‘w’ is the dimension of the corrugation opening and ‘p’ is the corrugation period. This is done at the boundary condition to develop a complete field solution, where more detail can be found in [26]. This technique and variations thereof were investigated but not implemented.

In the present work, the field solutions for boundary ‘a’ is added with that of boundary ‘b’. This superposition of fields, produces the results shown for the runs labeled “Run a_plus_b...”. The results are compared to that of a smooth cylinder as well as to alternate methods for computing the scattered field of a corrugated cylinder [27]. This treatment of superposition of fields is done in [28], where the field of a cylinder without accounting for the corrugated perturbations, represented as metallic rings, and then added to the scattering due to the metallic rings.

7.2 RCS Computation

The model produces various Radar Cross Section (RCS) plots, as this is a typical convention in the electromagnetics scattering community, to display and compare

scattered fields. The RCS symbol, σ , is the designated symbol to represent the RCS value, which is in units of m^2 . The formula representing σ is derived from the free-space loss factor cause by the spherical spreading of a propagating planewave, which a full description of its derivation can be found in [29, p. 96]. This model uses σ in the form

$$\sigma = \lim_{R \rightarrow \infty} \left[4\pi R^2 \frac{|E^s|^2}{|E^i|^2} \right] \quad (7-5)$$

where ‘R’ is the distance of observation from the target, meters. The value ‘R’ needs to be large enough where $R \gg$ than the largest physical dimension of the target and wavelength so that the propagating planewave representation holds and the formula remains valid. The RCS, σ , can also be calculated in decibels, dB, in order to display a large range of data. The units are in decibels per square meter or dBsm. This is calculated as

$$\sigma_{dBsm} = \lim_{R \rightarrow \infty} \left[10 \log_{10} 4\pi R^2 \frac{|E^s|^2}{|E^i|^2} \right]. \quad (7-6)$$

It is important to take note of the aspect angles, ϕ , that are used in the σ calculations, as the computed results can vary. There is the ϕ of the incidence field, ϕ_i , and the ϕ of the observed or of the scattered field, ϕ_s . In each of the variations, ϕ_s values are typically swept through from 0 to 2π . The following are the different methods for varying the ϕ values in order to get the different σ results:

- *RCS ϕ Sweep Method 1:* ϕ_s is swept through 0 to 2π and ϕ_i is kept at a fixed constant value between 0 to 2π .
- *RCS ϕ Sweep Method 2:* ϕ_s is swept through 0 to 2π and $\phi_i = \phi_s$. This is typically referred to as a monostatic RCS since it assumes the transmitter and receiver, for typical radar applications, are at the same location.

- *RCS φ Sweep Method 3*: φ_s is swept through 0 to 2π and $\varphi_i = \varphi_s + \varphi_{\text{offset}}$, where φ_{offset} is an offset value of φ . This is typically referred to as a bistatic RCS since it assumes the transmitter and receiver, for typical radar applications, are at separate locations.

The technique used in this paper is RCS φ sweep method 1.

7.3 Smooth Cylinder Comparison Model

In order to have a comparison model for the periodic corrugated cylinder, a smooth cylinder was modeled. The dimensions of the corrugated cylinder can be adjusted to approximate a smooth cylinder and then compared to the smooth cylinder model.

A smooth cylinder model of oblique incidence planewave is found in [12, pp. 614-624]. This textbook model provided the basis for the TM_z mode scattered equations

$$E_{\rho}^S (TM) = jE_0 \cos \theta^i e^{+jk \cdot z \cdot \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n(k\rho_2 \sin \theta^i)}{H_n^{(2)}(k\rho_2 \sin \theta^i)} \left(\frac{H_{n-1}^{(2)}(k\rho \sin \theta^i) - H_{n+1}^{(2)}(k\rho \sin \theta^i)}{2} \right) e^{jn\varphi} \quad (7-7)$$

$$E_{\varphi}^S (TM) = jE_0 \frac{\cot \theta^i}{k\rho} e^{+jk \cdot z \cdot \cos \theta^i} \sum_{n=-\infty}^{\infty} nj^{-n+1} \frac{J_n(k\rho_2 \sin \theta^i)}{H_n^{(2)}(k\rho_2 \sin \theta^i)} H_n^{(2)}(k\rho \sin \theta^i) e^{jn\varphi} \quad (7-8)$$

$$E_z^S (TM) = E_0 \sin \theta^i e^{+jk \cdot z \cdot \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n(k\rho_2 \sin \theta^i)}{H_n^{(2)}(k\rho_2 \sin \theta^i)} H_n^{(2)}(k\rho \sin \theta^i) e^{jn\varphi} \quad (7-9)$$

and the TE_z mode scattered equations

$$E_{\rho}^S (TE) = -j \frac{H_0}{\omega \varepsilon \rho} \frac{e^{+jk \cdot z \cdot \cos \theta^i}}{\sin \theta^i} \sum_{n=-\infty}^{\infty} nj^{-n+1} \frac{J_{n-1}(k\rho_2 \sin \theta^i) - J_{n+1}(k\rho_2 \sin \theta^i)}{H_{n-1}^{(2)}(k\rho_2 \sin \theta^i) - H_{n+1}^{(2)}(k\rho_2 \sin \theta^i)} H_n^{(2)}(k\rho \sin \theta^i) e^{jn\varphi} \quad (7-10)$$

$$E_{\varphi}^S (TE) = jH_0 \sqrt{\frac{\mu}{\varepsilon}} e^{+jk \cdot z \cdot \cos \theta^i} \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_{n-1}(k\rho_2 \sin \theta^i) - J_{n+1}(k\rho_2 \sin \theta^i)}{H_{n-1}^{(2)}(k\rho_2 \sin \theta^i) - H_{n+1}^{(2)}(k\rho_2 \sin \theta^i)} \left(\frac{H_{n-1}^{(2)}(k\rho \sin \theta^i) - H_{n+1}^{(2)}(k\rho \sin \theta^i)}{2} \right) e^{jn\varphi} \quad (7-11)$$

$$E_z^S (TE) = 0. \quad (7-12)$$

The Hankel and Bessel order 'n' is set to the same 'n' as used in the corrugated cylinder model. The radius of the smooth cylinder is ρ_2 , the same dimension as the larger radius of the corrugated cylinder.

Note that only the electric field components were used. Using only the electric fields provides an adequate comparison, as there is no polarization and therefore no need to fully represent a system of each TM_z and TE_z mode as in the corrugated case. Each mode will have the fields calculated separately and then, through the principle of superposition, combined with each other on certain plots in the following section. Also, the incident field is the same as that incident onto the corrugated cylinder in the model described in Chapter 3.

The smooth cylinder results are computed and displayed alongside the periodic corrugated cylinder results. Since the periodic corrugated cylinder is of a hybrid mode, both TM_z and TE_z modes exist within the periodic corrugated cylinder scattered field. However, the data displayed for the smooth cylinder is made available to show the separate TM_z and TE_z modes, as well as the superposition combined modes. The data sets were created for the different cylindrical coordinate axes.

A subset of the data is collected and analytically compared between periodic corrugated cylinder and the smooth cylinder, in order to calculate the mean of percent error between them. This data set is composed of the superposition combined modes, in RCS dBsm, for each of the cylindrical coordinate axes and the total field. The data points at each ϕ , for the smooth and corrugated cylinders, are subtracted from each other and the absolute value of that is divided by the smooth cylinder dBsm value, and finally multiplied by 100% to give the percent error, as in equation (7-13).

$$\frac{|\sigma_{dBsm [smooth]} - \sigma_{dBsm [corr]}|}{\sigma_{dBsm [smooth]}} \cdot 100\% = \% \text{ error of } \sigma_{dBsm} . \quad (7-13)$$

Then, the mean of the percent error is found for each of the data subsets.

7.4 Alternate Corrugated Cylinder Method Comparison

In order to fully validate the results of the periodic corrugated cylinder scattered field, a comparison to an alternate method for the same geometry is merited. The chosen comparison method was from A. Freni et al [27] where results for a Finite Element Method (FEM) and the Method of Moments (MoM) are captured in figure 3 of that paper. The geometry referenced in figure 3 of [27] was utilized and the cross-polar plot was recreated in this paper, by extracting the FEM and MoM data curves, shown in Figure 7-150. Also captured in Figure 7-150 are the results using this research's technique. Data was extracted from figure 3 of [27] using a curve mapping and data extraction tool called WebPlotDigitizer [30]. The data plotted is, $\sigma_{\phi\theta}/\lambda_0$ (dB), which is the cross-polar scatter width derived from

$$\sigma_{\phi\theta} = \lim_{\rho \rightarrow \infty} \left[2\pi\rho \frac{|E_{\phi}^s|^2}{|E_{\theta}^i|^2} \right] \quad (7-14)$$

which the first subscript is the polarization of the scattered field and the second subscript is the polarization of the incident field [28]. A comparison of this technique can also be found in [31] by the author of this research.

7.5 Results

A variety of different runs were executed, as was discussed earlier. Table 1 captures a summary of the boundary 'a' simulation runs with the adjusted parameters identified, on runs comparing the corrugated cylinder to that of the smooth cylinder. Also, boundary 'b' runs were generated (see Table 2), using the same parameters as the subset runs of boundary 'a' shown in this chapter, except with a z position in the

boundary ‘b’ region. Table 3 captures a summary of the boundary ‘a’ plus boundary ‘b’ runs, which represent the final solution approach. The different runs captured in the subsequent sections use a title scheme described by the example in Figure 7-1, in order to help identify the configuration for each run and the plots captured in that section.

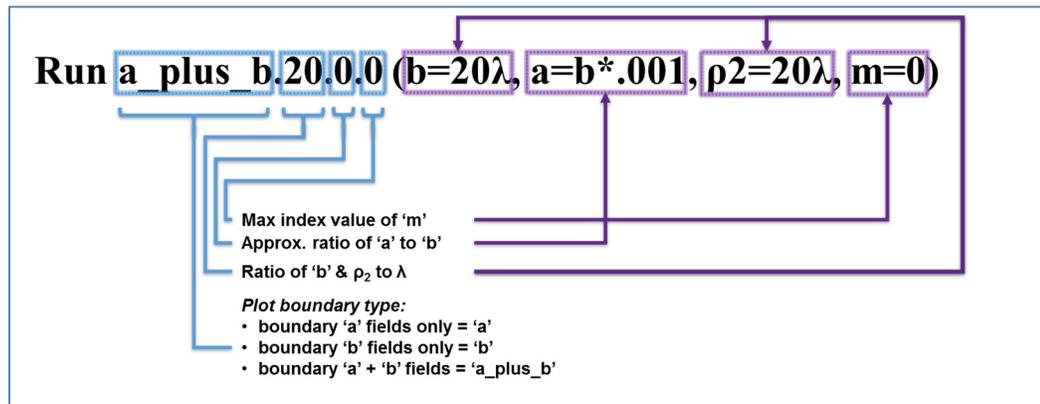


Figure 7-2 A run title example describing each component of the title and how it relates to the run’s configuration

From Table 1, it can be seen that some of the runs have a status of ‘Bad Data/III-Condition’. These were mostly runs that had ‘m’ or ‘l’ that were exceeding their max allowable value, allowing k_p to become imaginary. As mentioned in section 6.3, these modes in which k_p are imaginary, produce evanescent waves which decay rapidly when moving away from the field source at the cylinder edge, and thus can be ignored.

Another item to note, is that all the runs were kept at $n=3$. This an acceptable mode or Hankel function order as much of the work with similar scattering geometries have been conducted at $n=1$ or $n=2$, such as [32]. This upper limit was also a computational limitation. Orders above $n=3$ would not produce a solution with the capability and the time allotted for the computer systems used.

The following subsections provide a subset of the simulation runs collected as part of this research effort. They are pertinent comparative material between the periodic

corrugated cylinder model and the comparison model which are used to draw conclusions from. The mean error, as described in section 7.3 are shown for boundary 'a'(Figure 7-3), boundary 'b'(Figure 7-4) and boundary 'a+b'(Figure 7-5).

Each of the presented runs are in their own section with multiple plots. Each section consists of the following:

- 1 detailed summary table of all the ϕ changing plot parameters,
- 4 Polar Plots of RCS dBsm (E_z , E_ρ , E_ϕ and E_{Total} of $\text{TM}_z + \text{TE}_z$ modes)
- 4 XY Plots of RCS dBsm (E_z , E_ρ , E_ϕ and E_{Total} of $\text{TM}_z + \text{TE}_z$ modes)
- 1 detailed summary table of all the ρ changing plot parameters
- 8 XY field amplitude plots (Absolute value of the fields : E_z , E_ρ , E_ϕ and E_{Total} of $\text{TM}_z + \text{TE}_z$ modes, for scattered field and for scattered + incident field)..

Additional results are also provided here. As mentioned in section 7.4 , an alternate method in representing scattering of a corrugated cylinder is discussed with results in section 7.5.10 . Also, the relative dielectric constant in region I is varied and compared, showing the effects of dielectric loading and lossy dielectric loading, with results in section 7.5.11 .

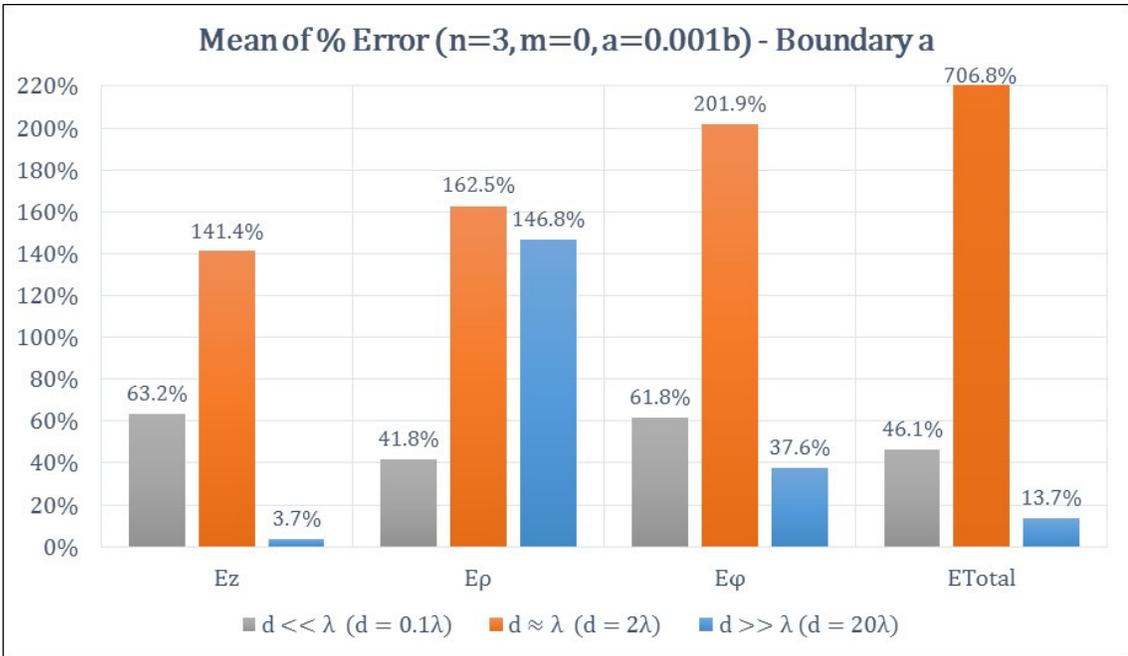


Figure 7-3 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'a'

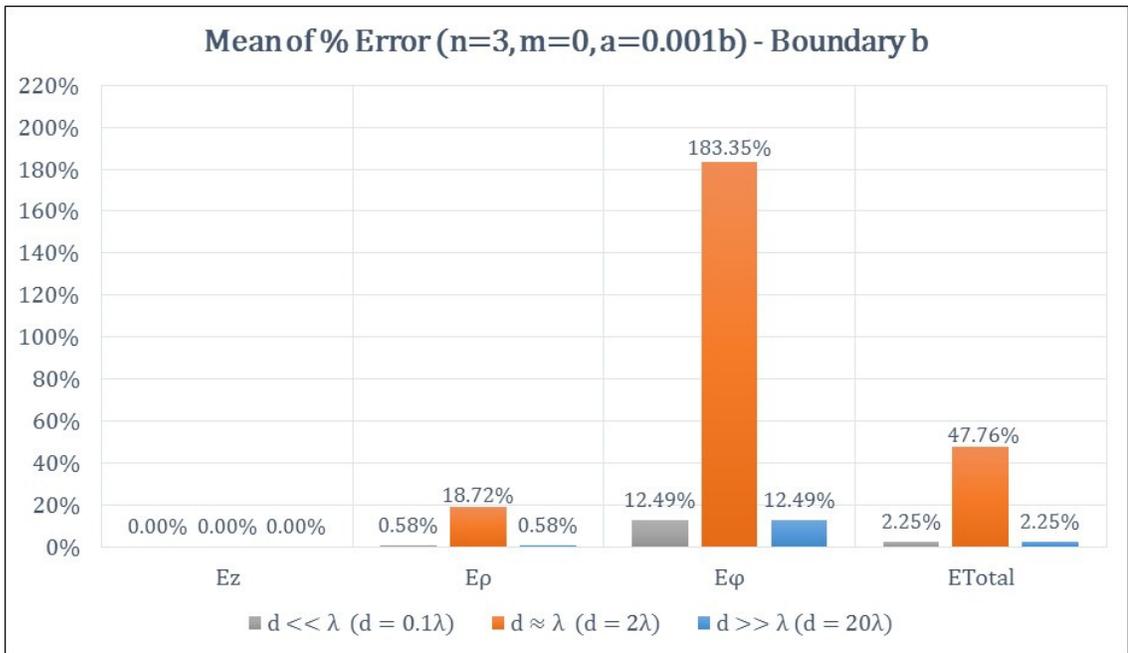


Figure 7-4 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'b'

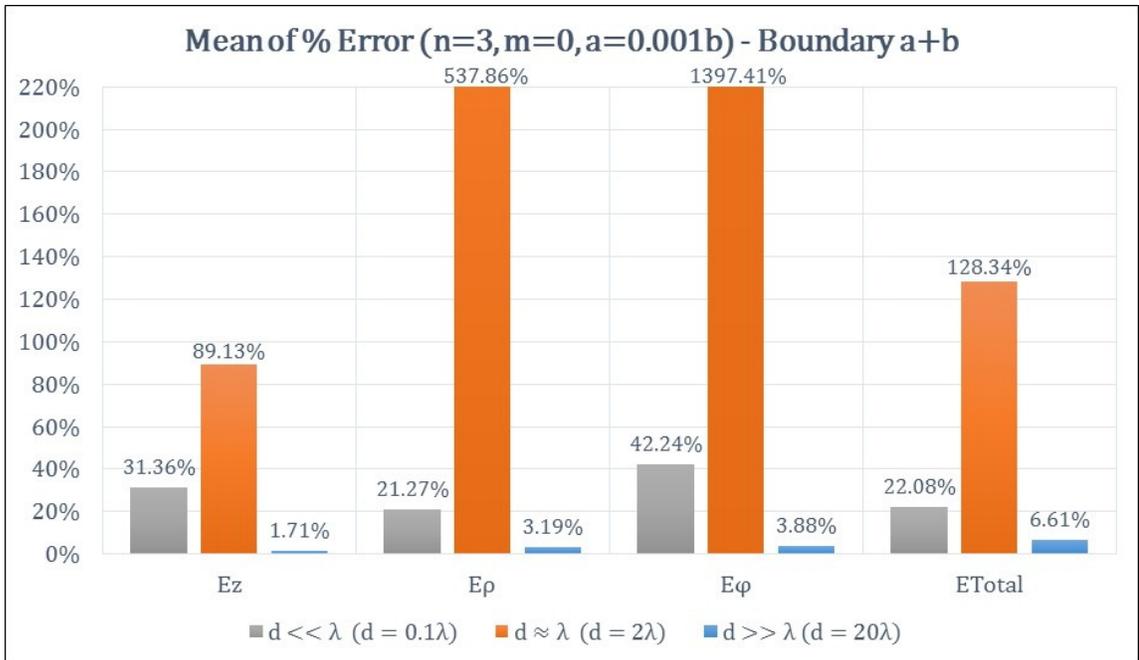


Figure 7-5 Mean of %error between corrugated cylinder and smooth cylinder model, for boundary 'a+b'

Table 1 Summary of boundary 'a' simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models

	Run Title	b	a	ρ_2	ρ_1	ρ_{far}	n	m	Status	Plot Location	Max Allowable "m" or "l"
$d=20*\lambda$	Run a.20.100.0	$20*\lambda$	$b*1$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Appendix	17
	Run a.20.100.1	$20*\lambda$	$b*1$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	17
	Run a.20.75.0	$20*\lambda$	$b*.75$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	14
	Run a.20.75.1	$20*\lambda$	$b*.75$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	14
	Run a.20.50.0	$20*\lambda$	$b*.5$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	12
	Run a.20.50.1	$20*\lambda$	$b*.5$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	12
	Run a.20.25.0	$20*\lambda$	$b*.25$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	10
	Run a.20.25.1	$20*\lambda$	$b*.25$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	10
	Run a.20.0.0	$20*\lambda$	$b*.001$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Chapter 7	0
	Run a.20.0.0	$20*\lambda$	$b*.001$	$20*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
$d=2*\lambda$	Run a.2.100.0	$2*\lambda$	$b*1$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Appendix	4
	Run a.2.100.1	$2*\lambda$	$b*1$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	4
	Run a.2.75.0	$2*\lambda$	$b*.75$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	3
	Run a.2.75.1	$2*\lambda$	$b*.75$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	3
	Run a.2.50.0	$2*\lambda$	$b*.5$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	2
	Run a.2.50.1	$2*\lambda$	$b*.5$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Complete	--	2
	Run a.2.25.0	$2*\lambda$	$b*.25$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	1
	Run a.2.25.1	$2*\lambda$	$b*.25$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Could not solve for 'a' coefficients "Input	N/A	1
	Run a.2.0.0	$2*\lambda$	$b*.001$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Chapter 7	0
	Run a.2.0.1	$2*\lambda$	$b*.001$	$2*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
$d=0.1*\lambda$	Run a.0.1.100.0	$.1*\lambda$	$b*1$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Appendix	0
	Run a.0.1.100.1	$.1*\lambda$	$b*1$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
	Run a.0.1.75.0	$.1*\lambda$	$b*.75$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	0
	Run a.0.1.75.1	$.1*\lambda$	$b*.75$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
	Run a.0.1.50.0	$.1*\lambda$	$b*.5$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	0
	Run a.0.1.50.1	$.1*\lambda$	$b*.5$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
	Run a.0.1.25.0	$.1*\lambda$	$b*.25$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	--	0
	Run a.0.1.25.1	$.1*\lambda$	$b*.25$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0
	Run a.0.1.0.0	$.1*\lambda$	$b*.001$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	0	Complete	Chapter 7	0
	Run a.0.1.0.1	$.1*\lambda$	$b*.001$	$.1*\lambda$	$\rho_2*0.99$	ρ_2*10	3	1	Bad Data/III-Conditioned	N/A	0

Table 2 Summary of boundary 'b' simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models

Run Title	b	a	ρ_2	ρ_1	pfar	n	m	Status	Plot Location	Max Allowable "m" or "l"
Run b.20.0.0	20* λ	b*.001	20* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0
Run b.2.0.0	2* λ	b*.001	2* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0
Run b.0.1.0.0	.1* λ	b*.001	.1* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0

Table 3 Summary of boundary 'a+b' simulation runs conducted and adjusted parameters for comparing the corrugated cylinder and smooth cylinder models

Run Title	b	a	ρ_2	ρ_1	pfar	n	m	Status	Plot Location	Max Allowable "m" or "l"
Run a_plus_b.20.0.0	20* λ	b*.001	20* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0
Run a_plus_b..2.0.0	2* λ	b*.001	2* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0
Run a_plus_b..0.1.0.0	.1* λ	b*.001	.1* λ	ρ_2 *0.99	ρ_2 *10	3	0	Complete	Chapter 7	0

For sections 7.5.1 through 7.5.9, refer to Figure 7-2 to interpret the title of each section in order to understand the overall configuration of the model for the plots captured in that section. Also, the first table in each section will provide a more detailed set of configuration parameters specifically for the polar plots, preceding the polar plots. The second table in each section, after the polar plots but prior to the XY phi plots, will provide a detailed set of configuration parameters specifically for the XY phi plots. The third table in each section (if present, as not all results had these sets of plots), after the XY phi plots but prior to the XY rho plots, will provide a detailed set of configuration parameters specifically for the XY rho plots.

7.5.1 Run a.20.0.0 (b=20 λ , a=b*.001, ρ_2 =20 λ , m=0)

Table 4 Detailed parameters summary for changing ϕ plots of Run a.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105 $\times 10^{10}$ Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.02 λ	-	-	-	-
b	20. λ	-	-	-	-
ρ_1	19.98 λ	-	-	-	-
ρ_2	20. λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	200. λ	-	-	-	-
z (observed)	0.25 a && 0.005 λ	-	-	-	-
Matching Points	-	-	-	-	7
ϕ_i	55. Deg	-	-	-	-
ϕ_l	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary a	-	-	-	-

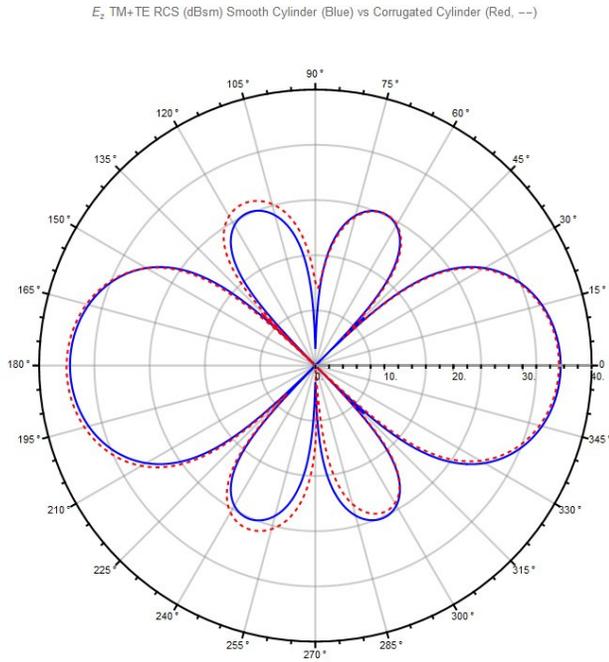


Figure 7-6 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0

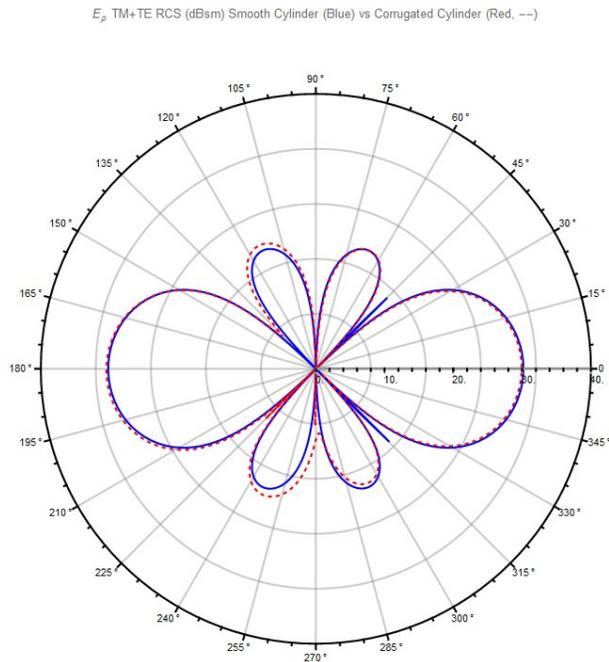


Figure 7-7 Polar Plot form of RCS dBsm for E_p of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0

E_{ϕ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

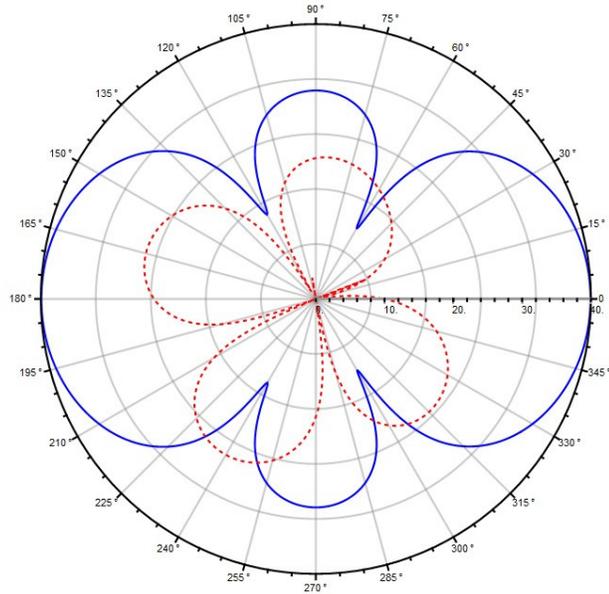


Figure 7-8 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.20.0.0

E_{Total} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

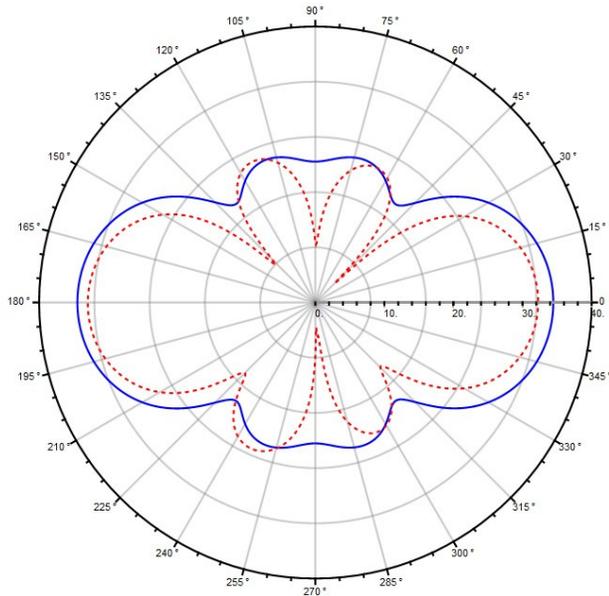


Figure 7-9 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

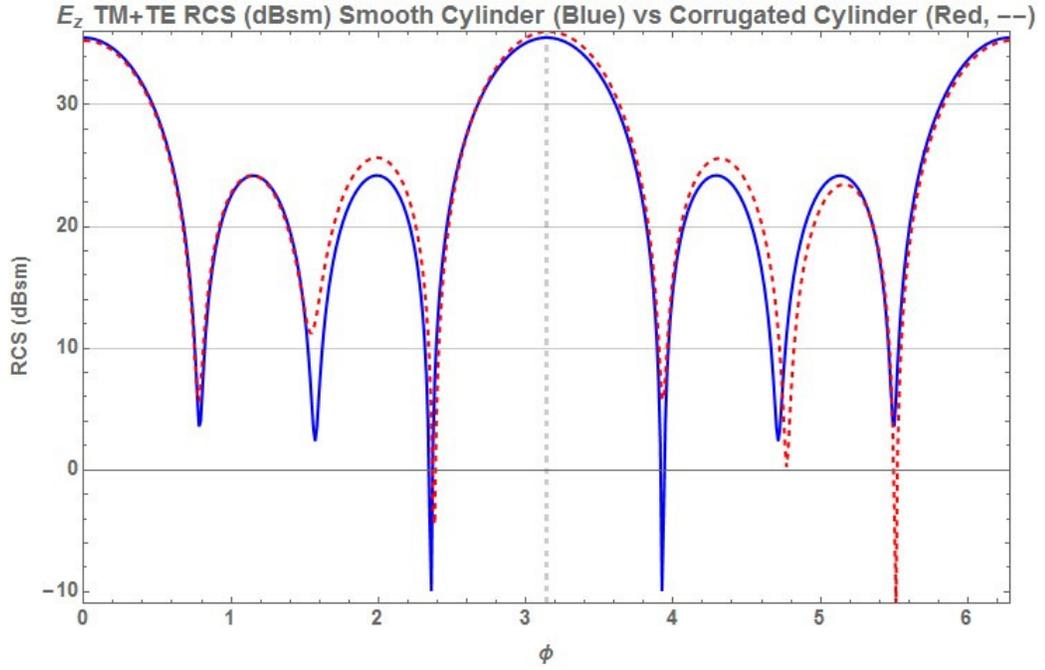


Figure 7-10 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

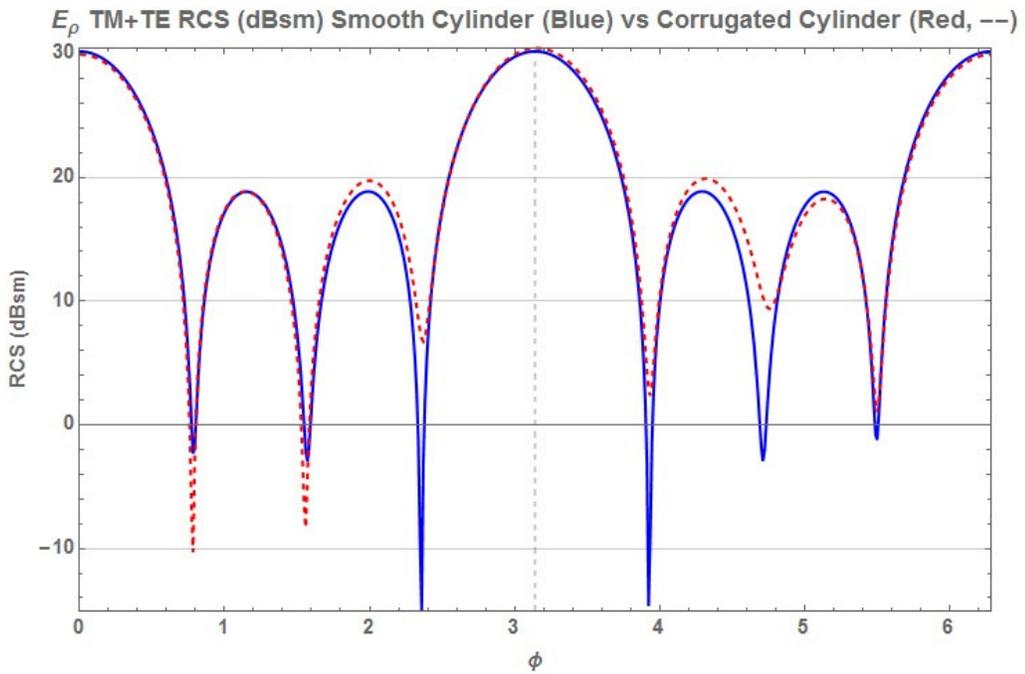


Figure 7-11 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

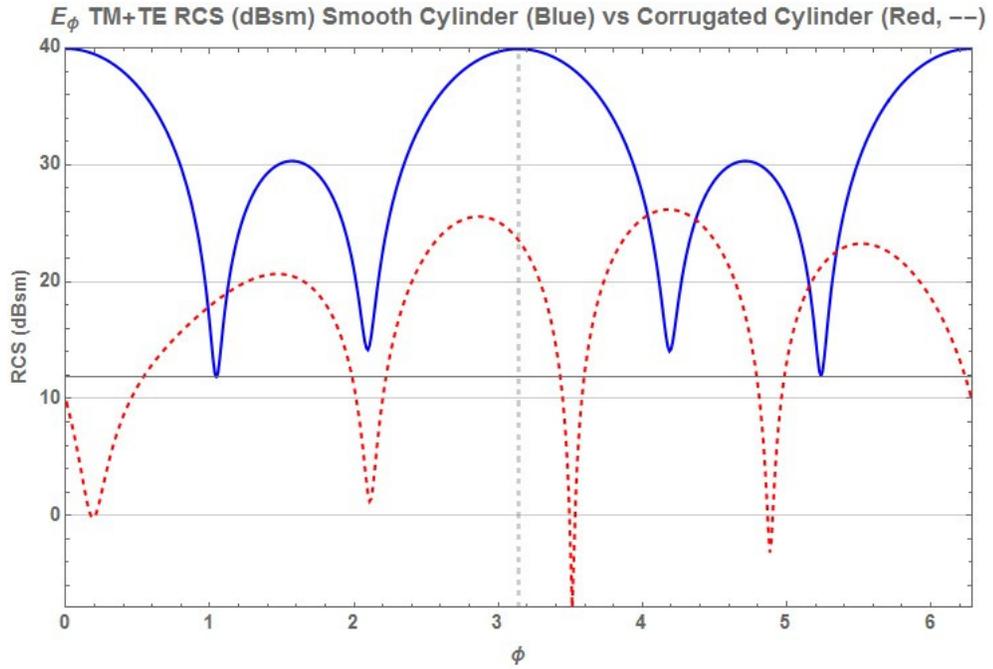


Figure 7-12 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

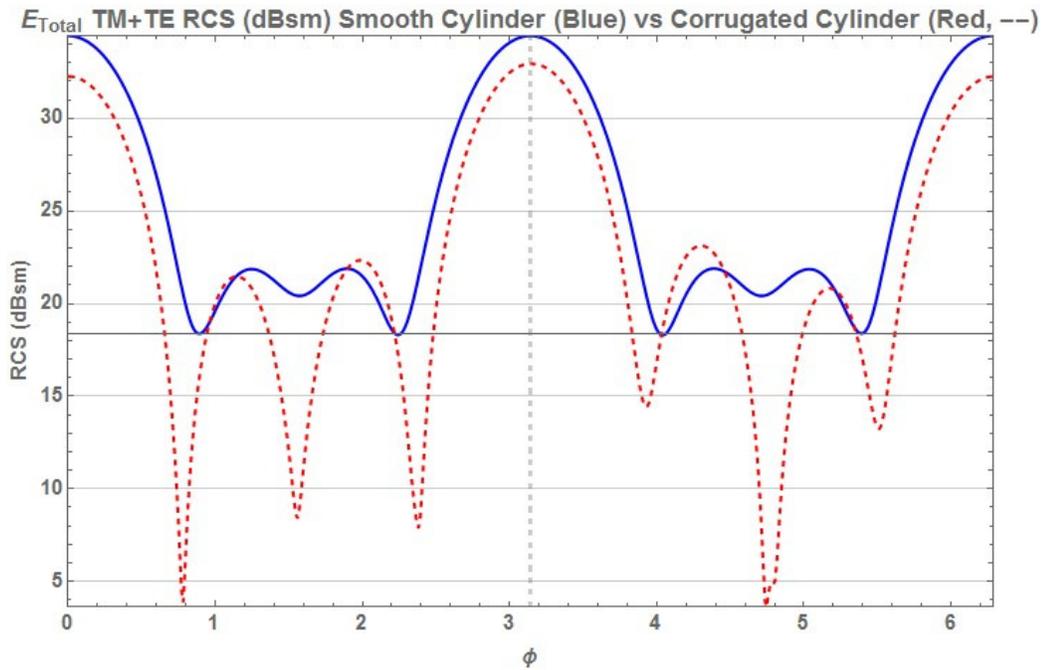


Figure 7-13 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

Table 5 Detailed parameters summary for changing ρ plots of Run a.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.02λ	-	-	-	-
b	$20. \lambda$	-	-	-	-
ρ_1	19.98λ	-	-	-	-
ρ_2	$20. \lambda$	-	-	-	-
ρ range	-	17.982λ	$30. \lambda$	0.0218907λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$0.25 a \&\& 0.005 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary a	-	-	-	-

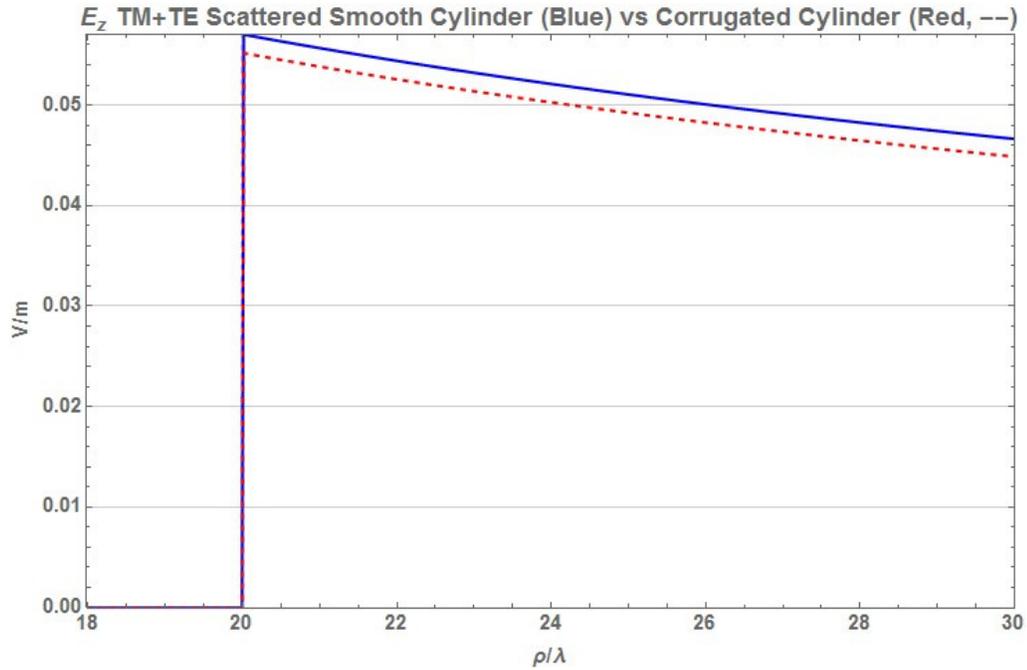


Figure 7-14 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

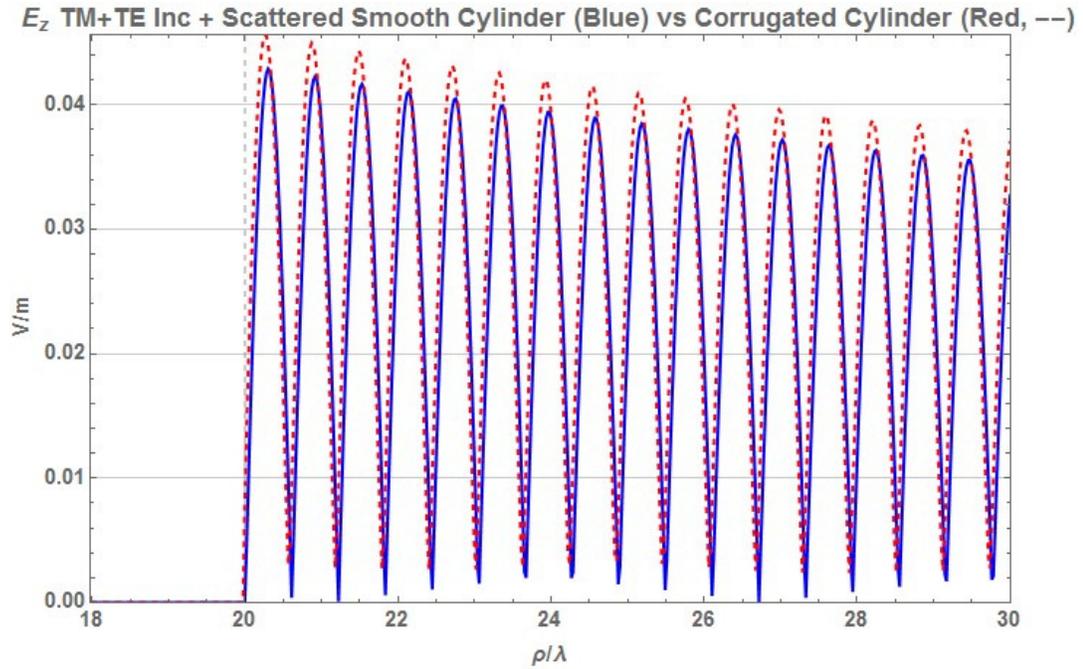


Figure 7-15 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

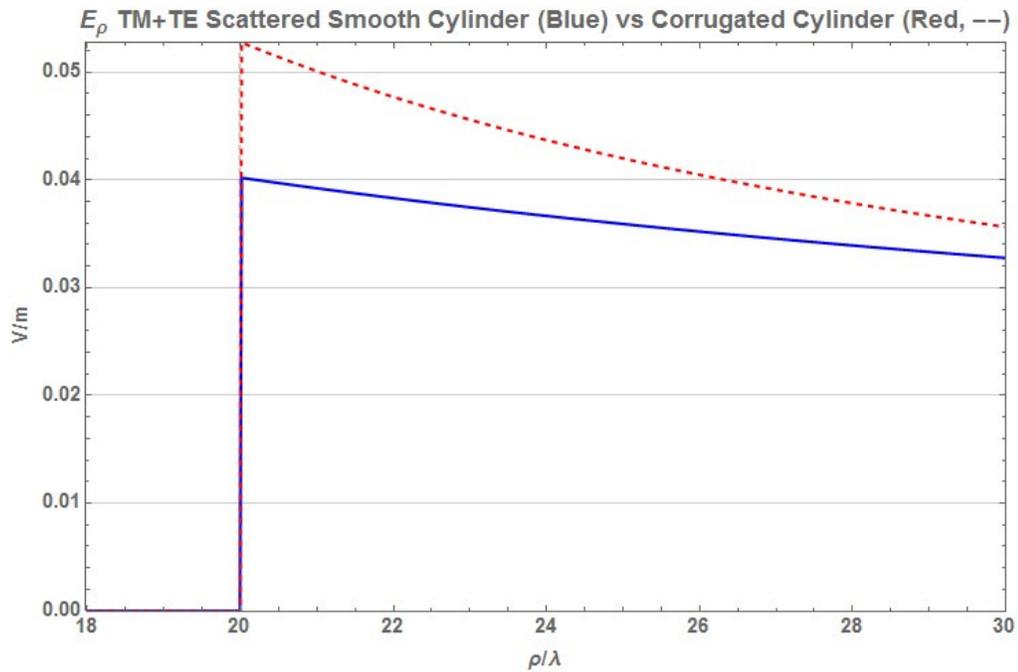


Figure 7-16 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

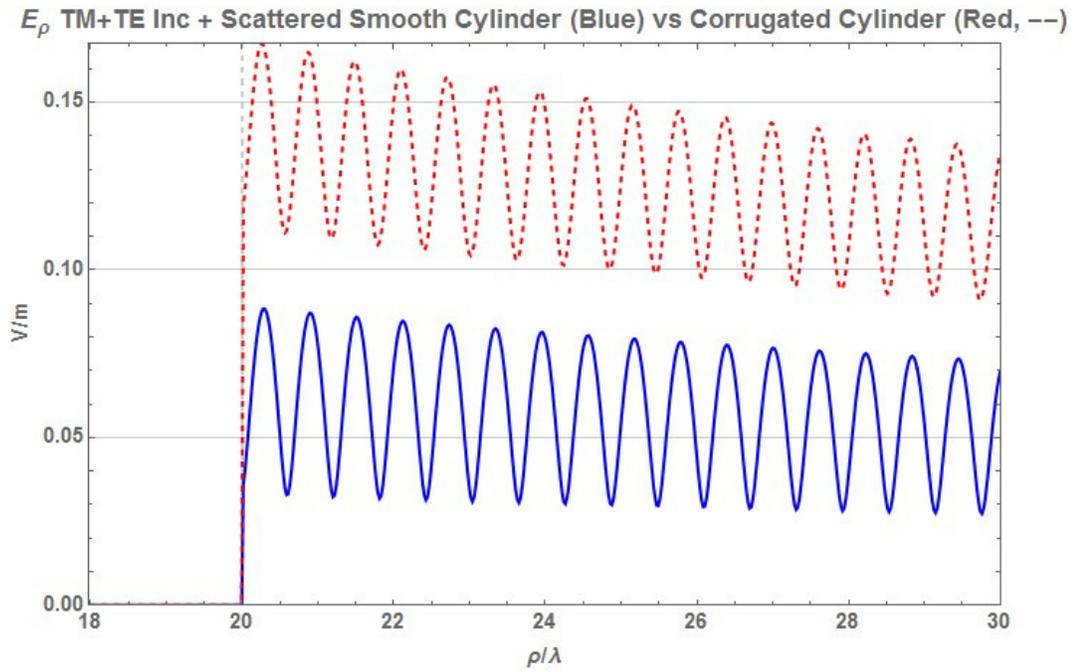


Figure 7-17 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

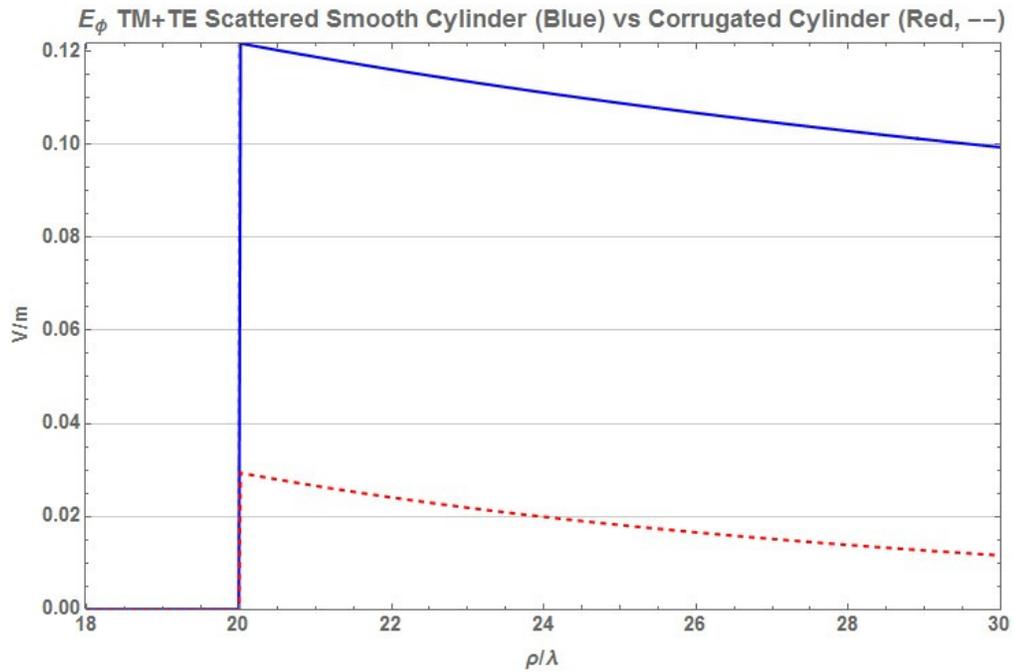


Figure 7-18 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

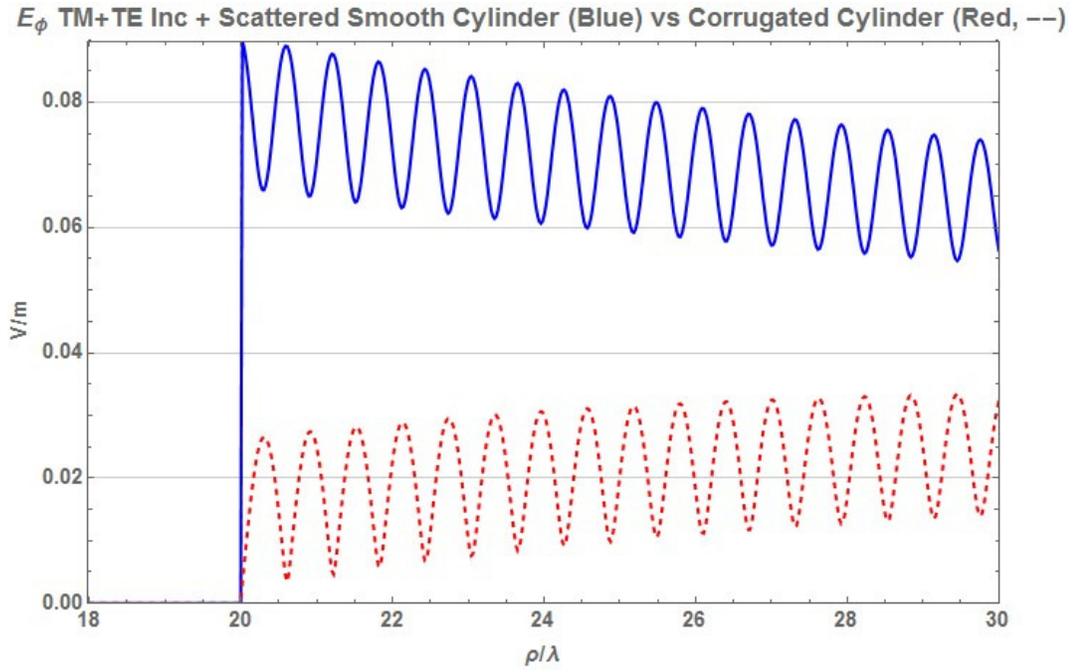


Figure 7-19 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

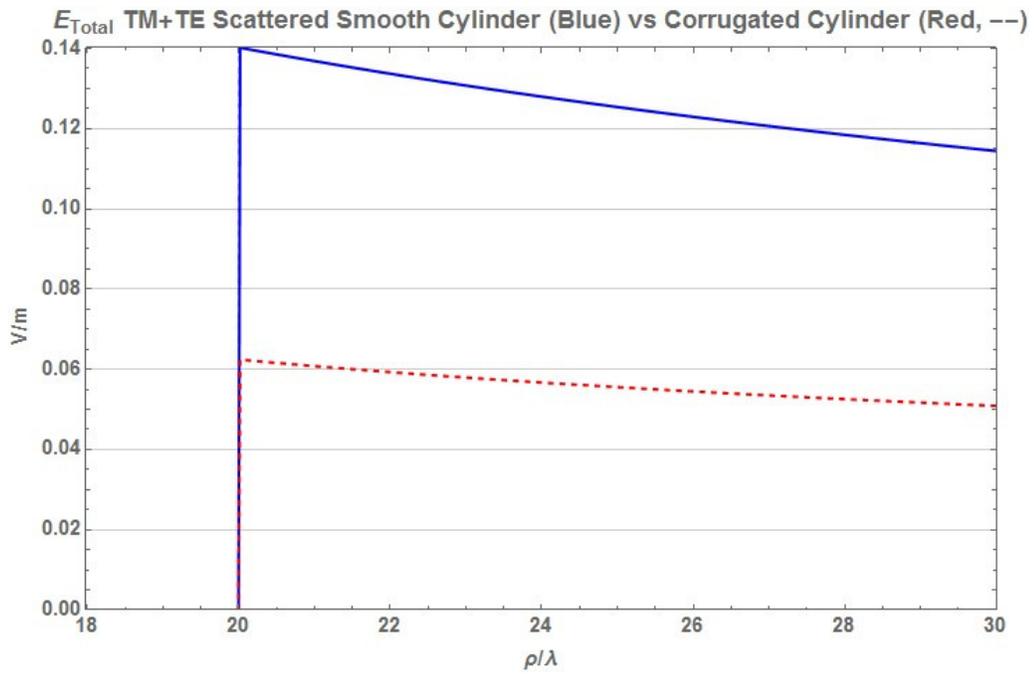


Figure 7-20 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

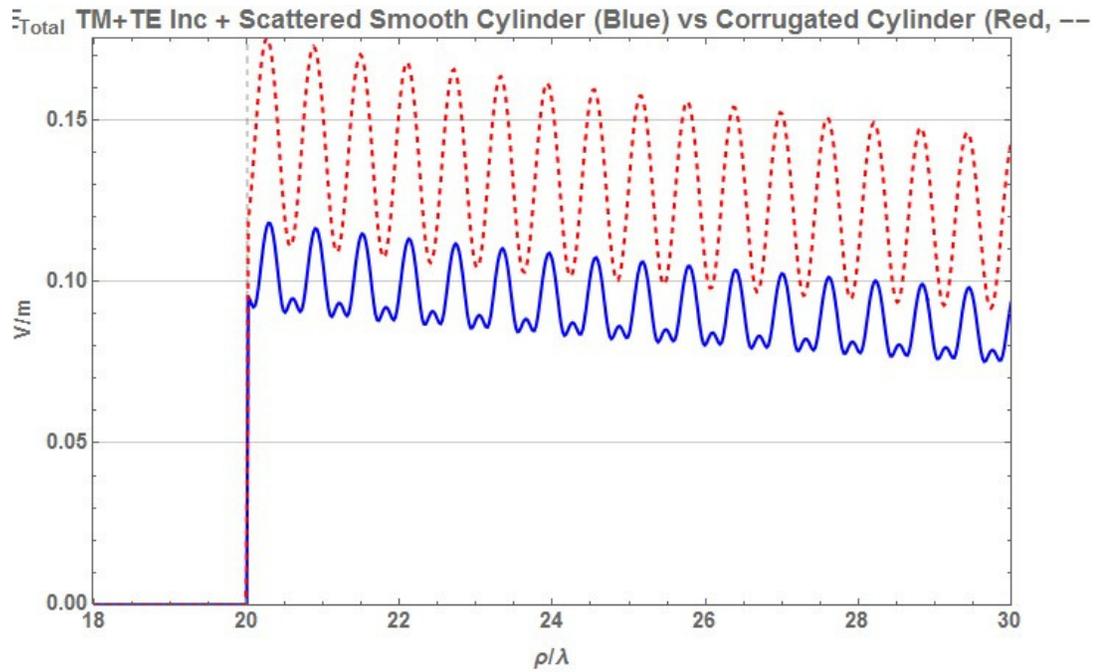


Figure 7-21 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.20.0.0

7.5.2 Run a.2.0.0 ($b=2\lambda$, $a=b*.001$, $\rho_2=2\lambda$, $m=0$)

Table 6 Detailed parameters summary for changing ϕ plots of Run a.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.002 λ	-	-	-	-
b	2. λ	-	-	-	-
ρ_1	1.998 λ	-	-	-	-
ρ_2	2. λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	20. λ	-	-	-	-
z (observed)	0.25 a && 0.0005 λ	-	-	-	-
Matching Points	-	-	-	-	7
ϕ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary a	-	-	-	-

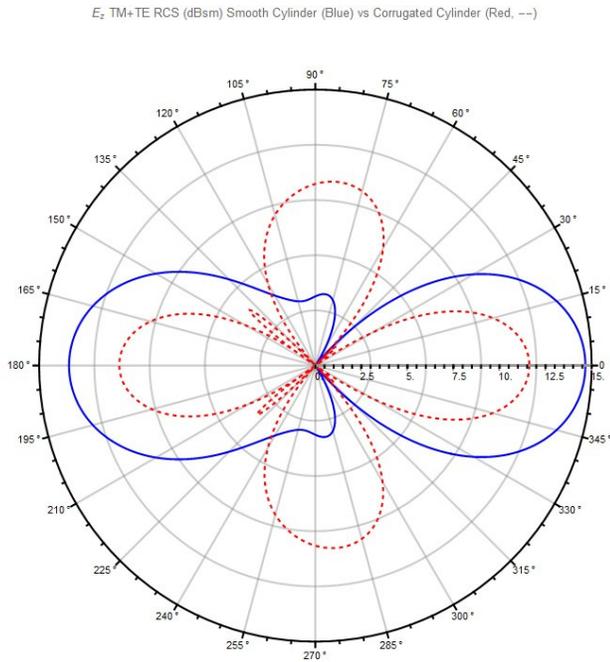


Figure 7-22 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0

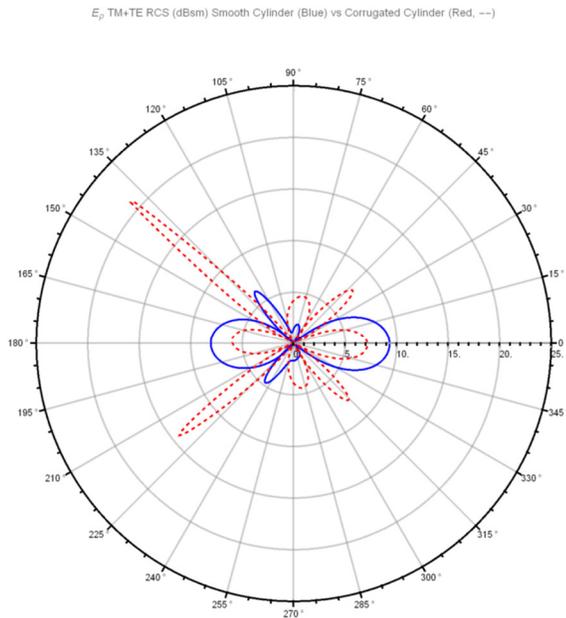


Figure 7-23 Polar Plot form of RCS dBsm for E_p of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0

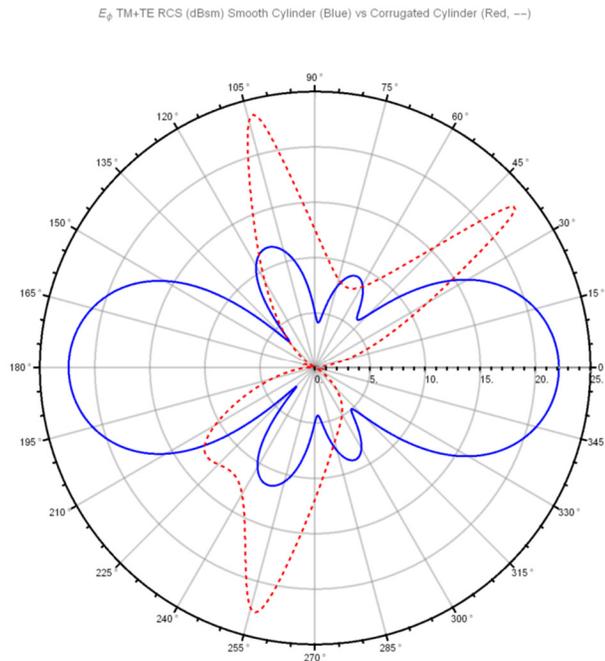


Figure 7-24 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.2.0.0

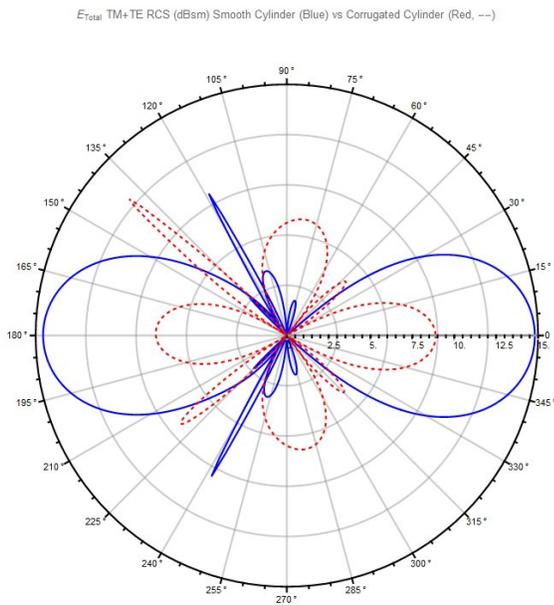


Figure 7-25 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

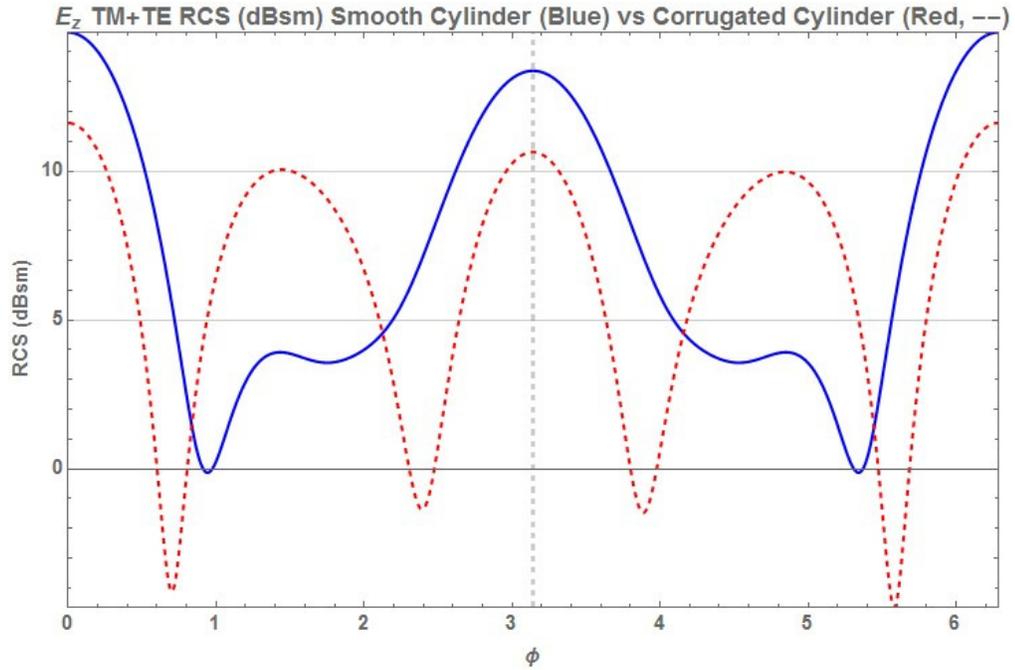


Figure 7-26 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

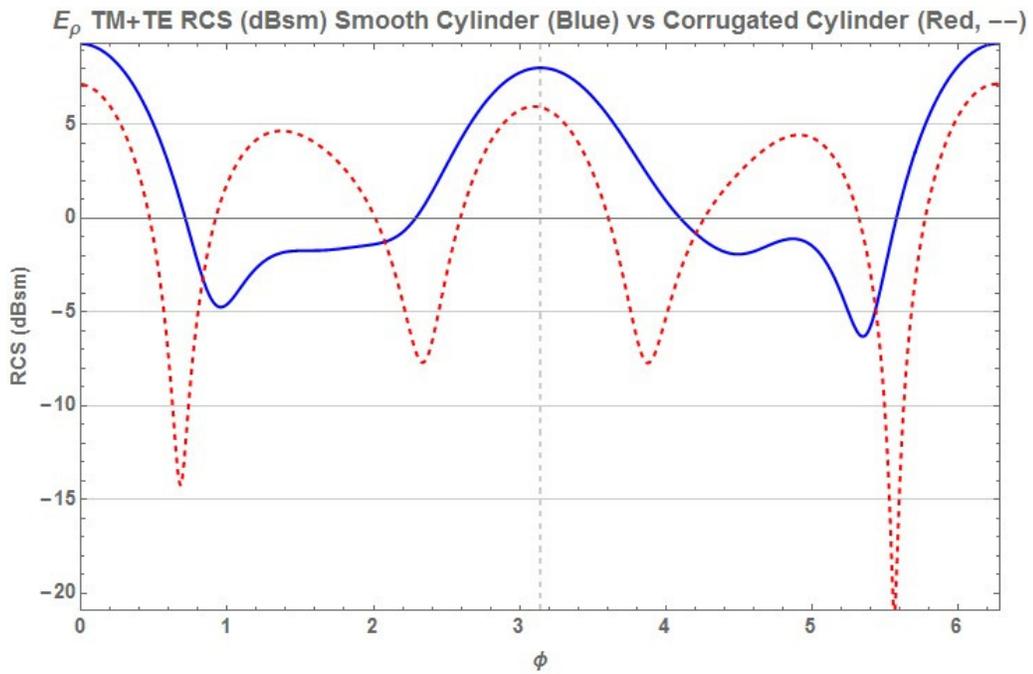


Figure 7-27 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

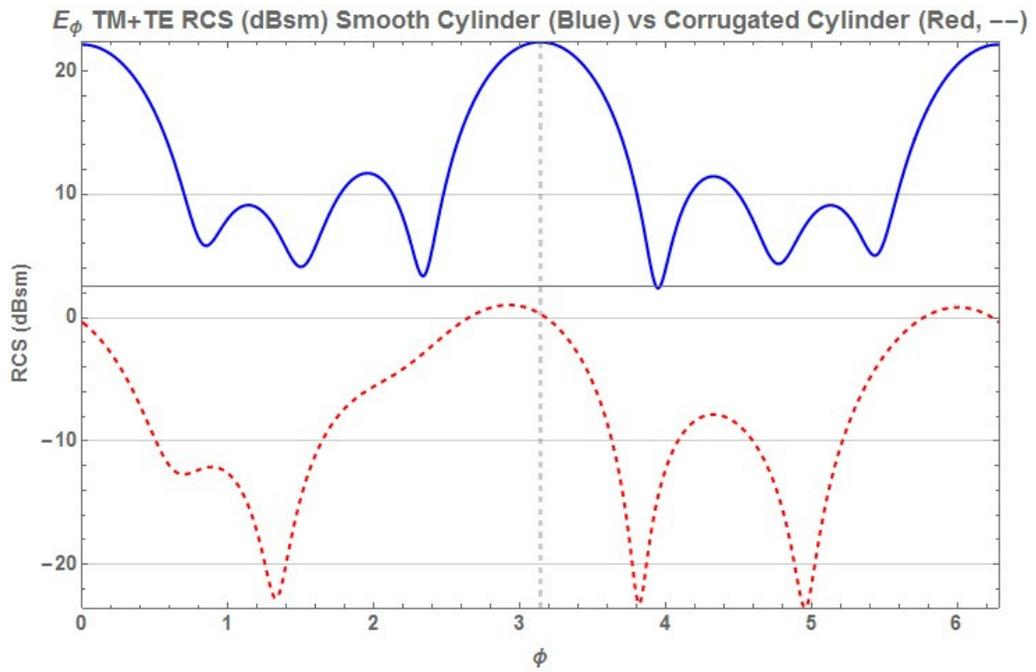


Figure 7-28 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

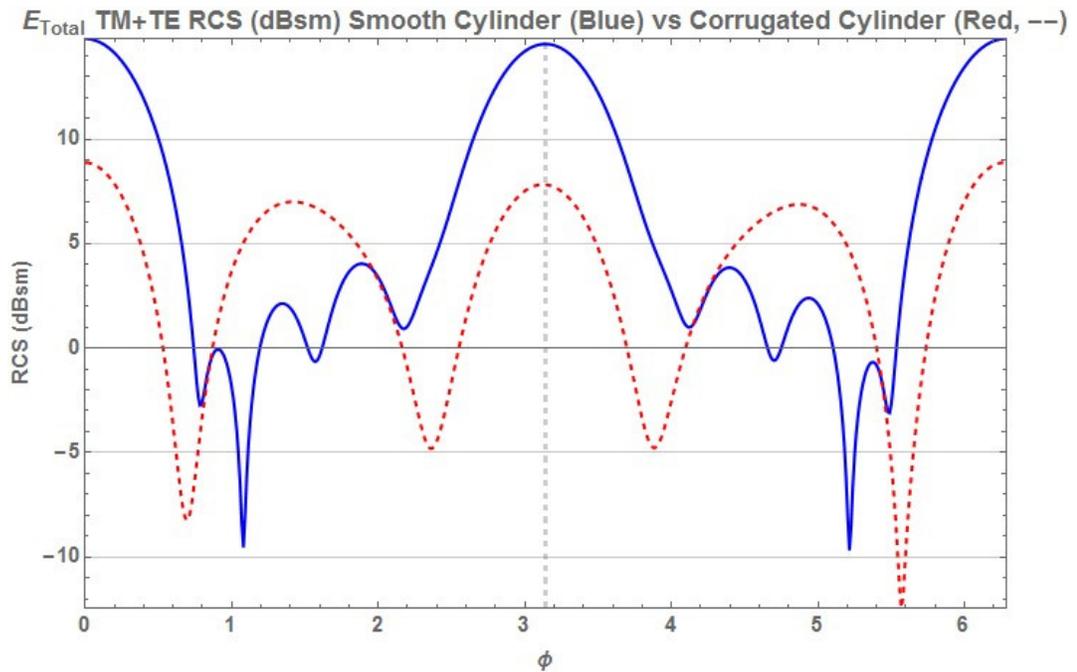


Figure 7-29 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

Table 7 Detailed parameters summary for changing ρ plots of Run a.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.002λ	-	-	-	-
b	$2. \lambda$	-	-	-	-
$\rho 1$	1.998λ	-	-	-	-
$\rho 2$	$2. \lambda$	-	-	-	-
ρ range	-	1.7982λ	$12. \lambda$	0.0185825λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$0.25 a \&\& 0.0005 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θi	55. Deg	-	-	-	-
ϕi	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary a	-	-	-	-

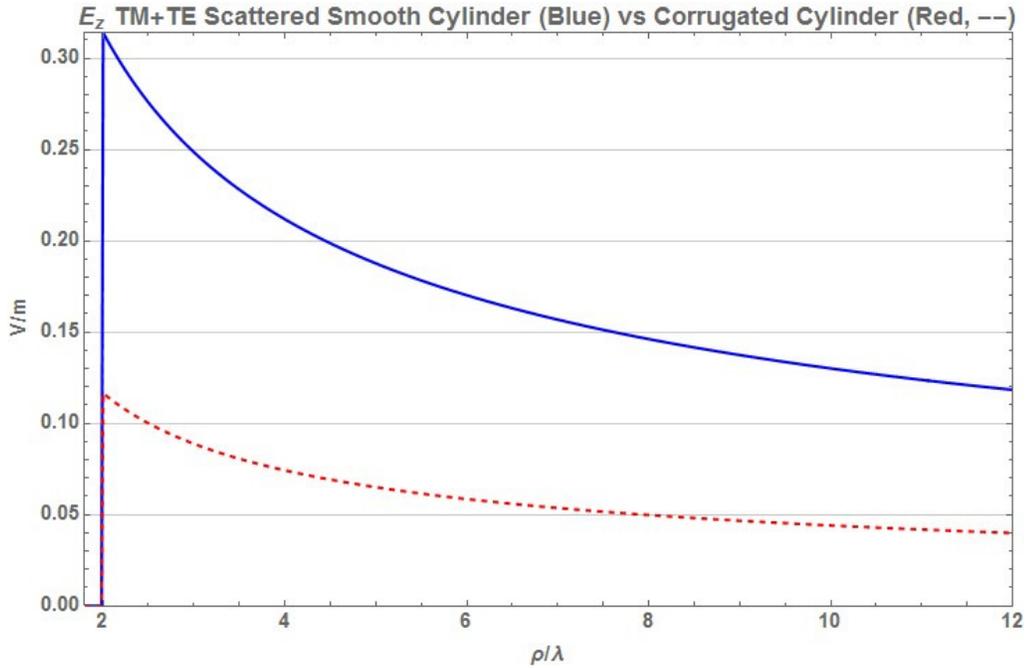


Figure 7-30 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

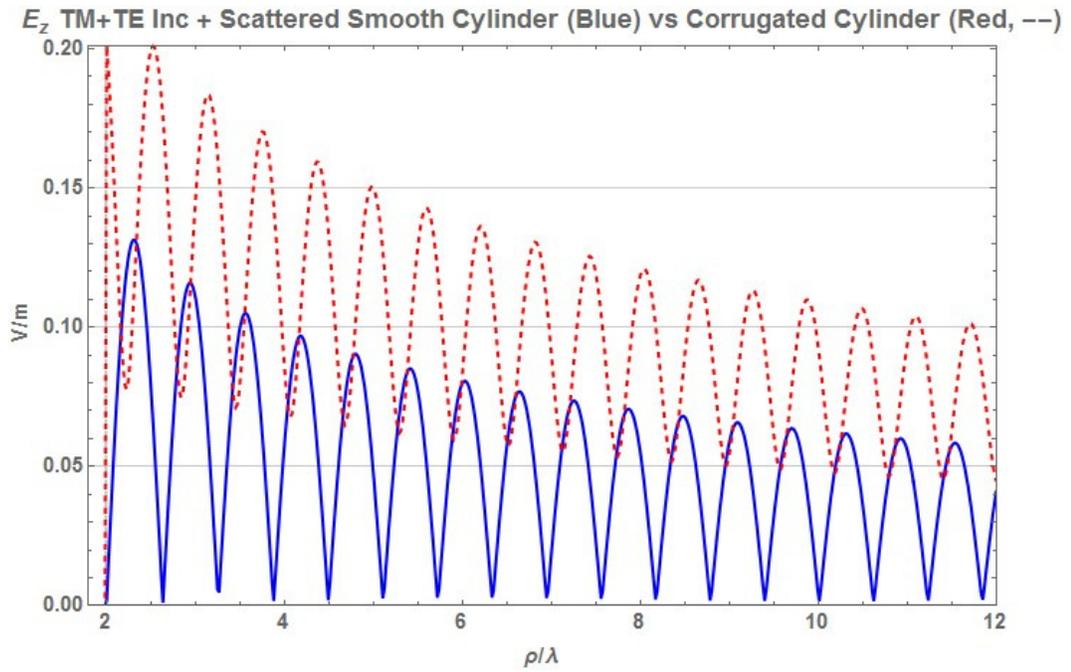


Figure 7-31 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

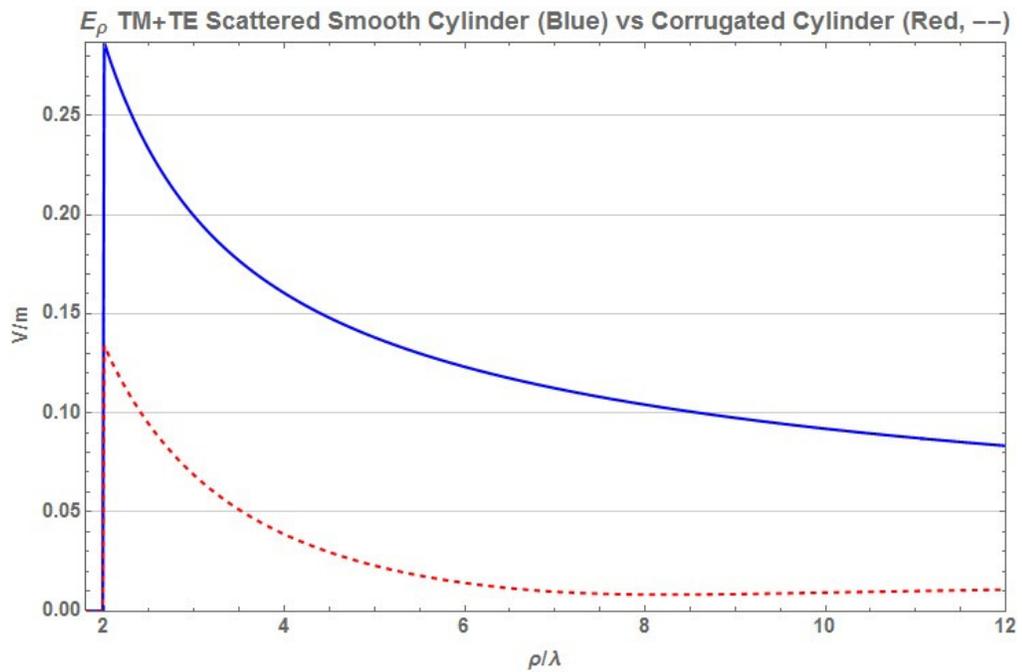


Figure 7-32 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

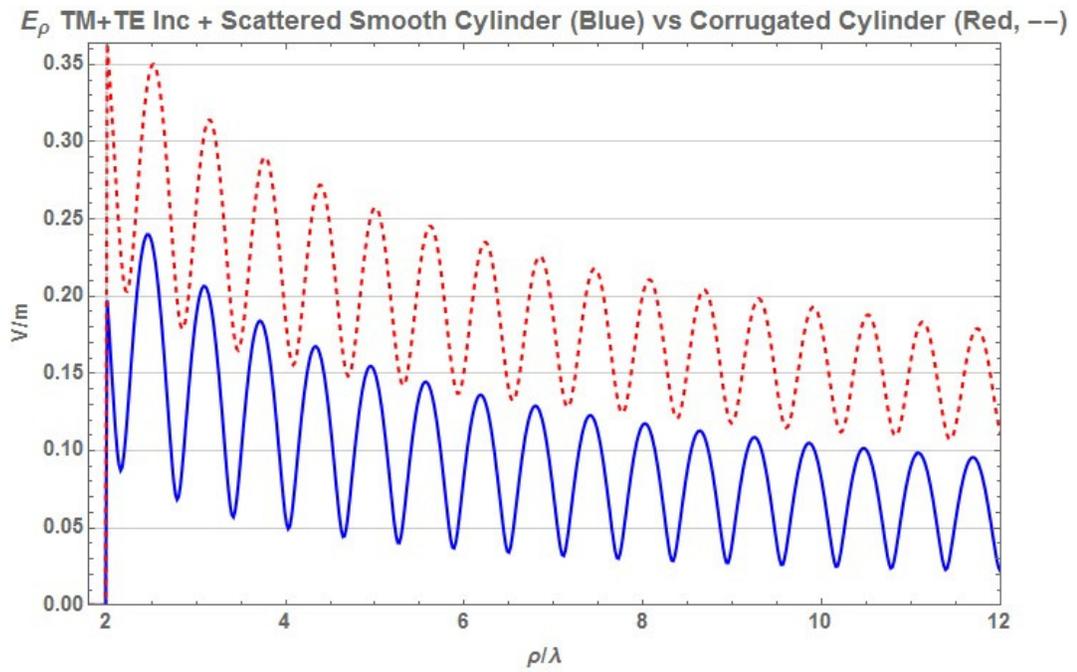


Figure 7-33 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

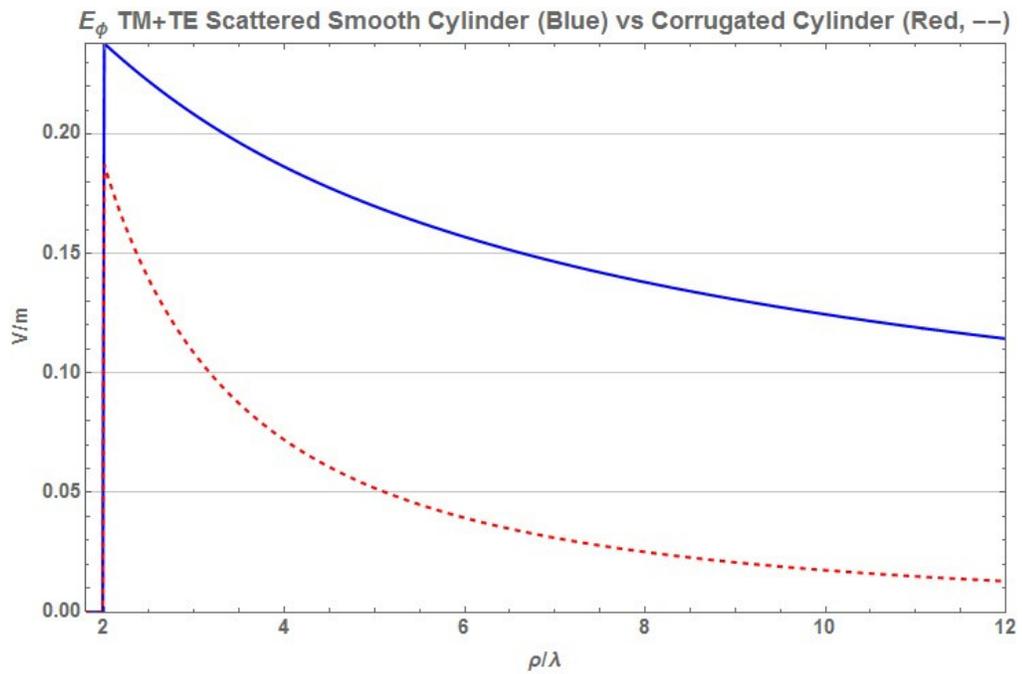


Figure 7-34 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

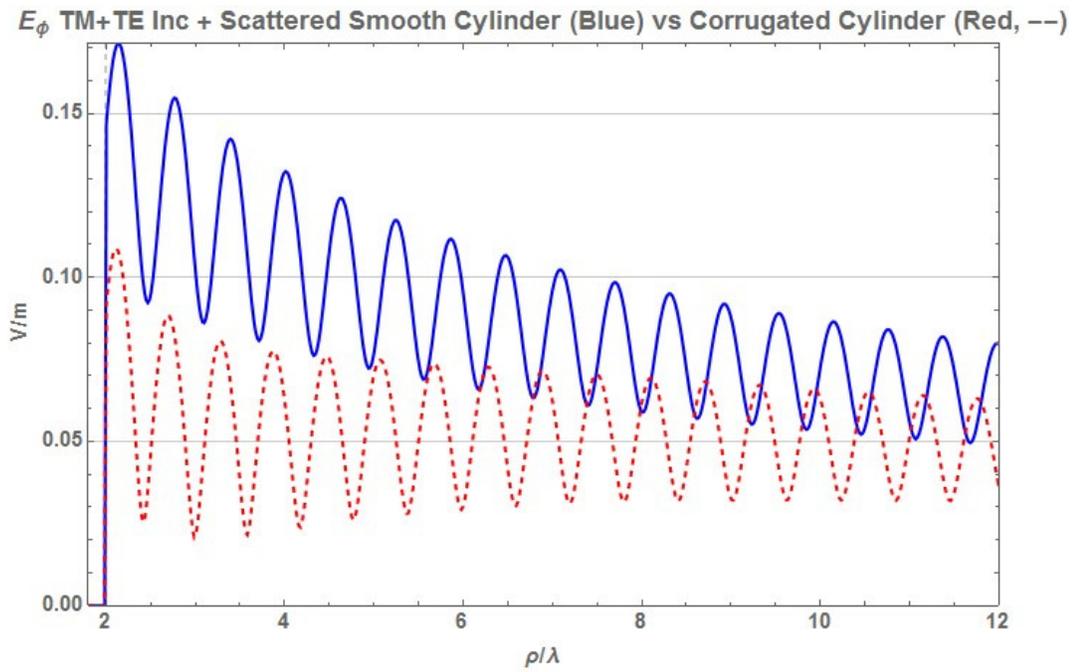


Figure 7-35 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

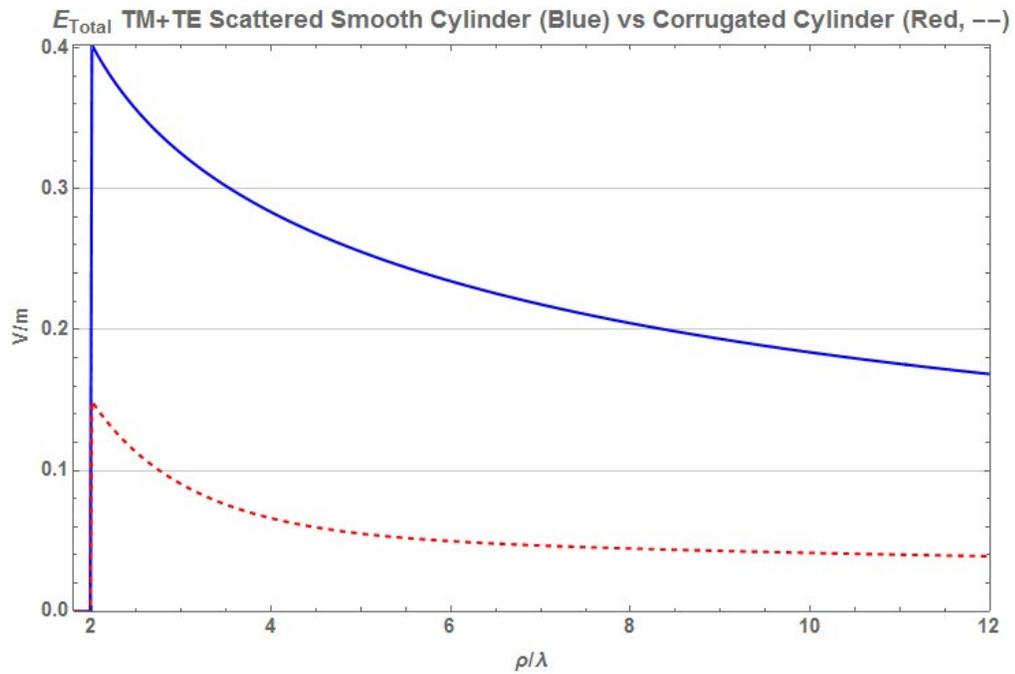


Figure 7-36 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

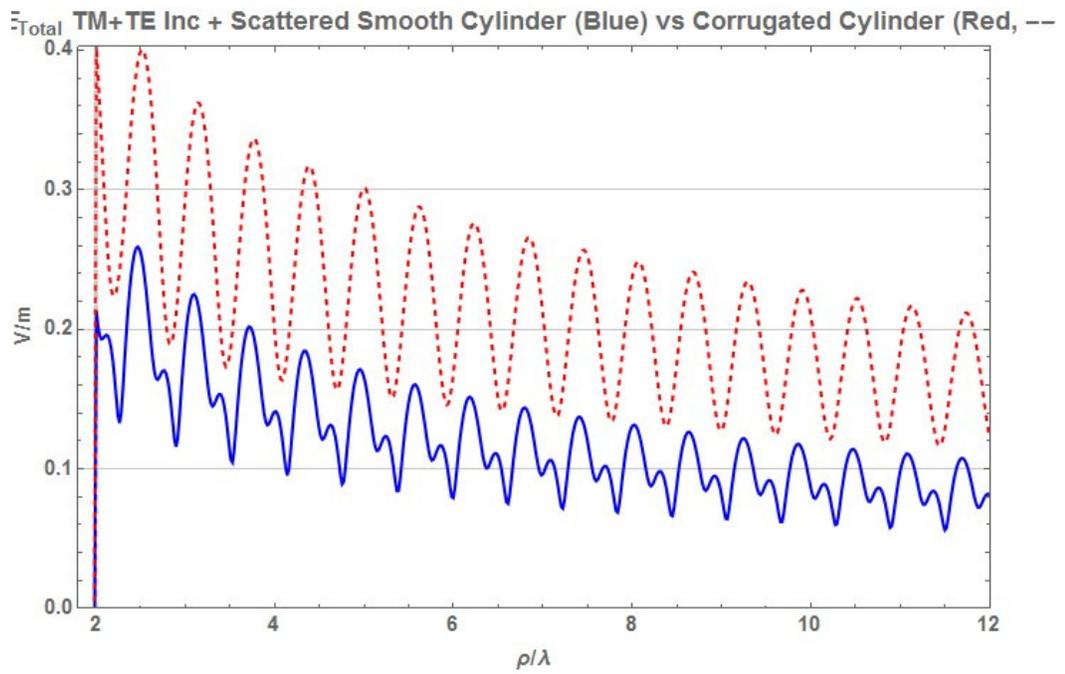


Figure 7-37 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.2.0.0

7.5.3 Run a.0.1.0.0 ($b=0.1\lambda$, $a=b*.001$, $\rho_2=0.1\lambda$, $m=0$)

Table 8 Detailed parameters summary for changing ϕ plots of Run a.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.0001 λ	-	-	-	-
b	0.1 λ	-	-	-	-
ρ_1	0.0999 λ	-	-	-	-
ρ_2	0.1 λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	1. λ	-	-	-	-
z (observed)	0.25 a && 0.000025 λ	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary a	-	-	-	-

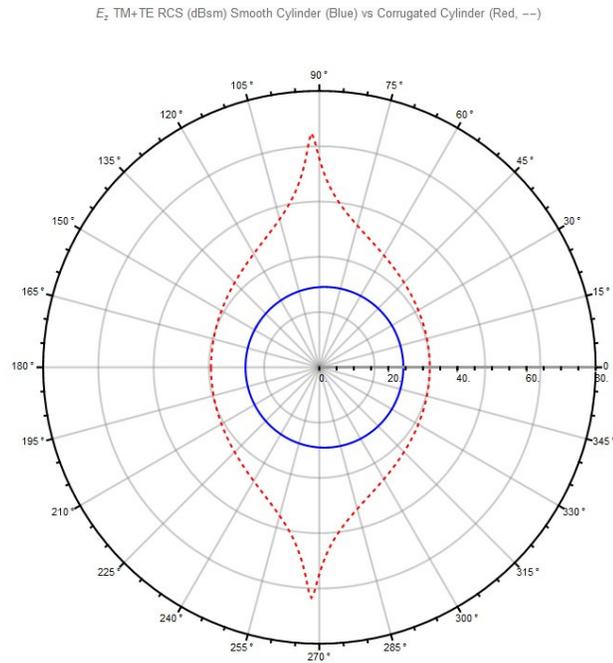


Figure 7-38 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

E_z TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

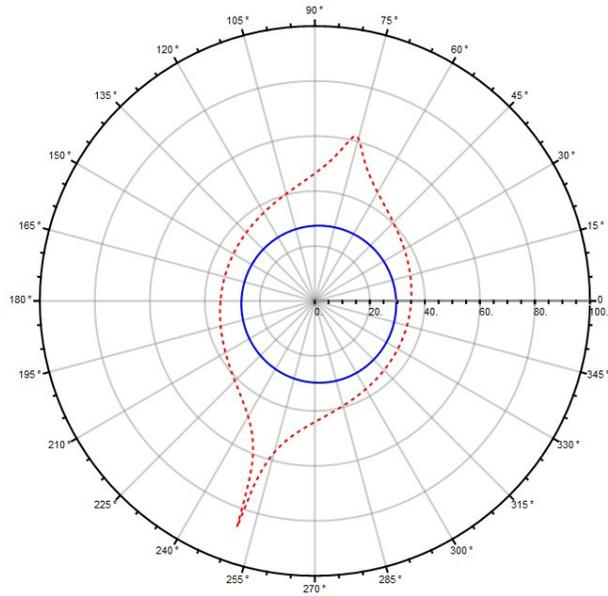


Figure 7-39 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

E_ϕ TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

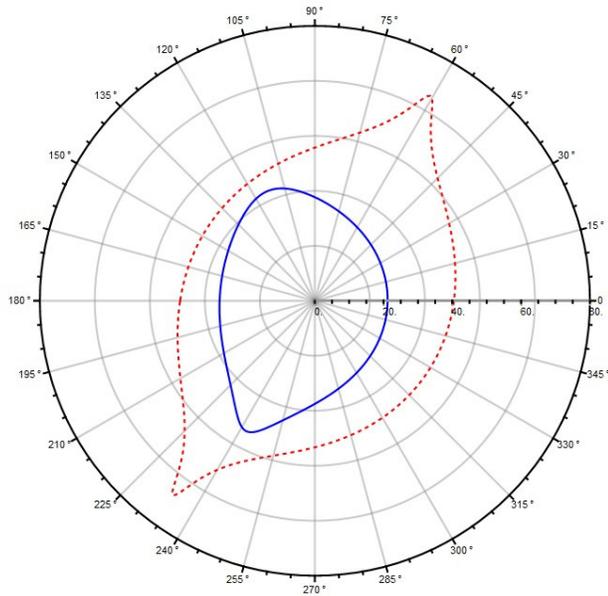


Figure 7-40 Polar Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

E_{Total} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

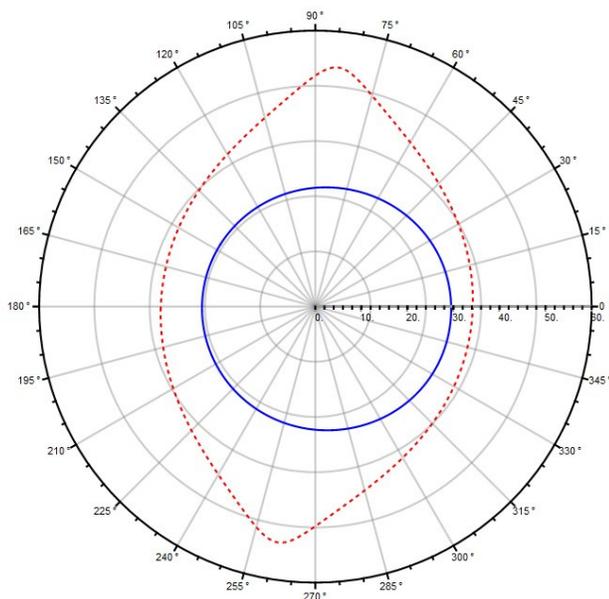


Figure 7-41 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

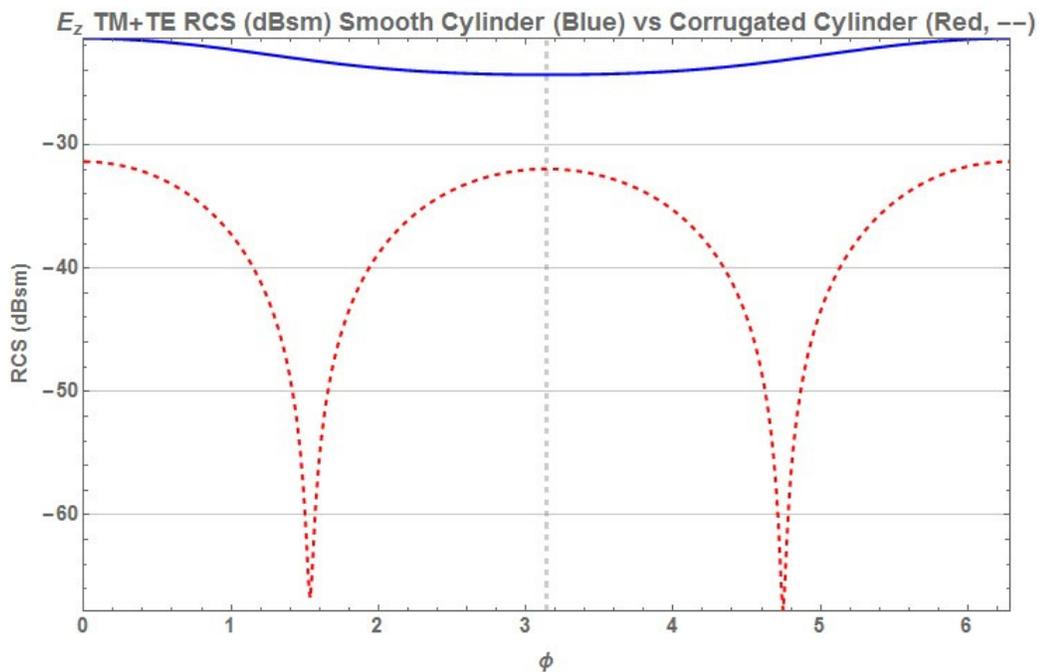


Figure 7-42 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

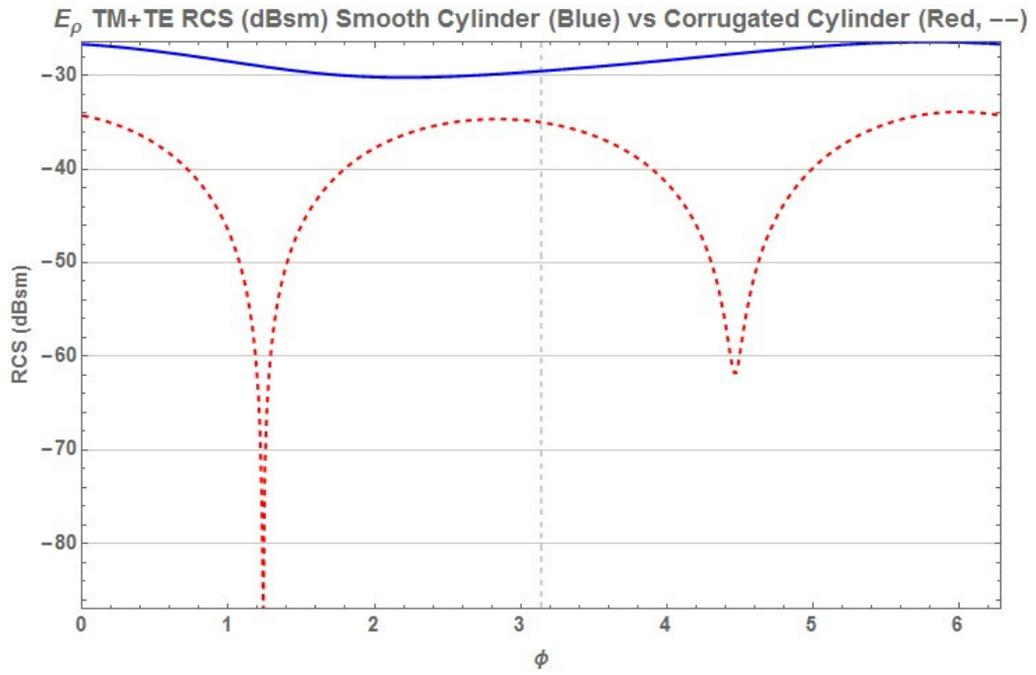


Figure 7-43 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

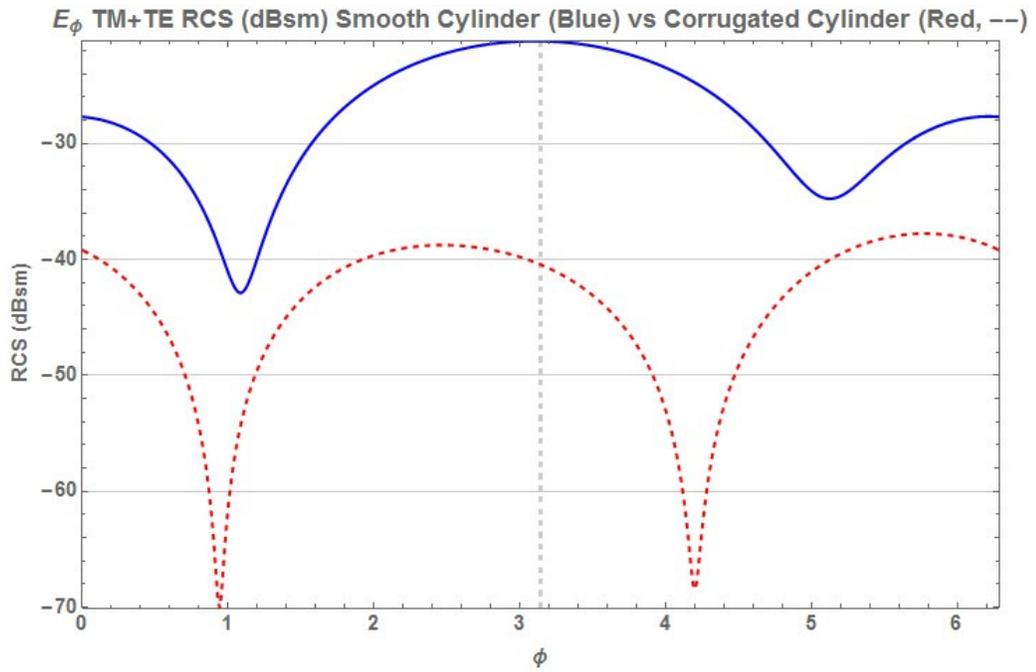


Figure 7-44 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

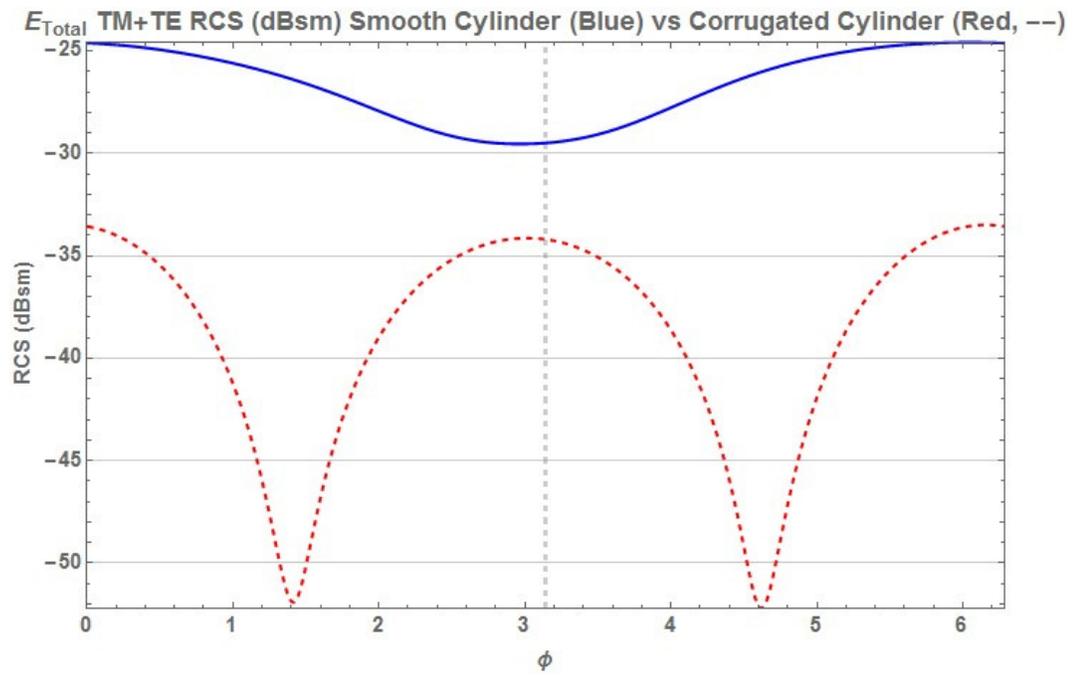


Figure 7-45 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.1.0.0

Table 9 Detailed parameters summary for changing ρ plots of Run a.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.0001 λ	-	-	-	-
b	0.1 λ	-	-	-	-
ρ_1	0.0999 λ	-	-	-	-
ρ_2	0.1 λ	-	-	-	-
ρ range	-	0.08991 λ	10.1 λ	0.0182333 λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	0.25 a && 0.000025 λ	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary a	-	-	-	-

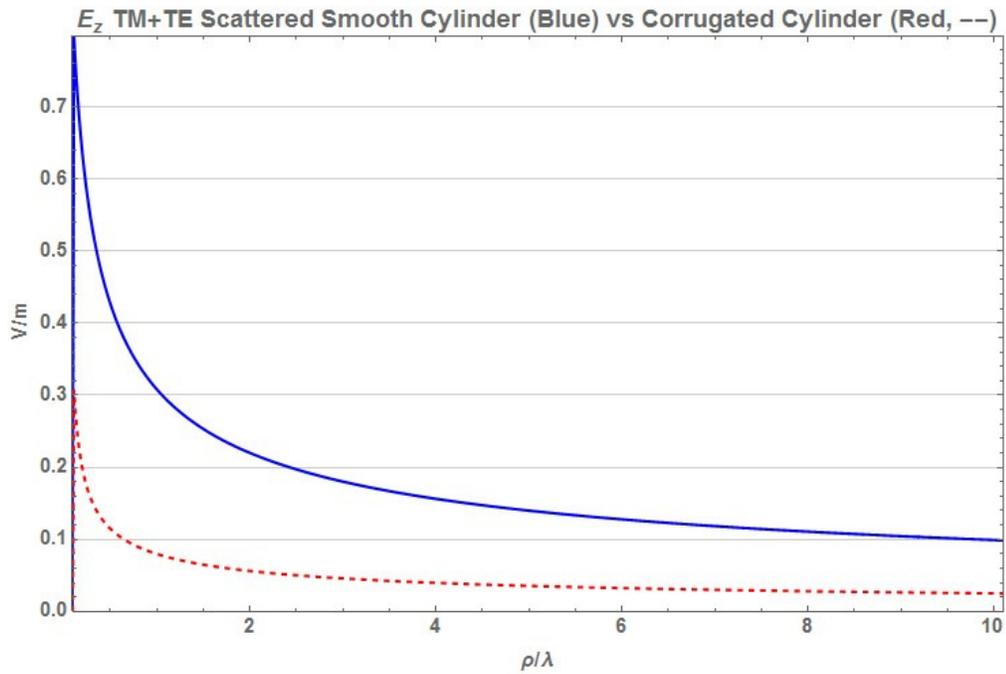


Figure 7-46 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

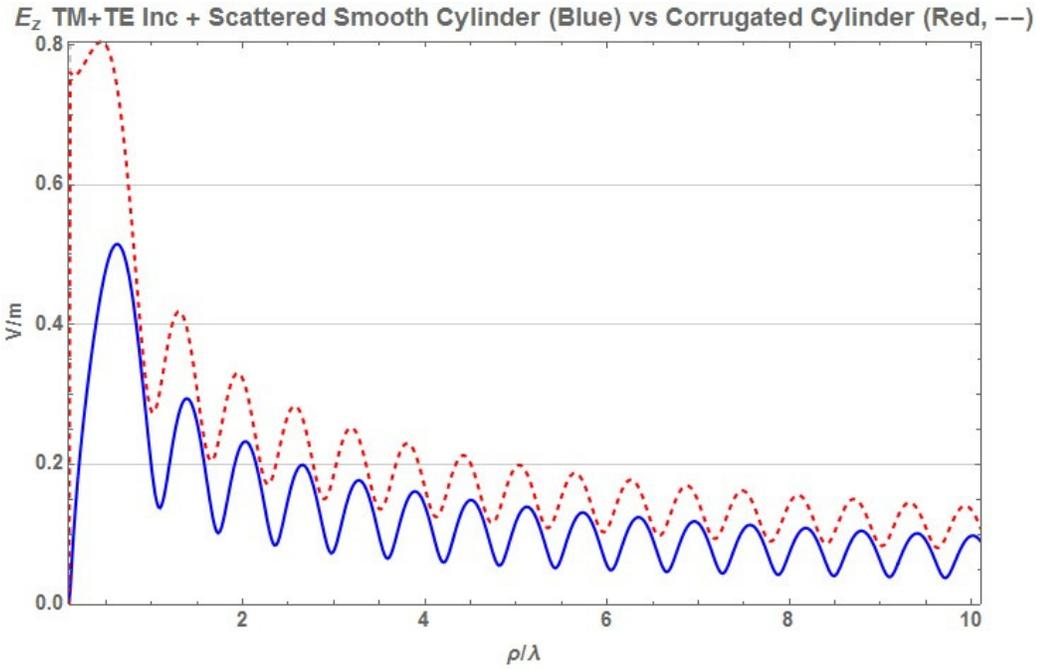
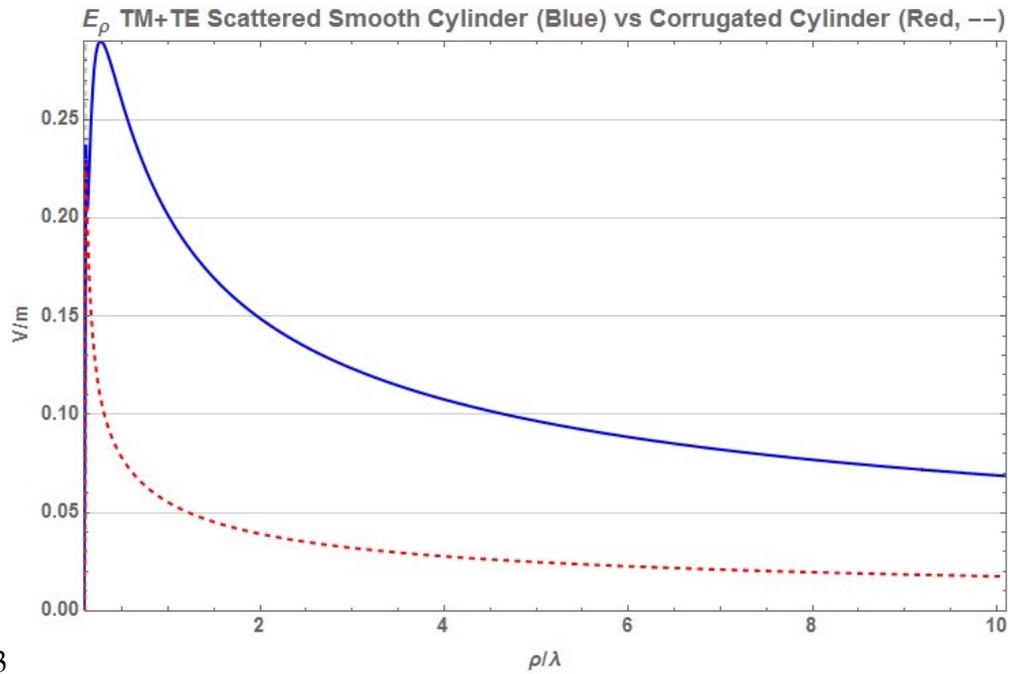


Figure 7-47 XY Plot of Scattered + Incident Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0



3

Figure 7-48 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

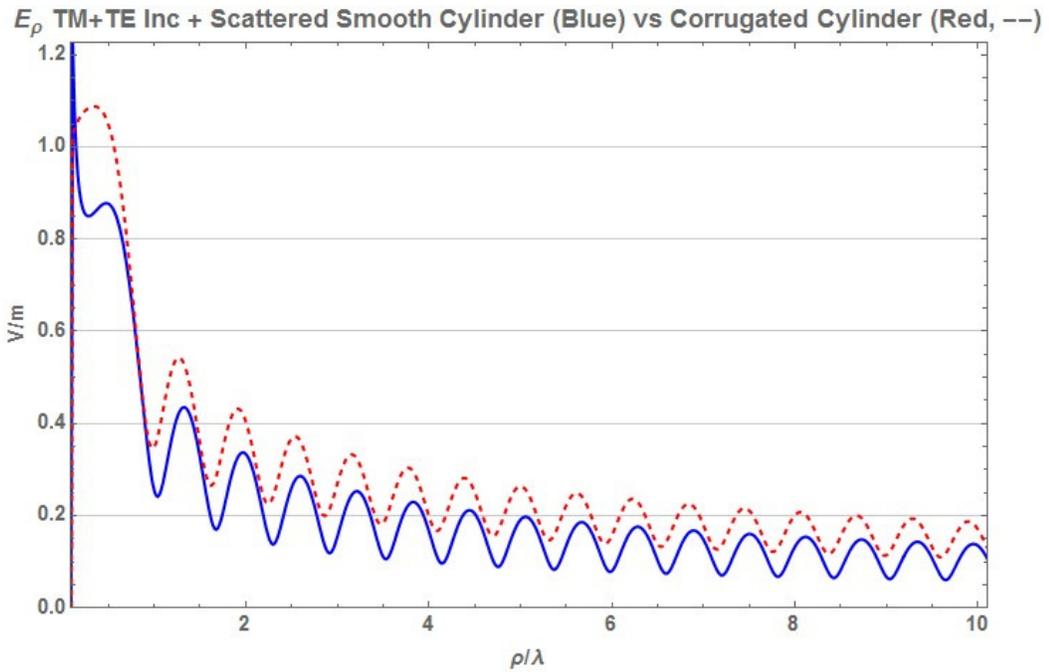


Figure 7-49 XY Plot of Scattered + Incident Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

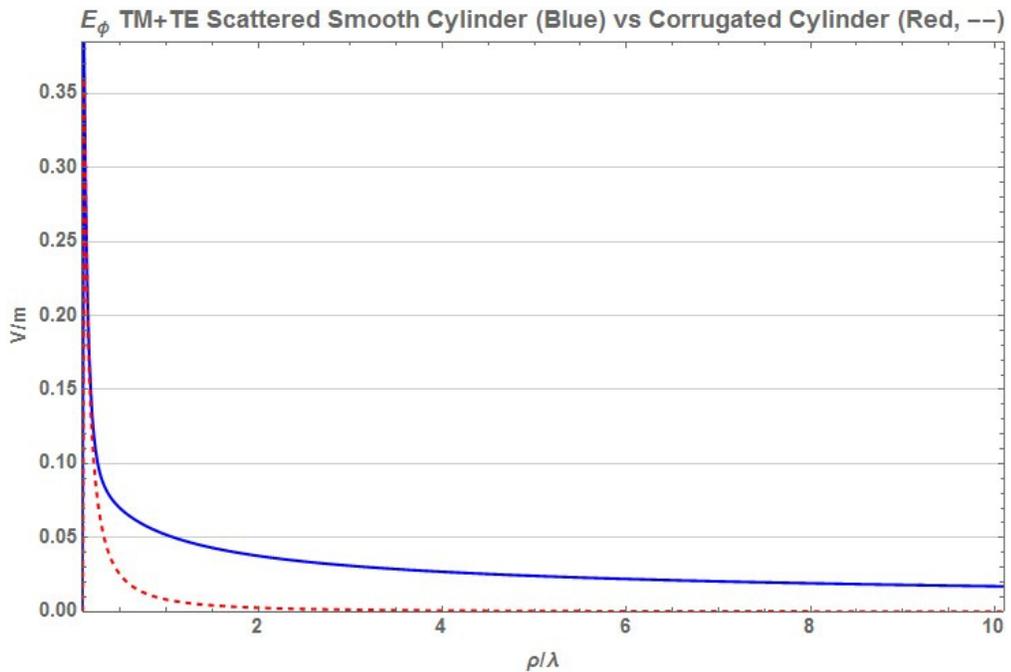


Figure 7-50 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

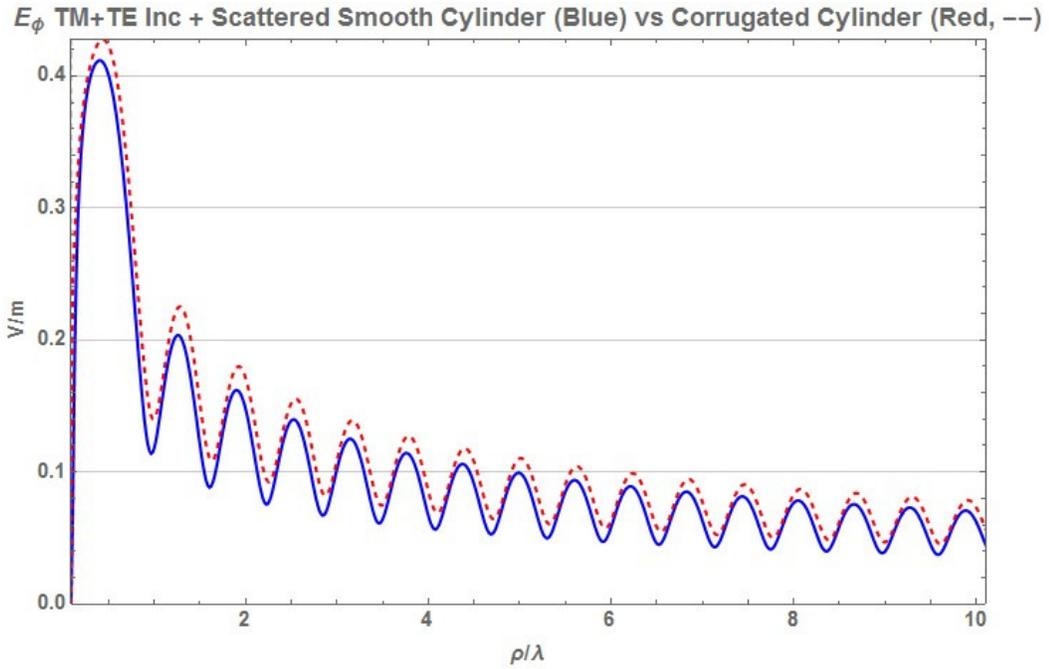


Figure 7-51 XY Plot of Scattered + Incident Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

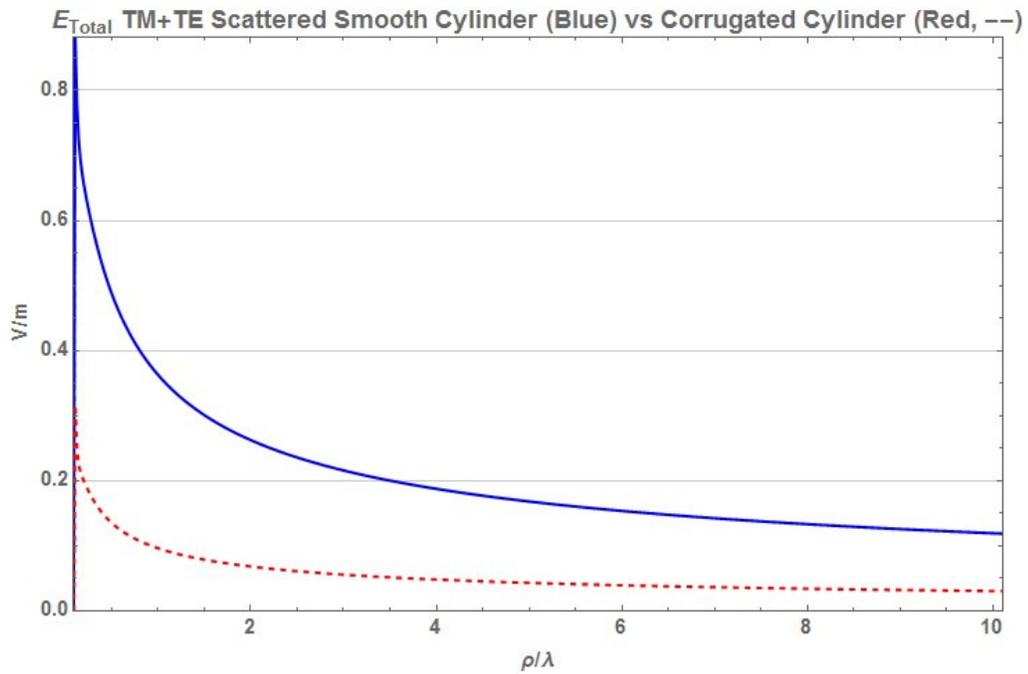


Figure 7-52 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

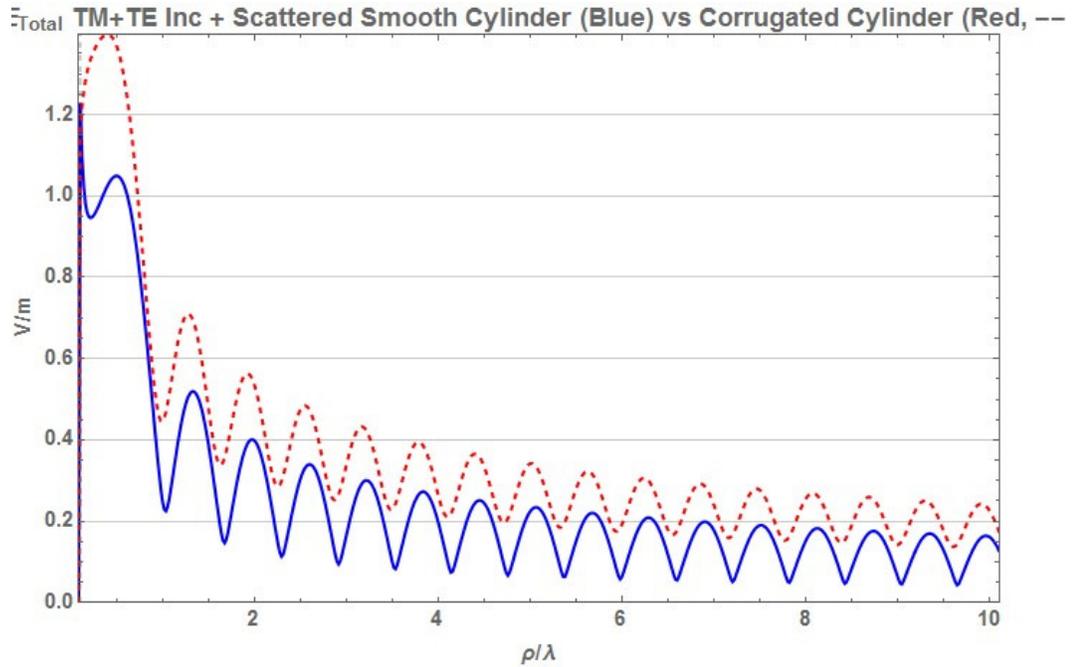


Figure 7-53 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a.0.10.0.0

7.5.4 Run b.20.0.0 ($b=20\lambda$, $a=b*.001$, $\rho_2=20\lambda$, $m=0$)

Table 10 Detailed parameters summary for changing ϕ plots of Run b.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.02λ	-	-	-	-
b	$20. \lambda$	-	-	-	-
ρ_1	19.98λ	-	-	-	-
ρ_2	$20. \lambda$	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	$200. \lambda$	-	-	-	-
z (observed)	$500.5 a \&\& 10.01 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
ϕ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary b	-	-	-	-

E_z TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, - -)

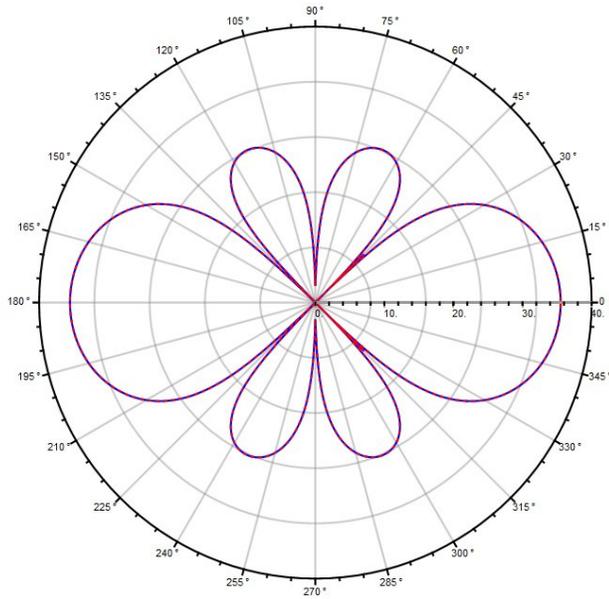


Figure 7-54 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0

E_p TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, - -)

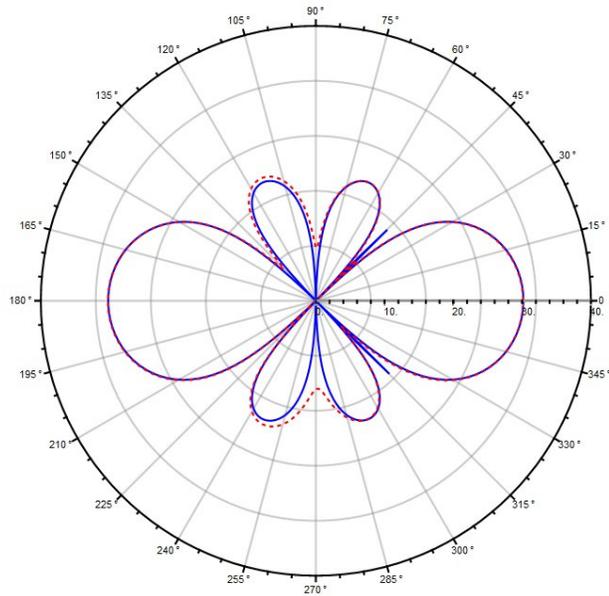


Figure 7-55 Polar Plot form of RCS dBsm for E_p of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0

E_{ϕ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

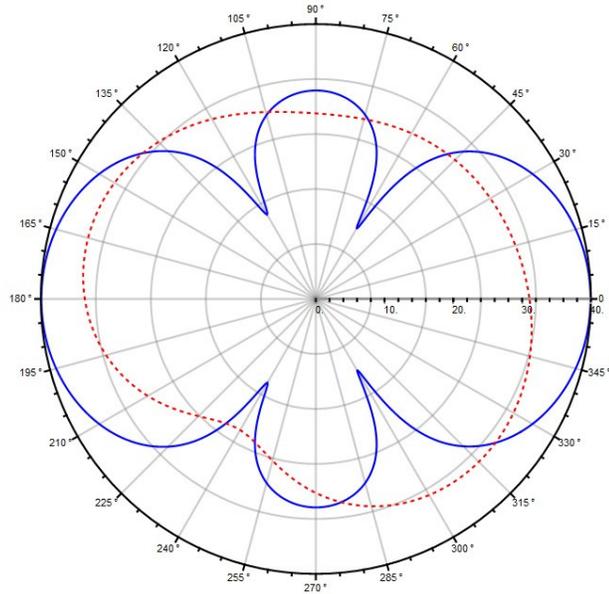


Figure 7-56 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.20.0.0

E_{Total} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

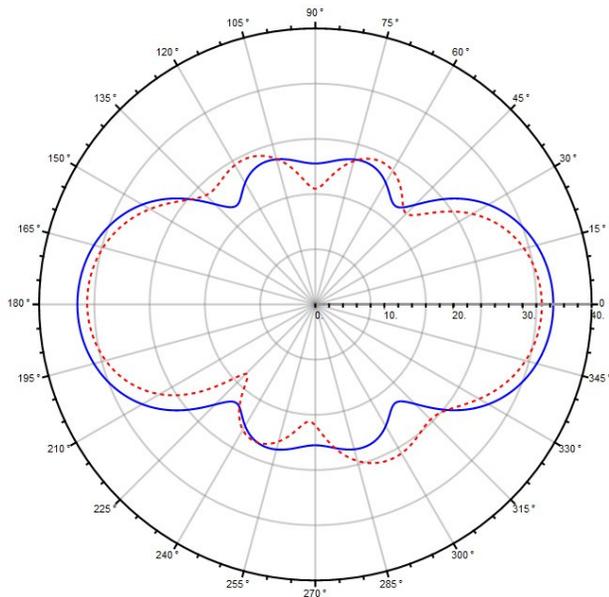


Figure 7-57 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

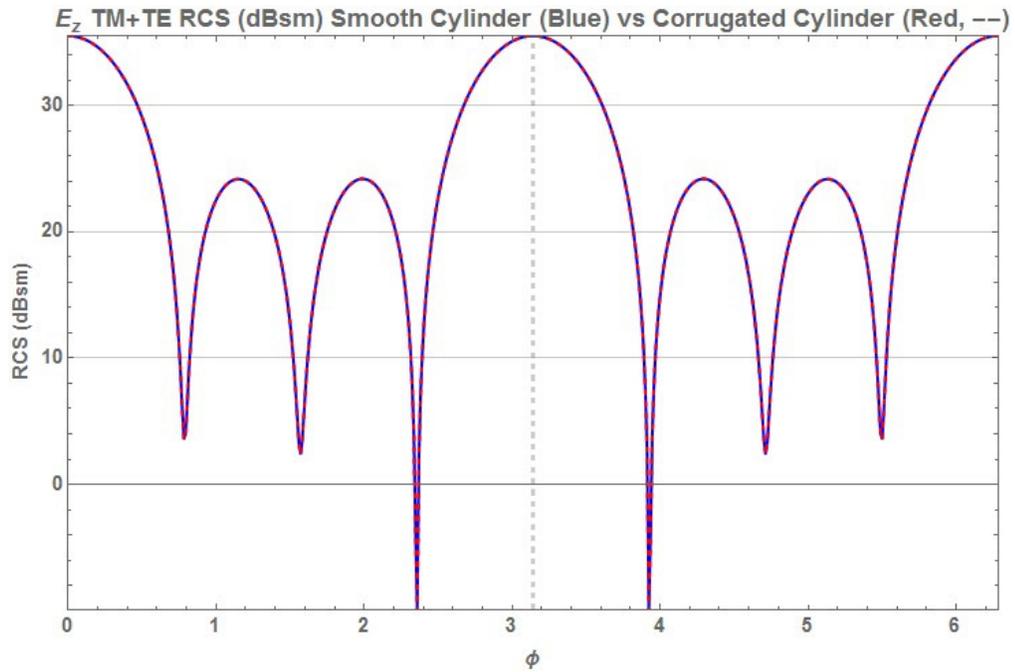


Figure 7-58 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

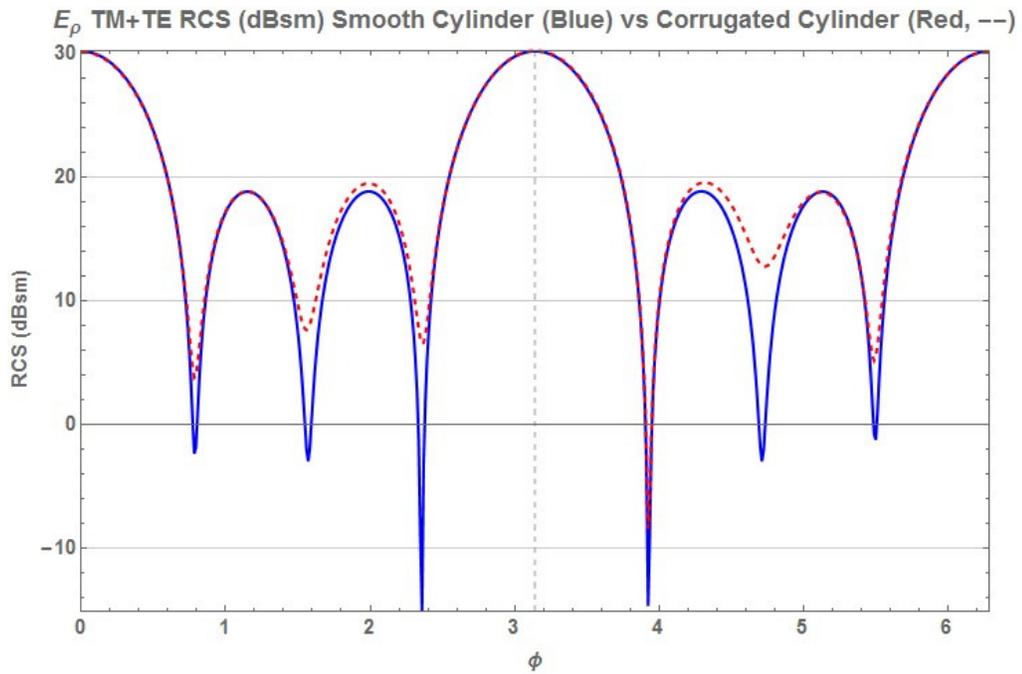


Figure 7-59 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

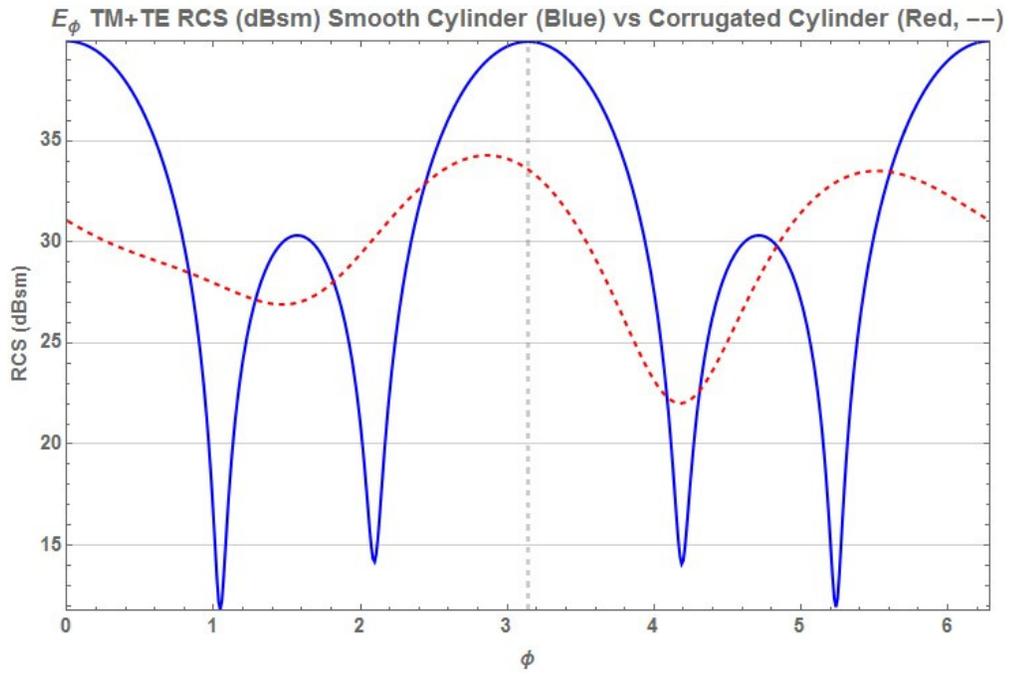


Figure 7-60 XY Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

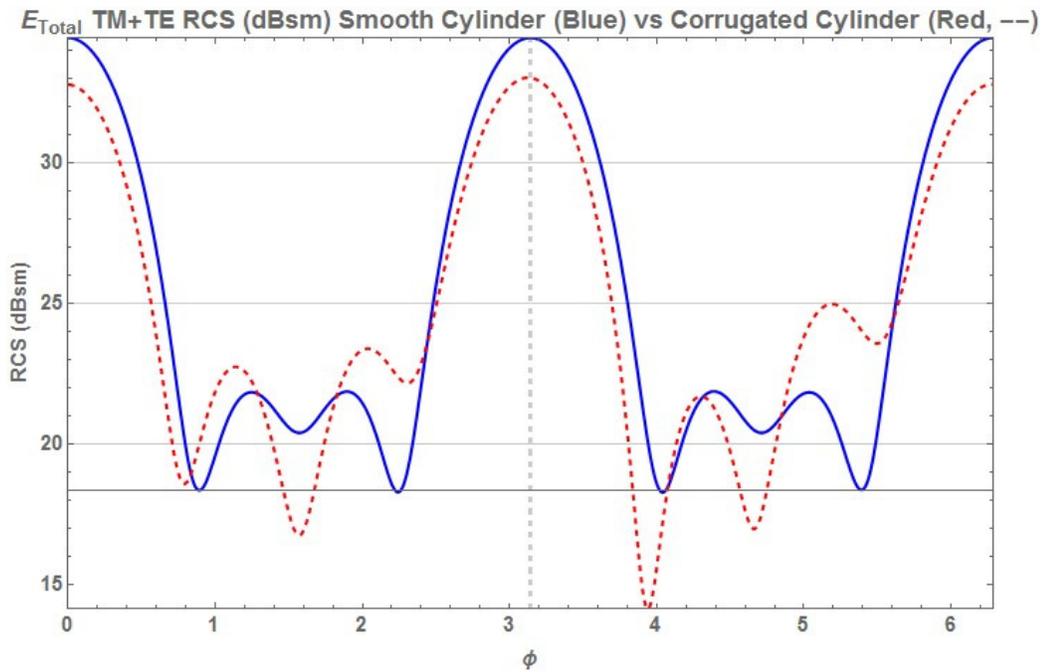


Figure 7-61 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

Table 11 Detailed parameters summary for changing ρ plots of Run b.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.02λ	-	-	-	-
b	$20. \lambda$	-	-	-	-
$\rho 1$	19.98λ	-	-	-	-
$\rho 2$	$20. \lambda$	-	-	-	-
ρ range	-	17.982λ	$30. \lambda$	0.0218907λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$500.5 a \&\& 10.01 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
ϕi	55. Deg	-	-	-	-
ϕi	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary b	-	-	-	-



Figure 7-62 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

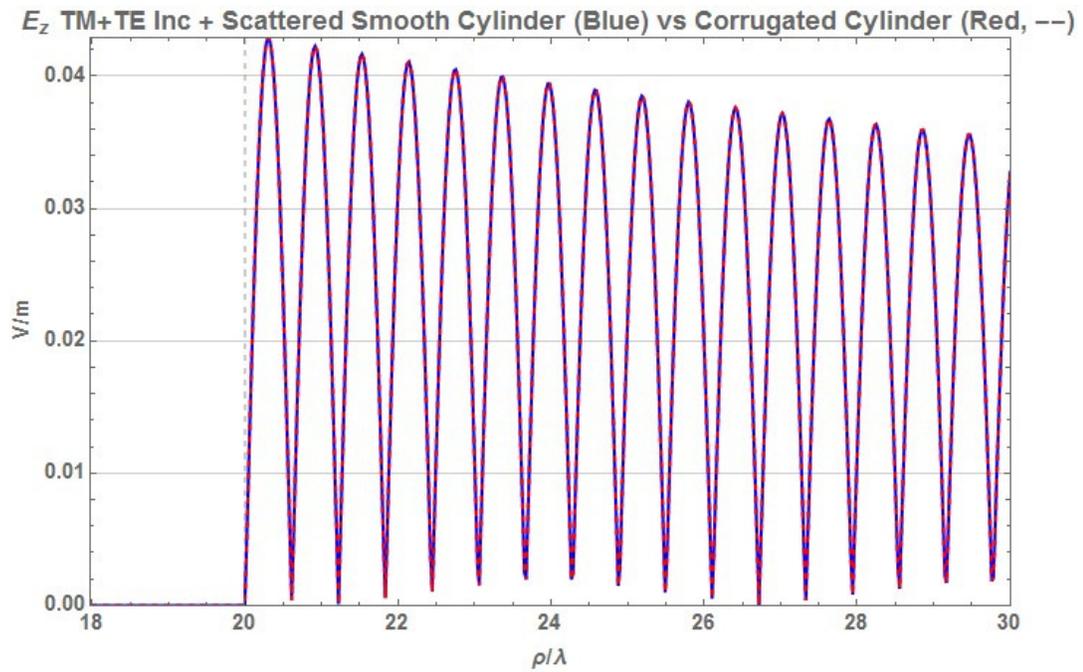


Figure 7-63 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

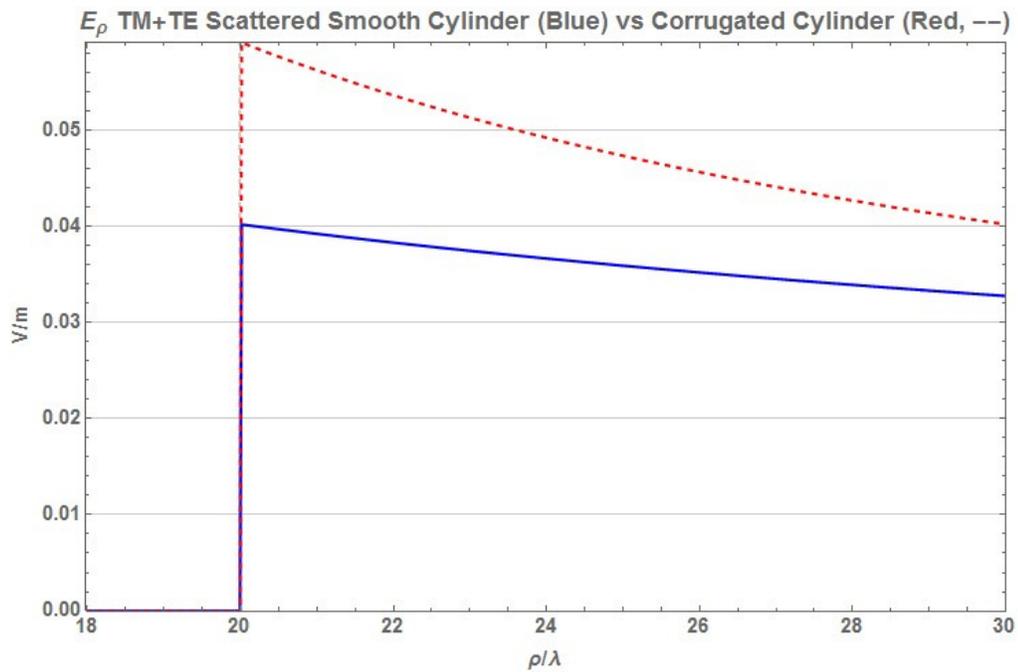


Figure 7-64 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

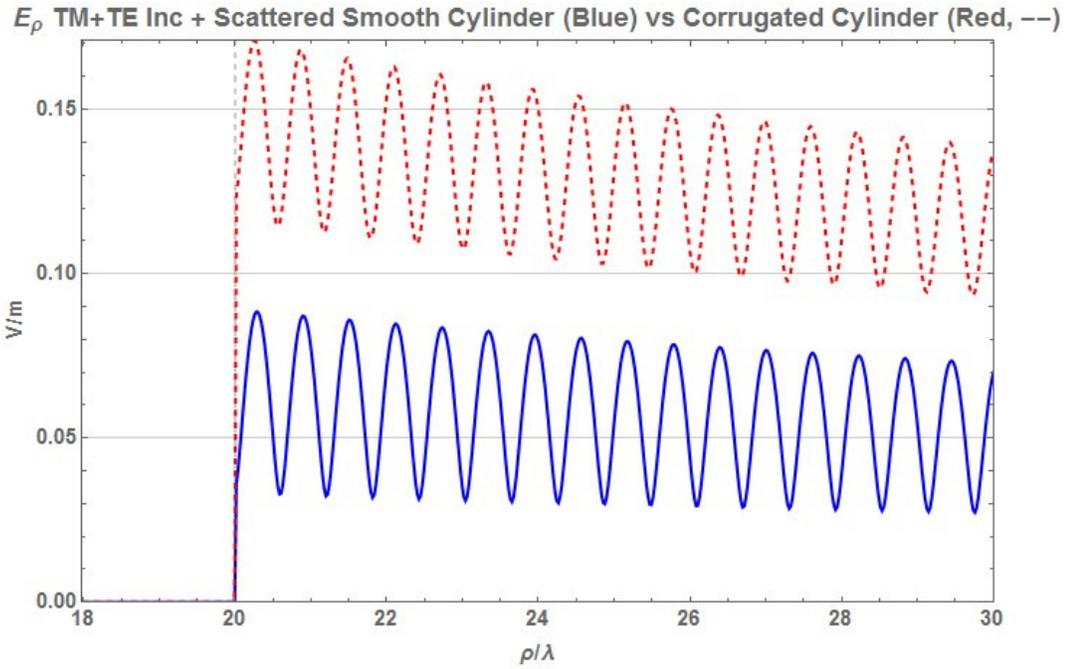


Figure 7-65 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

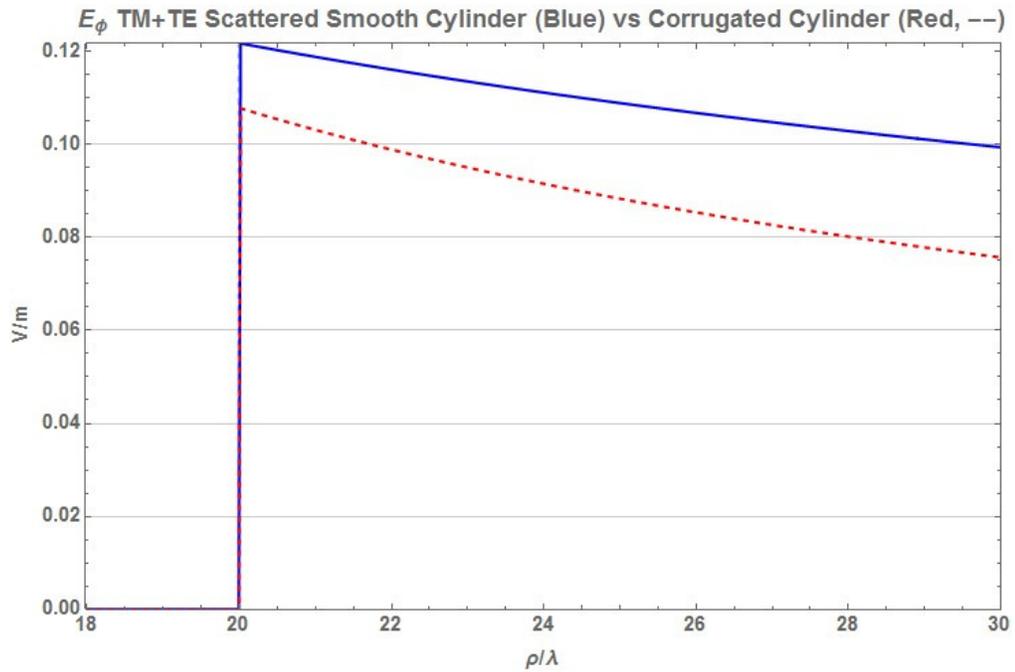


Figure 7-66 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

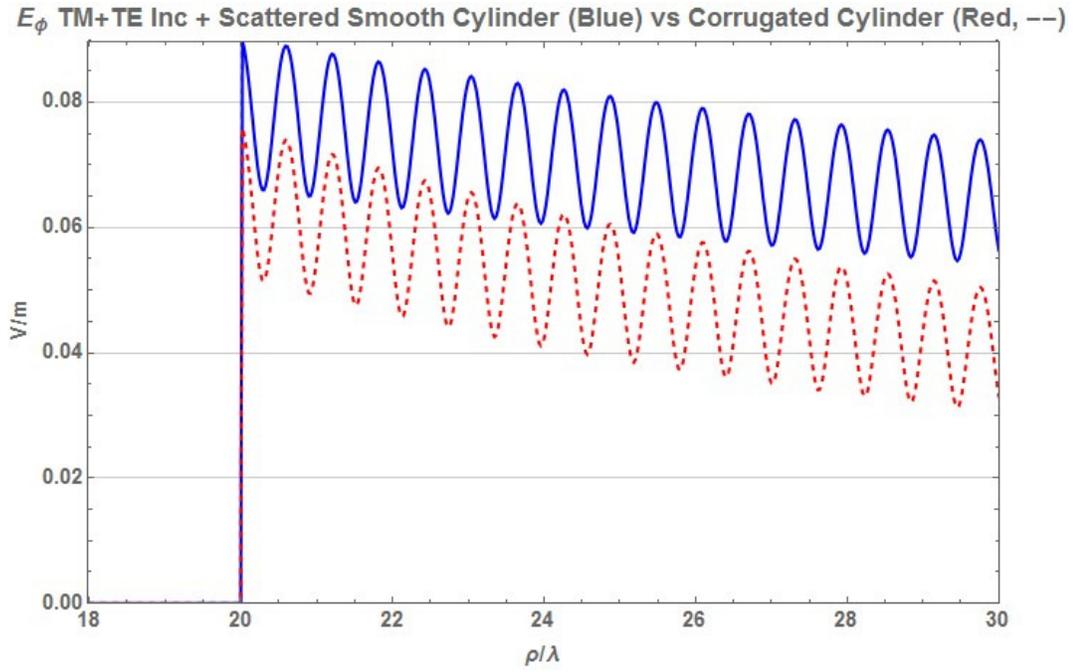


Figure 7-67 XY Plot of Scattered + Incident Field Amplitude, for E_{ϕ} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

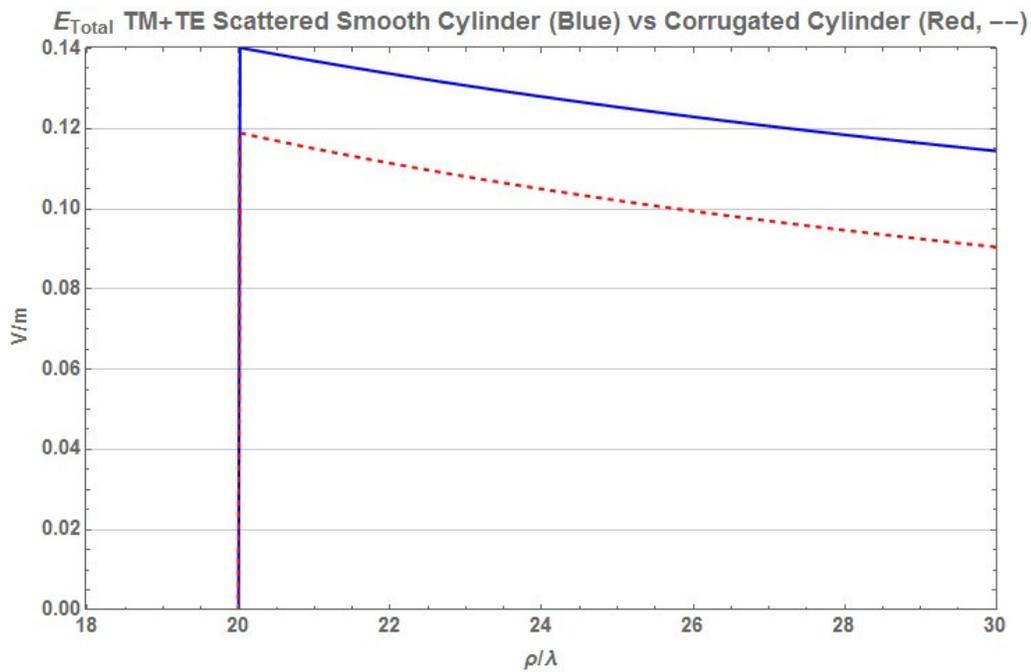


Figure 7-68 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

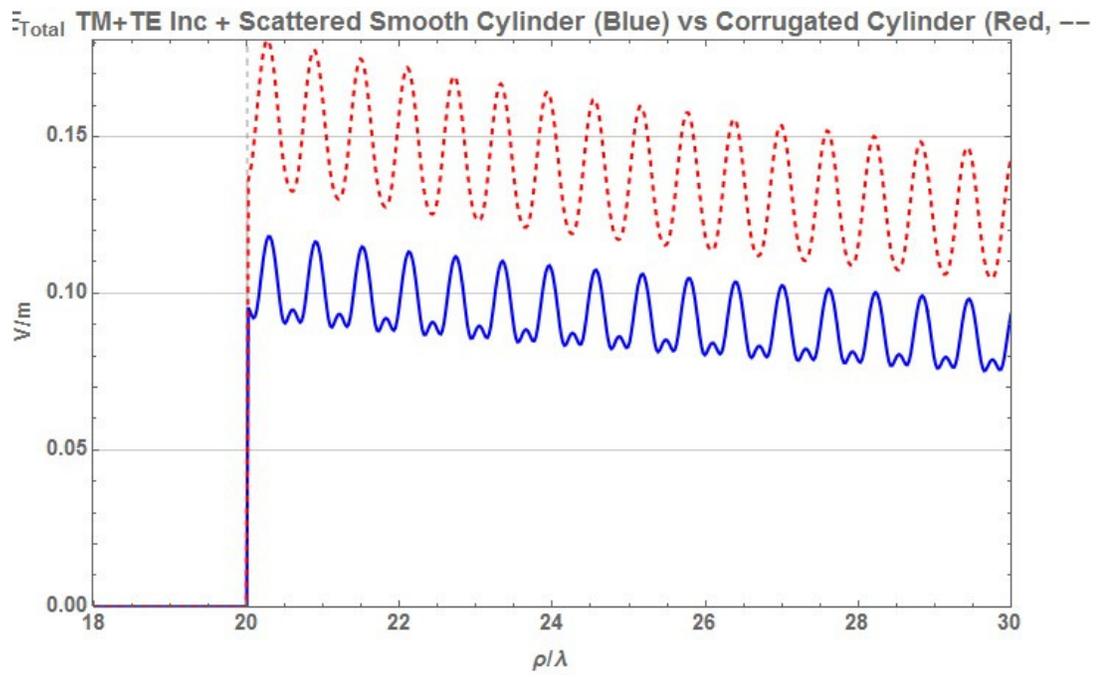


Figure 7-69 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.20.0.0

7.5.5 Run b.2.0.0 ($b=2\lambda$, $a=b \cdot .001$, $\rho_2=2\lambda$, $m=0$)

Table 12 Detailed parameters summary for changing ϕ plots of Run b.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.002 λ	-	-	-	-
b	2. λ	-	-	-	-
ρ_1	1.998 λ	-	-	-	-
ρ_2	2. λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	20. λ	-	-	-	-
z (observed)	500.5 a && 1.001 λ	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary b	-	-	-	-

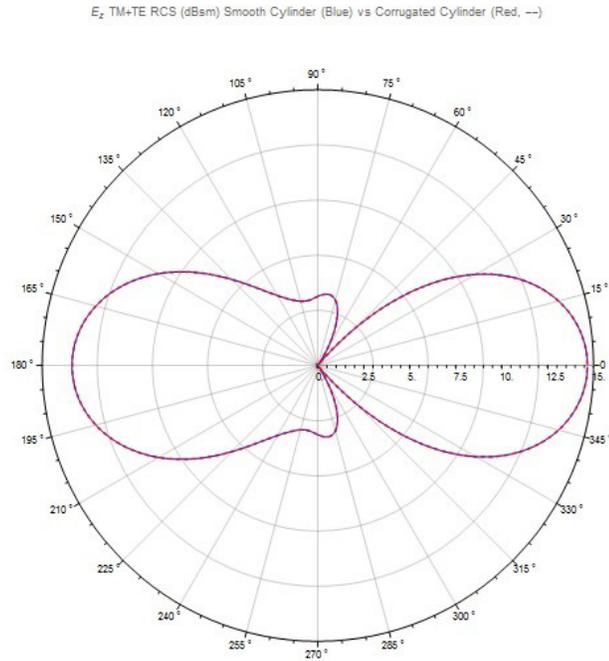


Figure 7-70 Polar Plot form of RCS dBsm for Ez of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0

E_{θ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

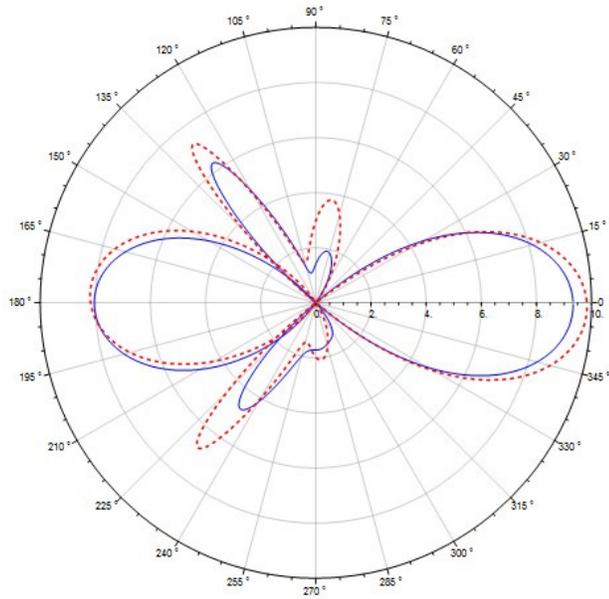


Figure 7-71 Polar Plot form of RCS dBsm for E_{θ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0

E_{ϕ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

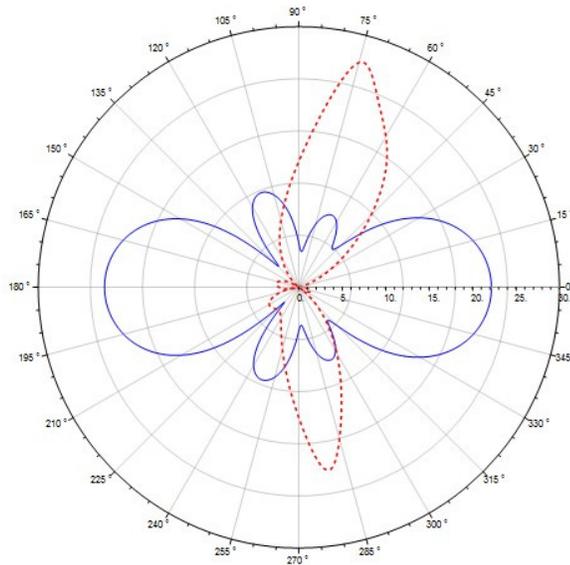


Figure 7-72 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.2.0.0

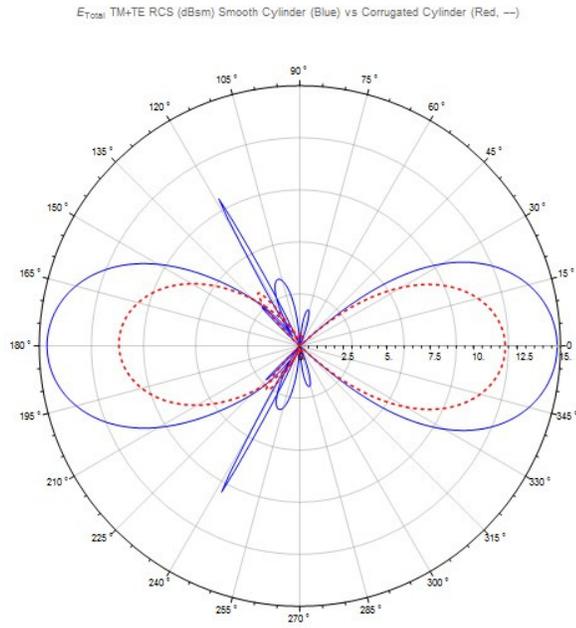


Figure 7-73 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

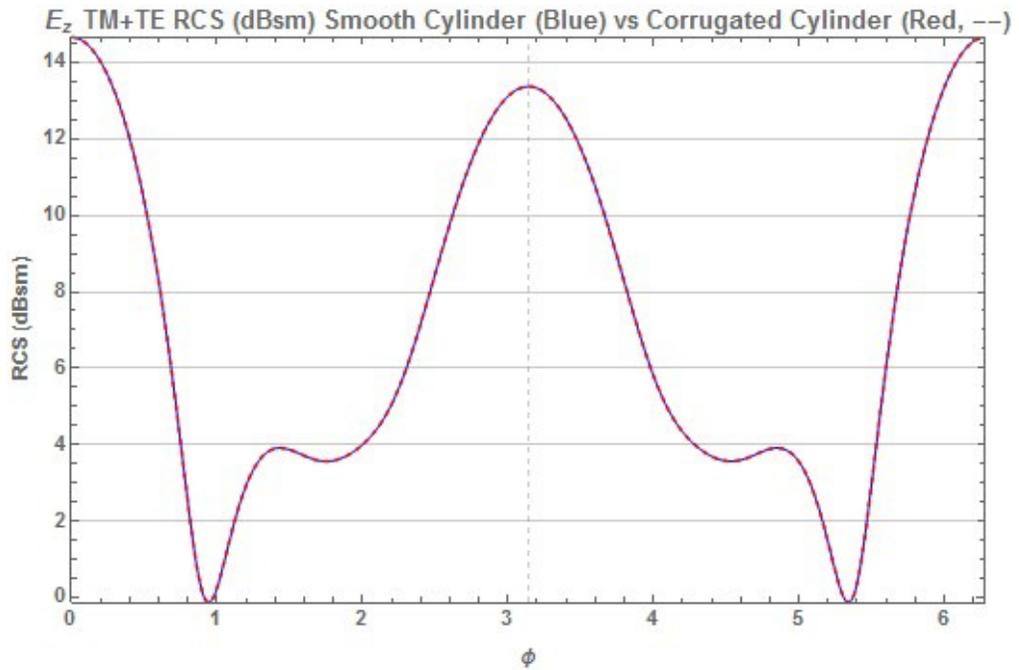


Figure 7-74 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

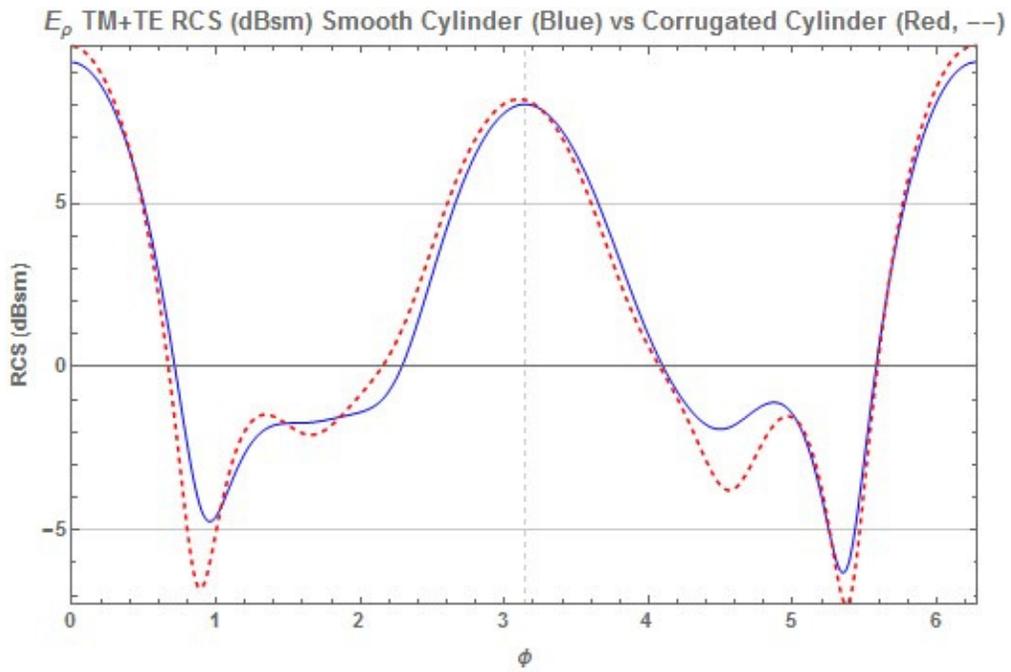


Figure 7-75 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

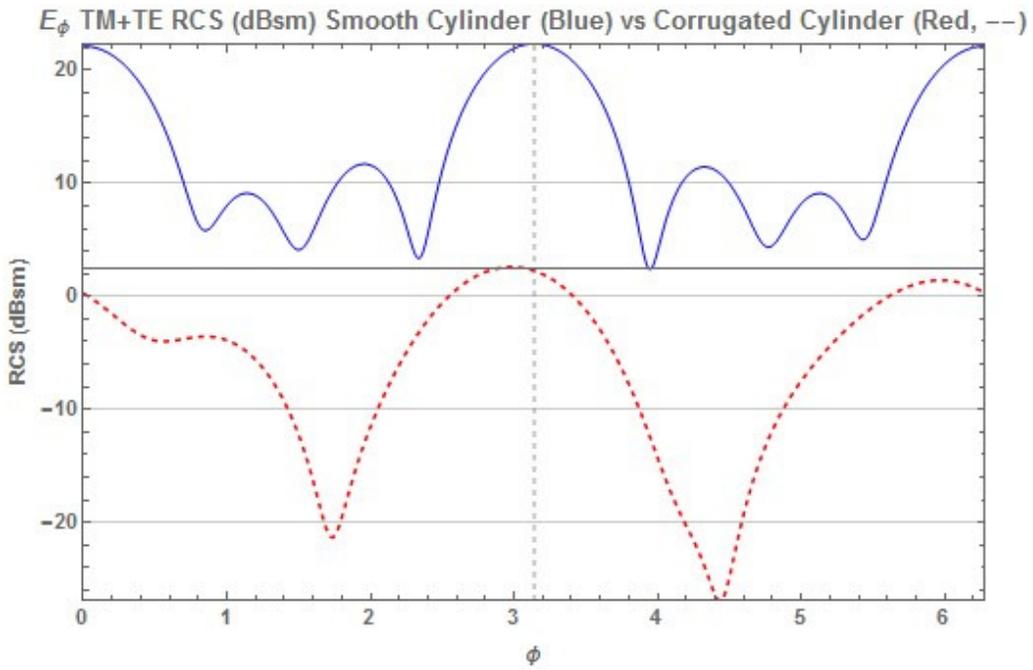


Figure 7-76 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

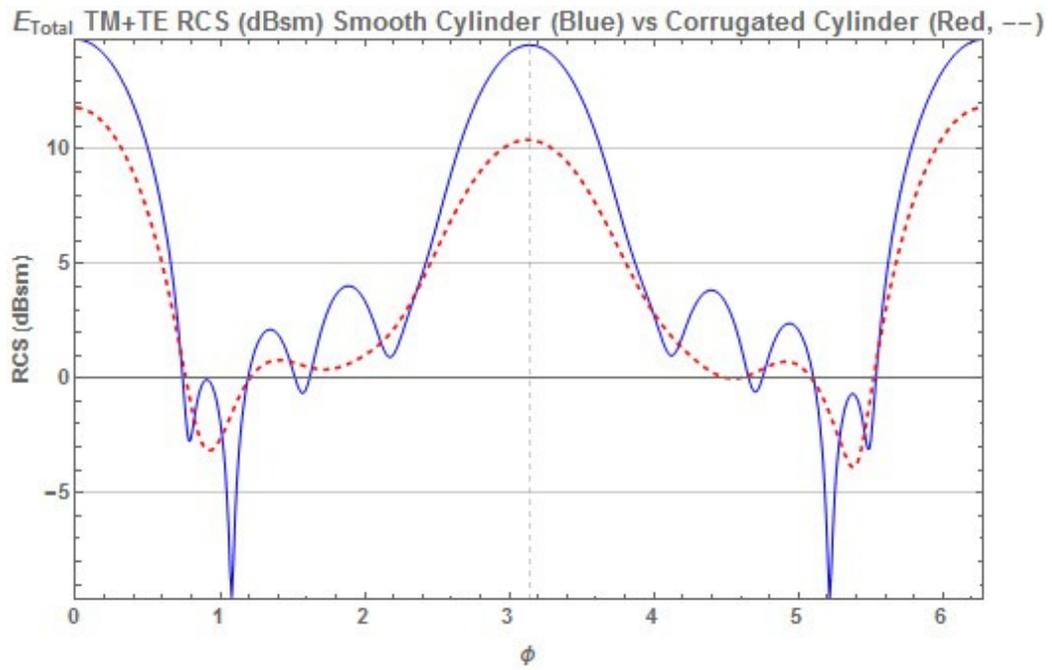


Figure 7-77 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

Table 13 Detailed parameters summary for changing ρ plots of Run b.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.002λ	-	-	-	-
b	$2. \lambda$	-	-	-	-
ρ_1	1.998λ	-	-	-	-
ρ_2	$2. \lambda$	-	-	-	-
ρ range	-	1.7982λ	$12. \lambda$	0.0185825λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$500.5 a \&\& 1.001 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary b	-	-	-	-

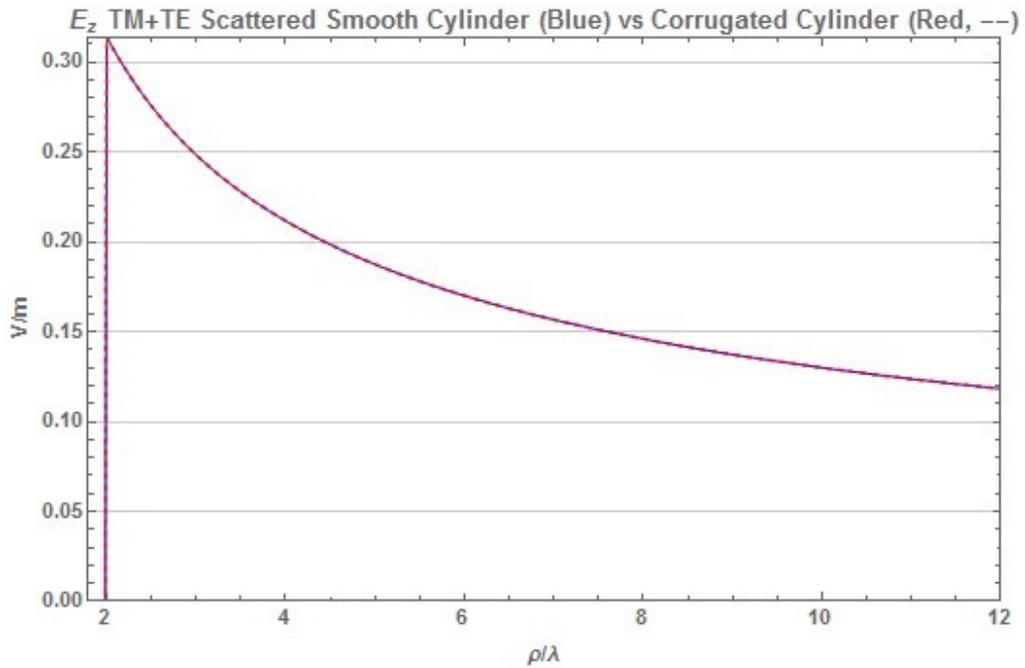


Figure 7-78 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

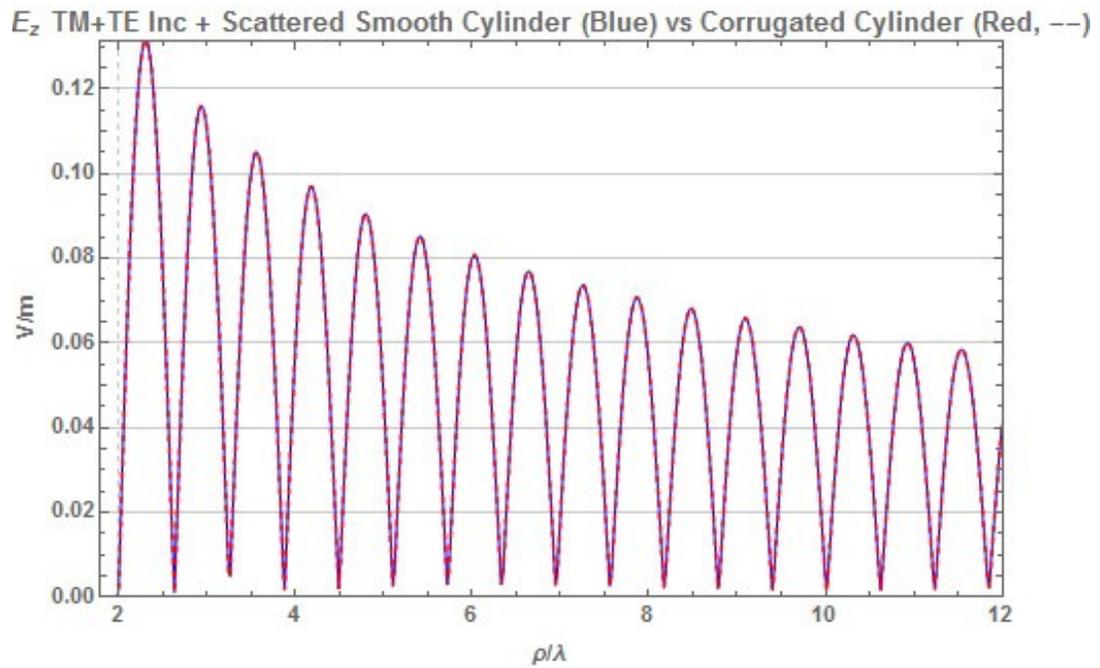


Figure 7-79 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

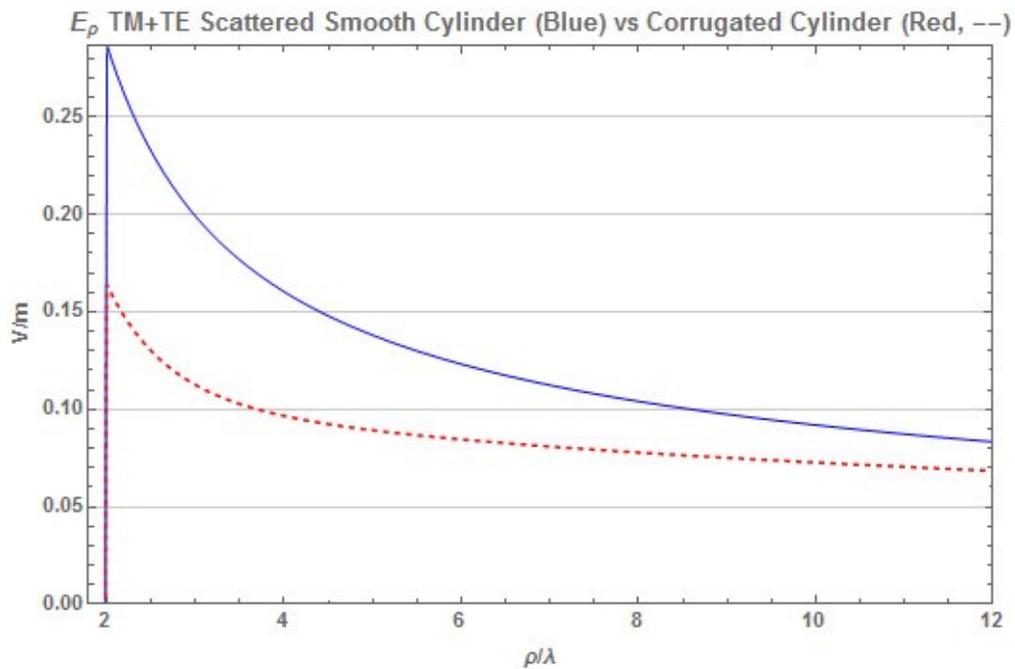


Figure 7-80 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

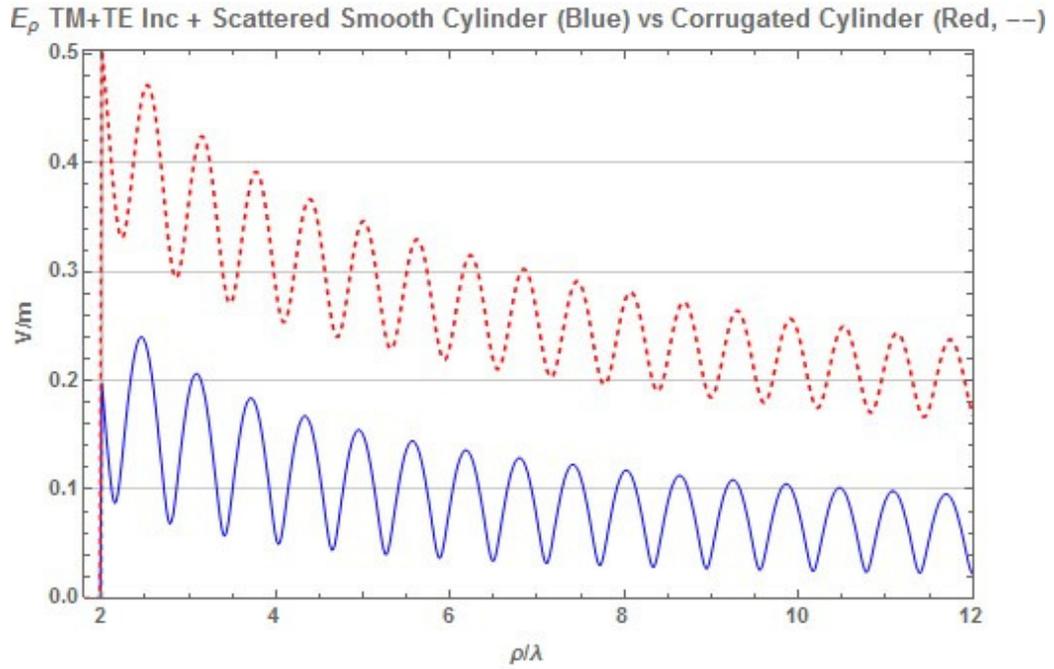


Figure 7-81 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

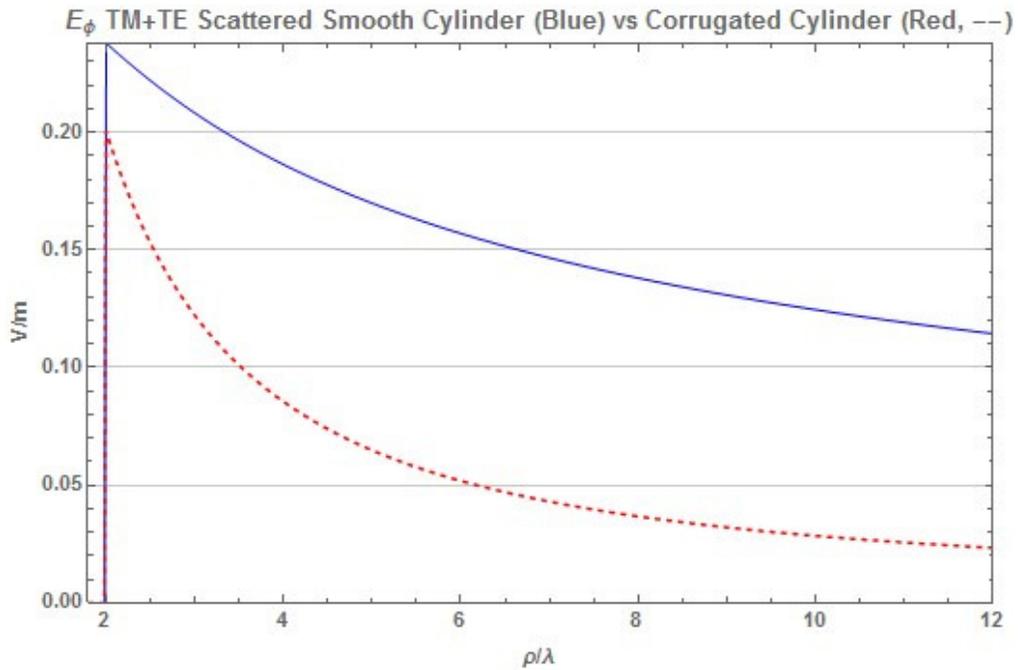


Figure 7-82 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

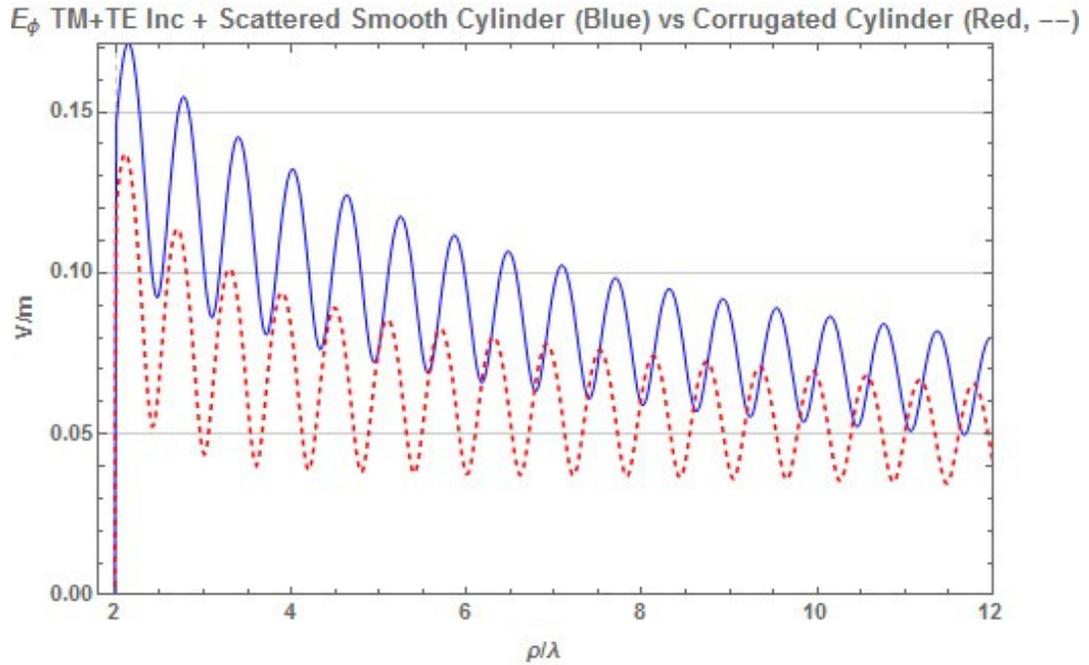


Figure 7-83 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

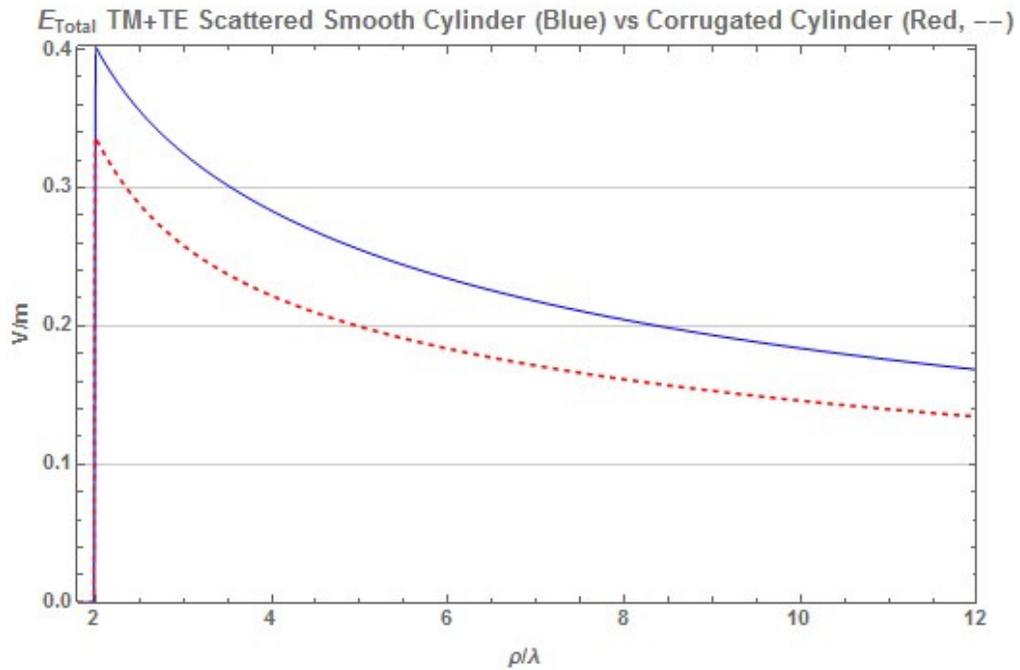


Figure 7-84 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

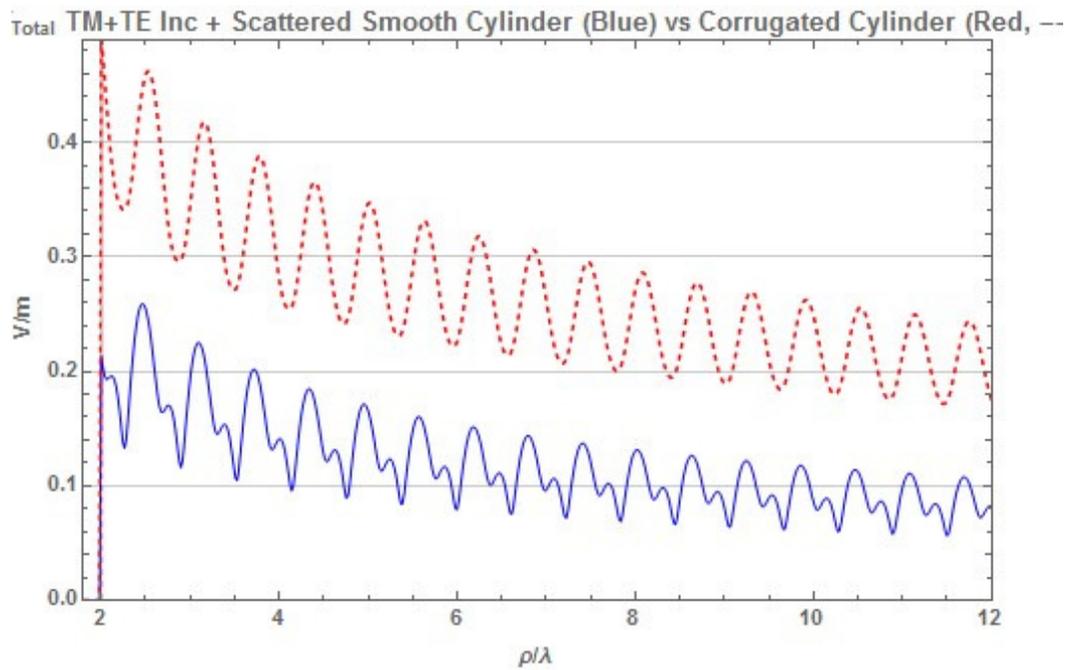


Figure 7-85 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.2.0.0

7.5.6 Run b.0.1.0.0 ($b=0.1\lambda$, $a=b*.001$, $\rho_2=0.1\lambda$, $m=0$)

Table 14 Detailed parameters summary for changing ϕ plots of Run b.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.0001 λ	-	-	-	-
b	0.1 λ	-	-	-	-
ρ_1	0.0999 λ	-	-	-	-
ρ_2	0.1 λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	1. λ	-	-	-	-
z (observed)	500.5 a && 0.05005 λ	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary b	-	-	-	-

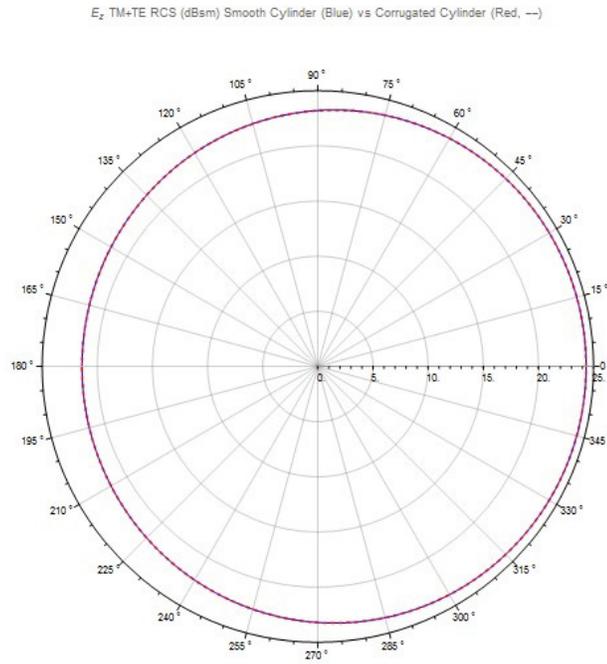


Figure 7-86 Polar Plot form of RCS dBsm for Ez of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

E_{ϕ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

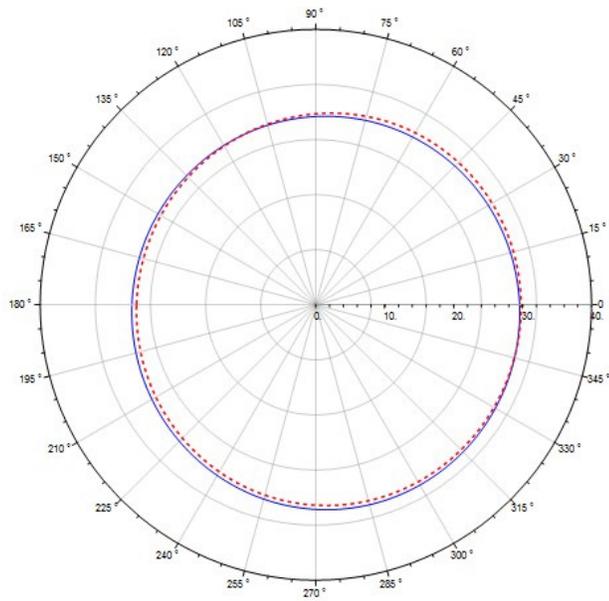


Figure 7-87 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

E_{ϕ} TM+TE RCS (dBsm) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)

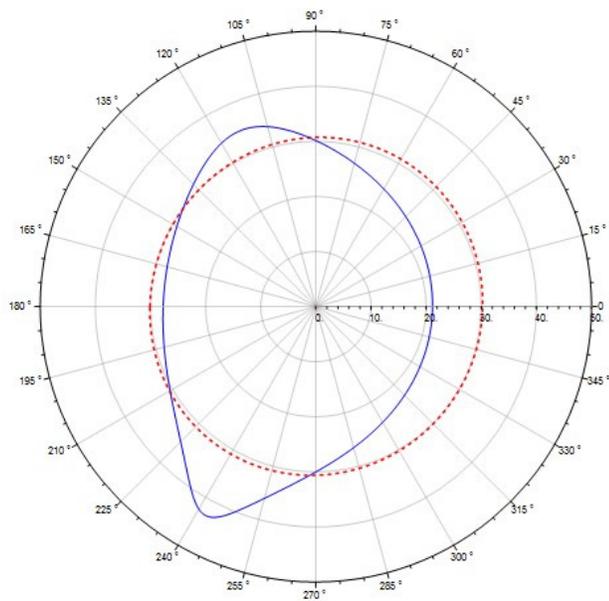


Figure 7-88 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

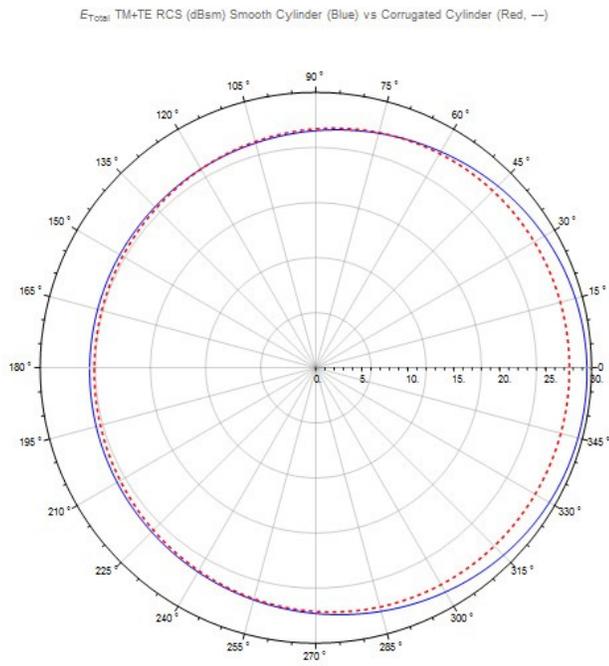


Figure 7-89 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

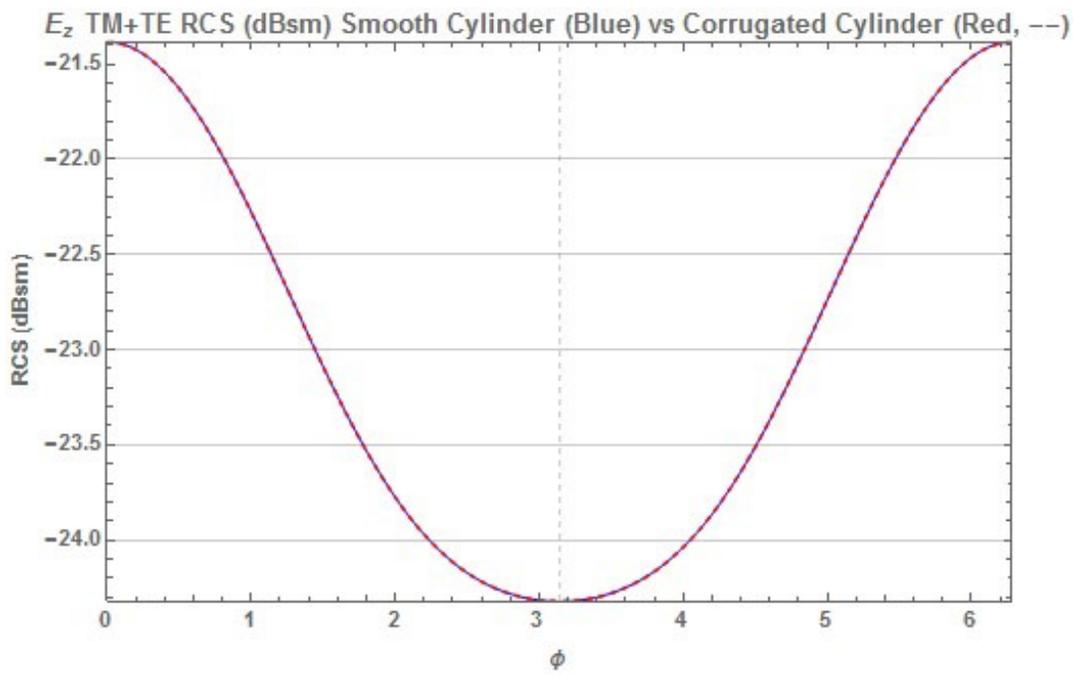


Figure 7-90 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

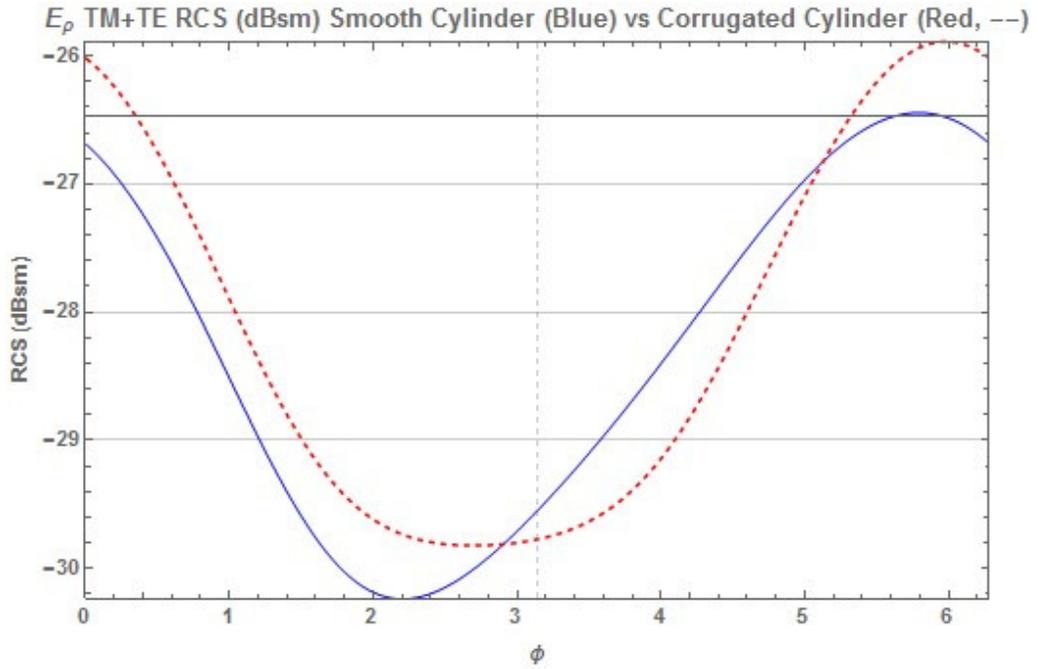


Figure 7-91 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

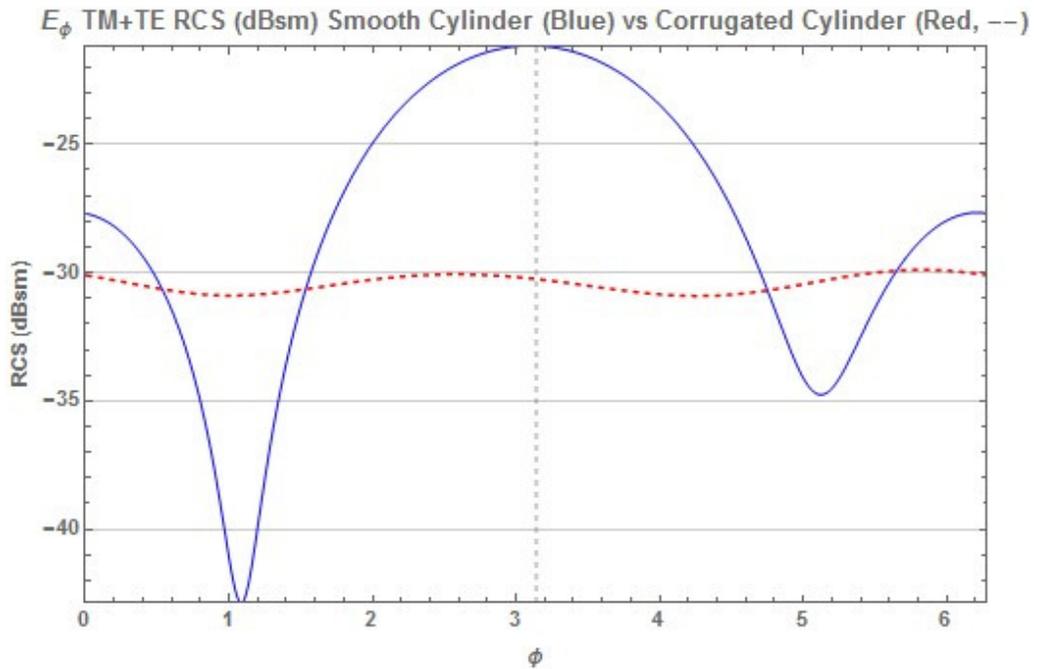


Figure 7-92 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

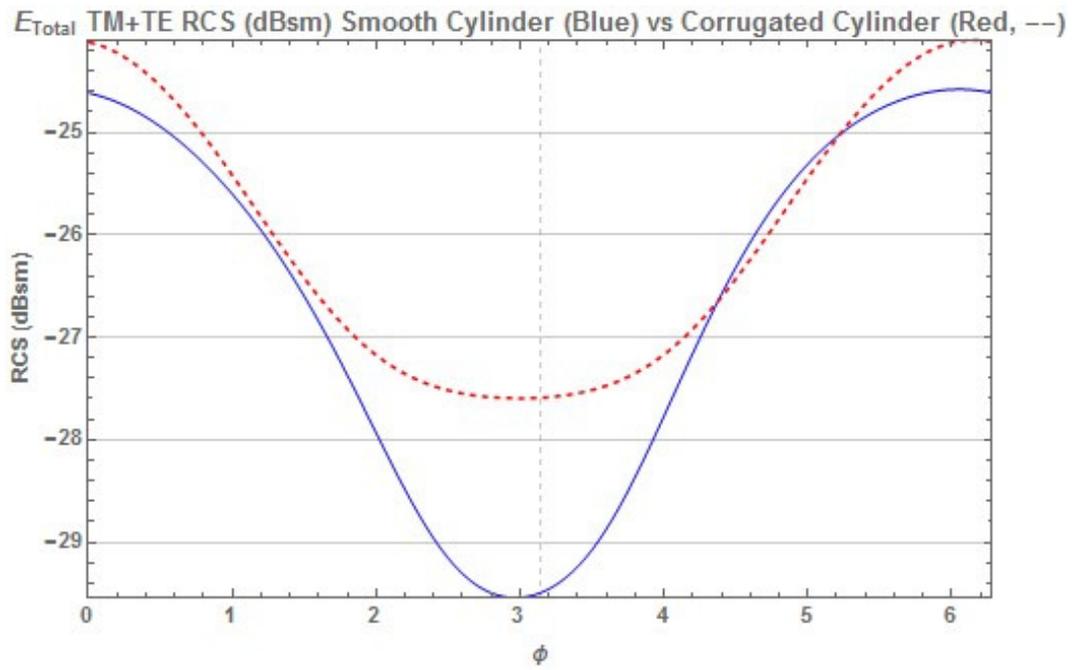


Figure 7-93 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.1.0.0

Table 15 Detailed parameters summary for changing ρ plots of Run b.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.0001 λ	-	-	-	-
b	0.1 λ	-	-	-	-
ρ_1	0.0999 λ	-	-	-	-
ρ_2	0.1 λ	-	-	-	-
ρ range	-	0.08991 λ	10.1 λ	0.0182333 λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	500.5 a && 0.05005 λ	-	-	-	-
Matching Points	-	-	-	-	7
θ_1	55. Deg	-	-	-	-
ϕ_1	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary b	-	-	-	-

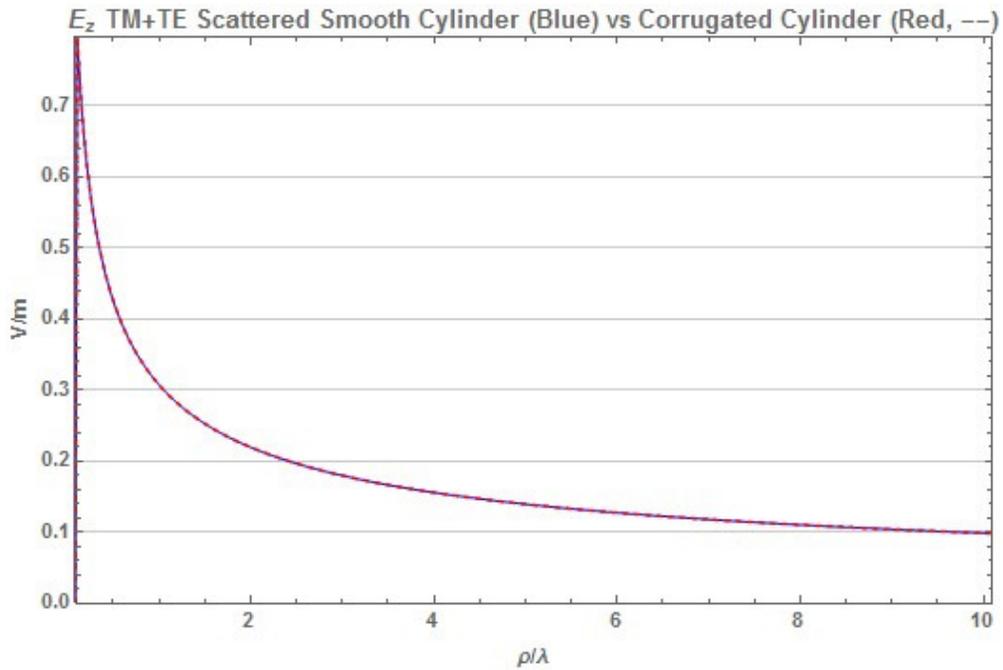


Figure 7-94 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

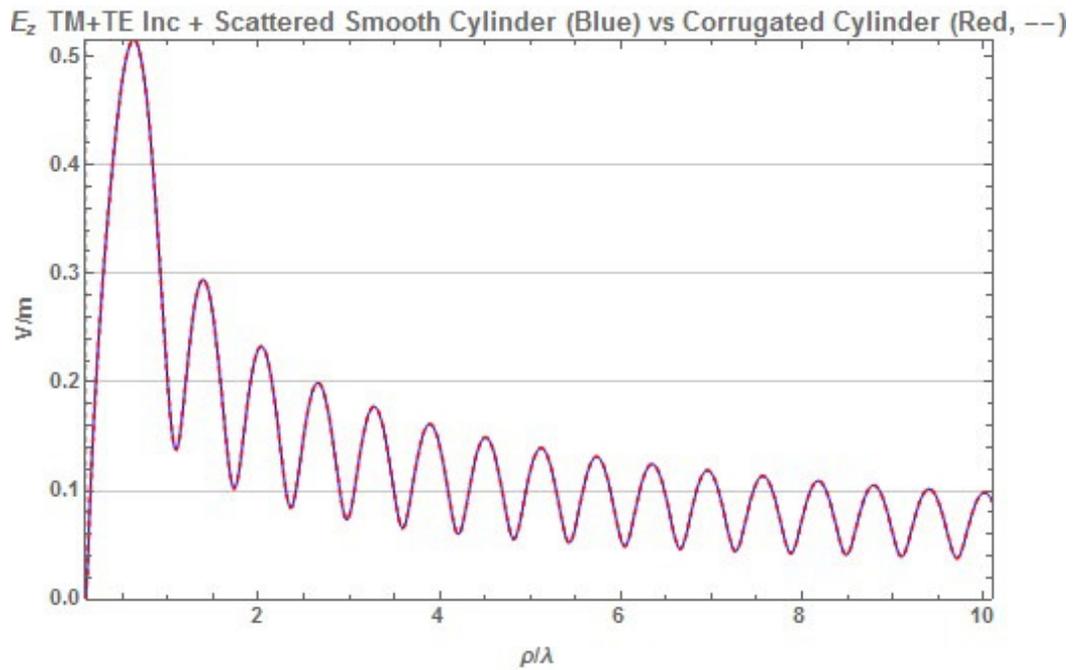


Figure 7-95 XY Plot of Scattered + Incident Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

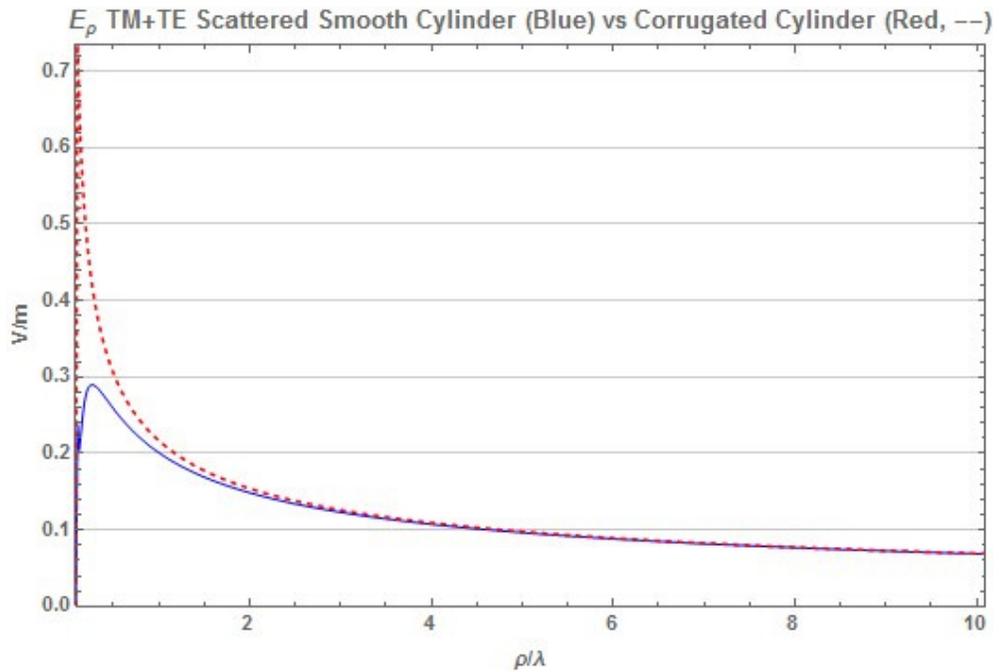


Figure 7-96 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

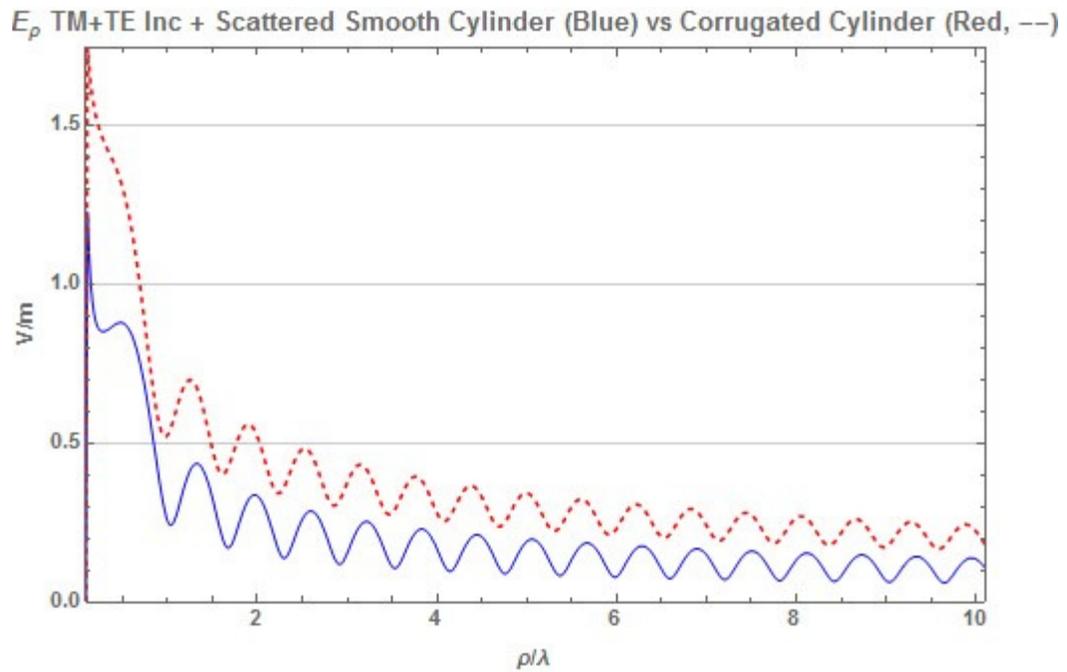


Figure 7-97 XY Plot of Scattered + Incident Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

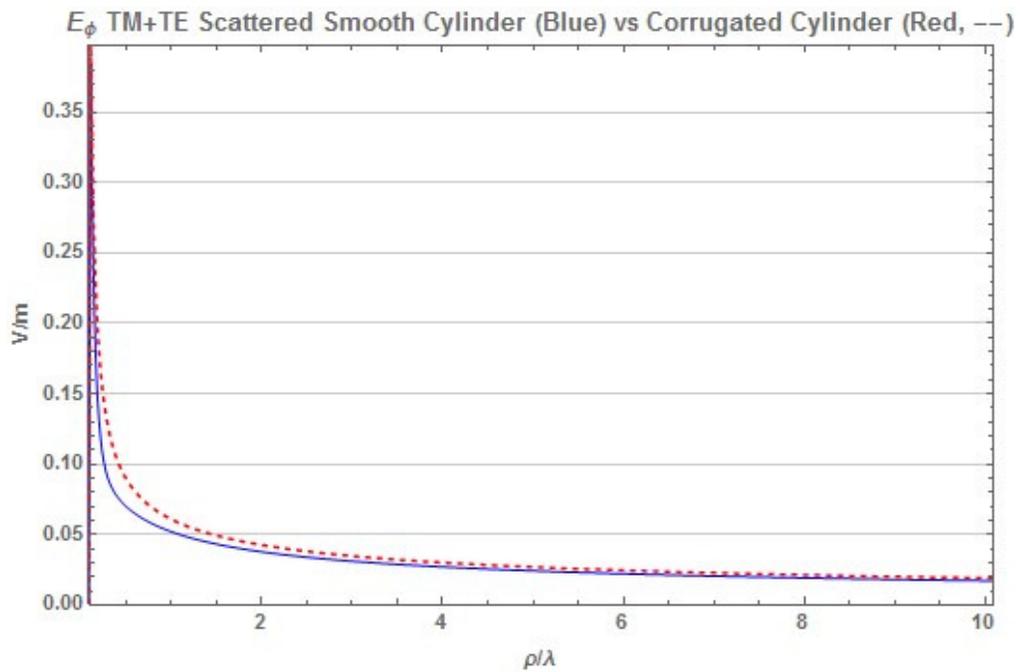


Figure 7-98 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

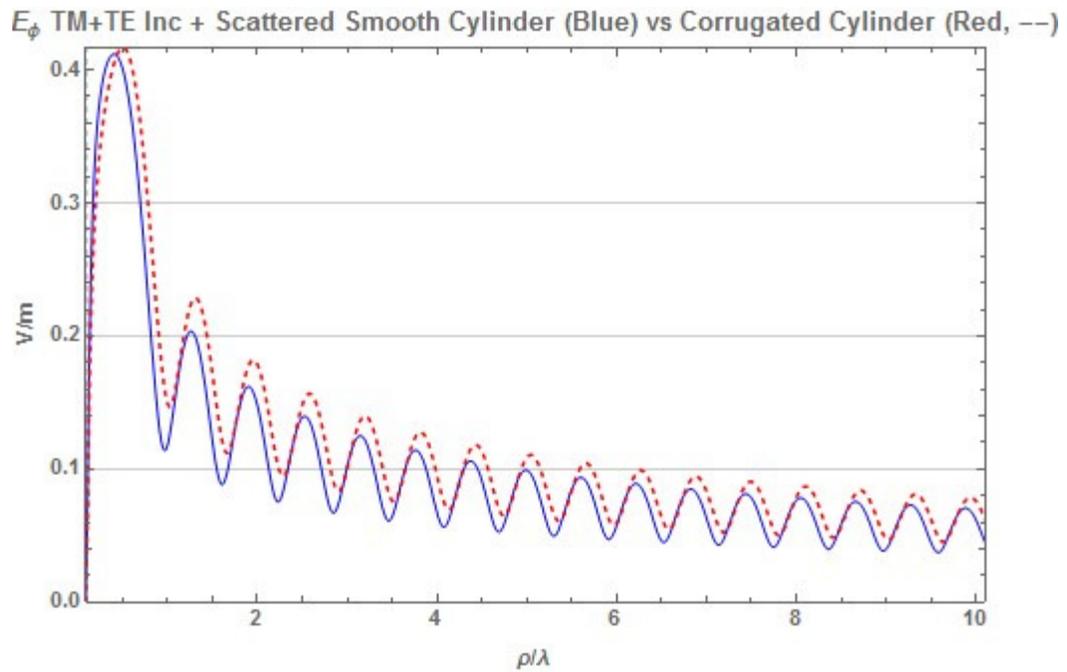


Figure 7-99 XY Plot of Scattered + Incident Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

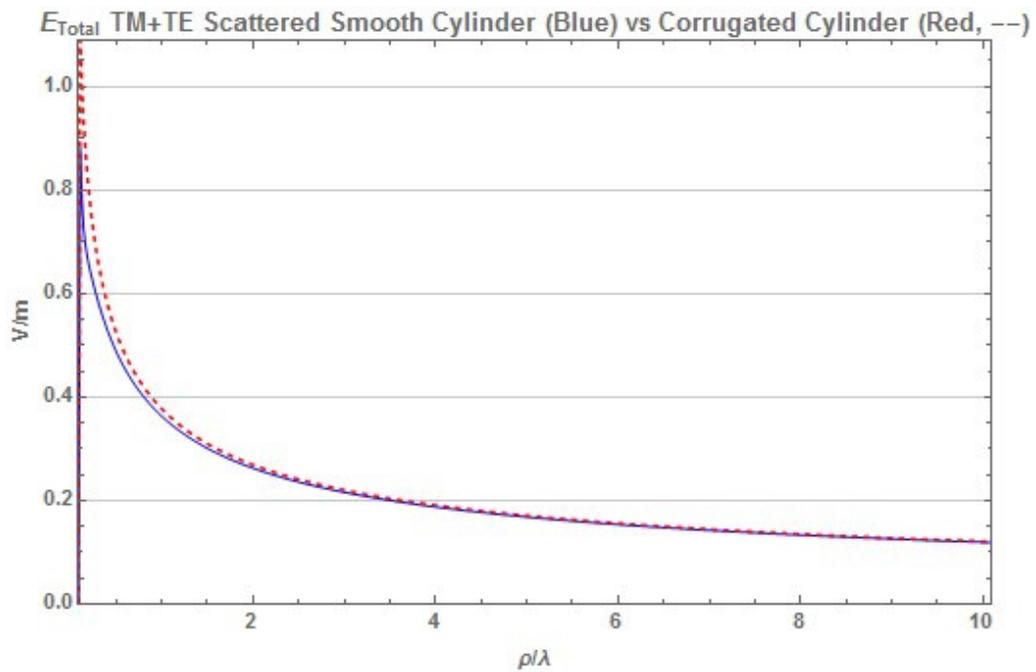


Figure 7-100 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

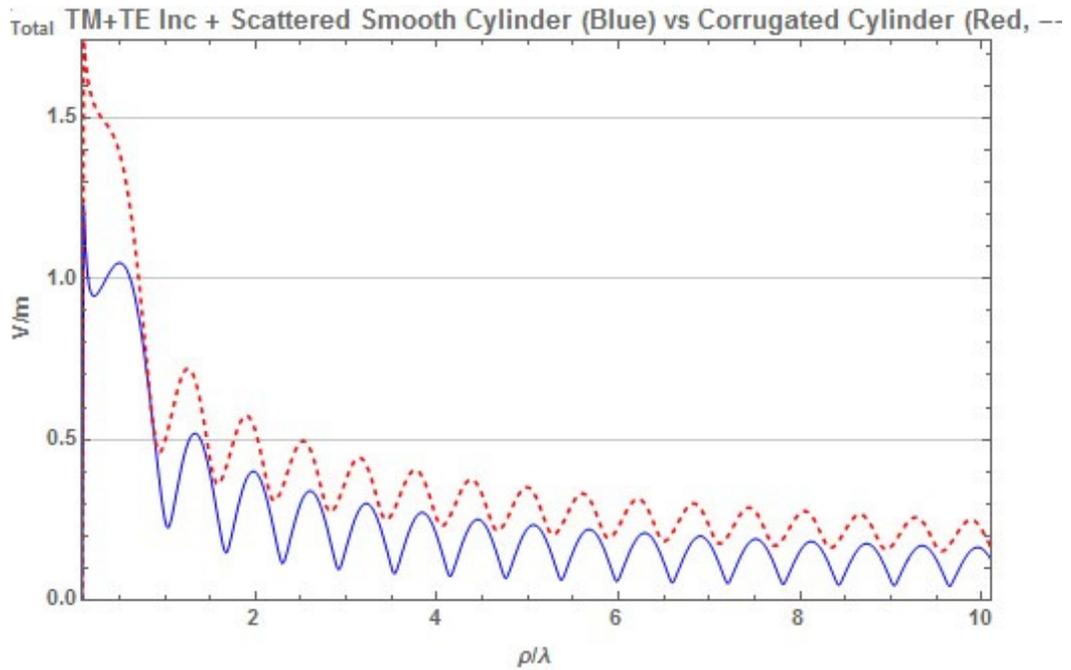


Figure 7-101 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run b.0.10.0.0

7.5.7 Run a_plus_b.20.0.0 ($b=20\lambda$, $a=b*0.001$, $\rho_2=20\lambda$, $m=0$)

Table 16 Detailed parameters summary for changing ϕ plots of Run a_plus_b.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.02λ	-	-	-	-
b	$20. \lambda$	-	-	-	-
ρ_1	19.98λ	-	-	-	-
ρ_2	$20. \lambda$	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	$200. \lambda$	-	-	-	-
z (observed)	$0.25 a \&\& 0.005 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

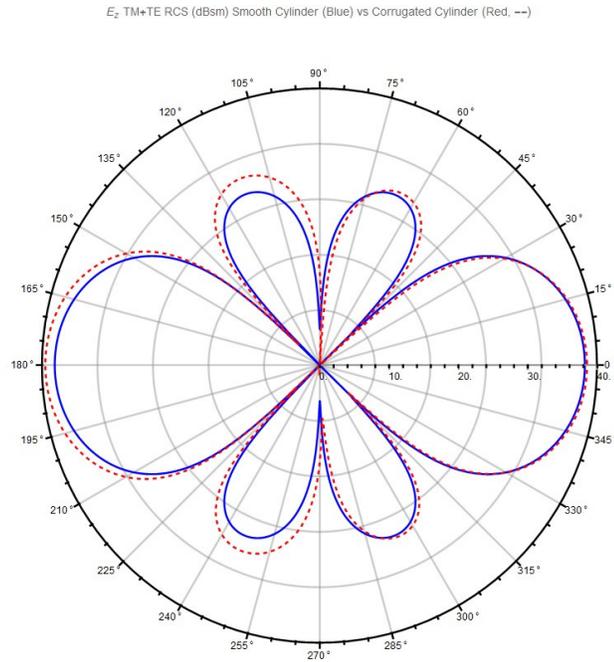


Figure 7-102 Polar Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

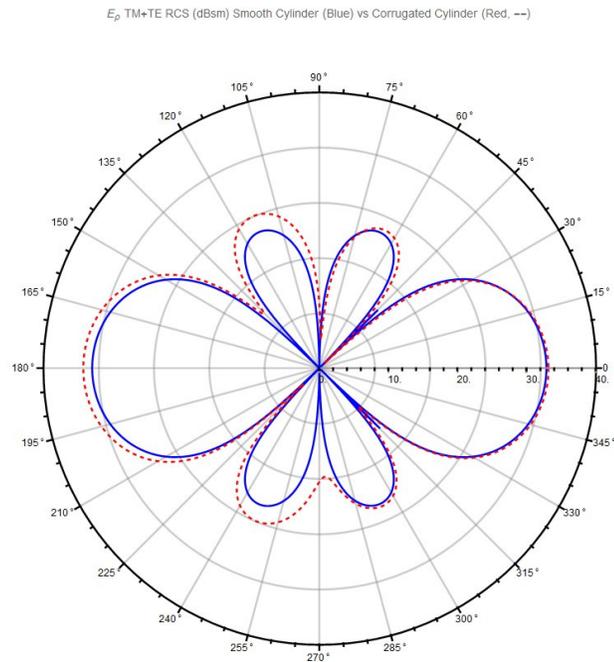


Figure 7-103 Polar Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

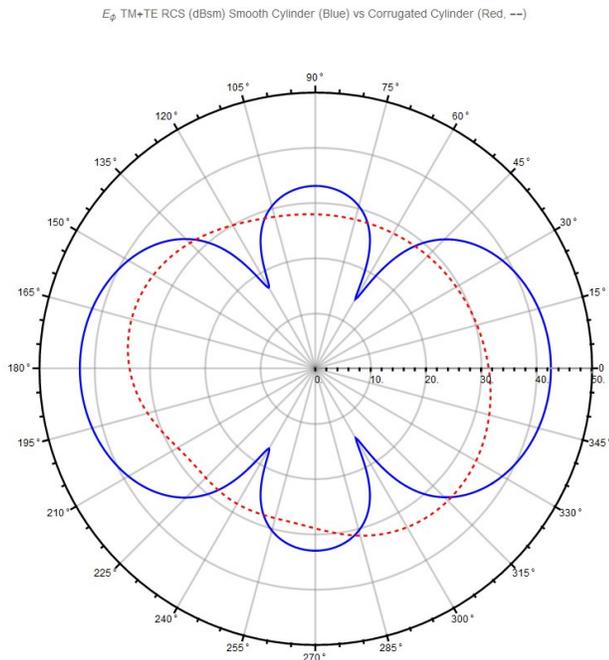


Figure 7-104 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

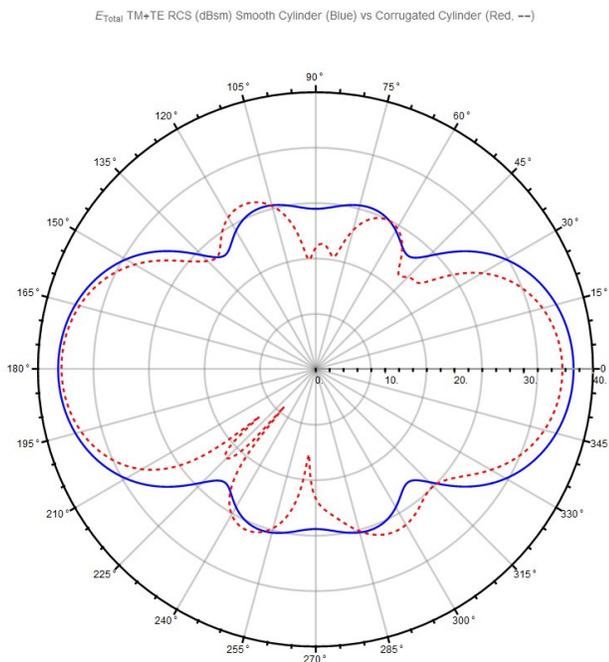


Figure 7-105 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

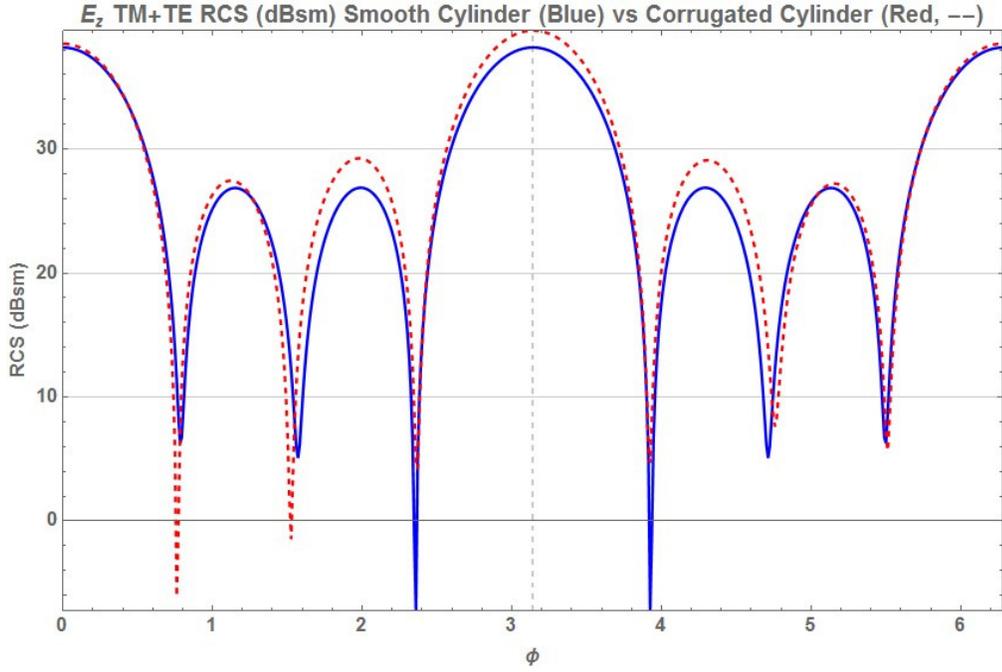


Figure 7-106 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

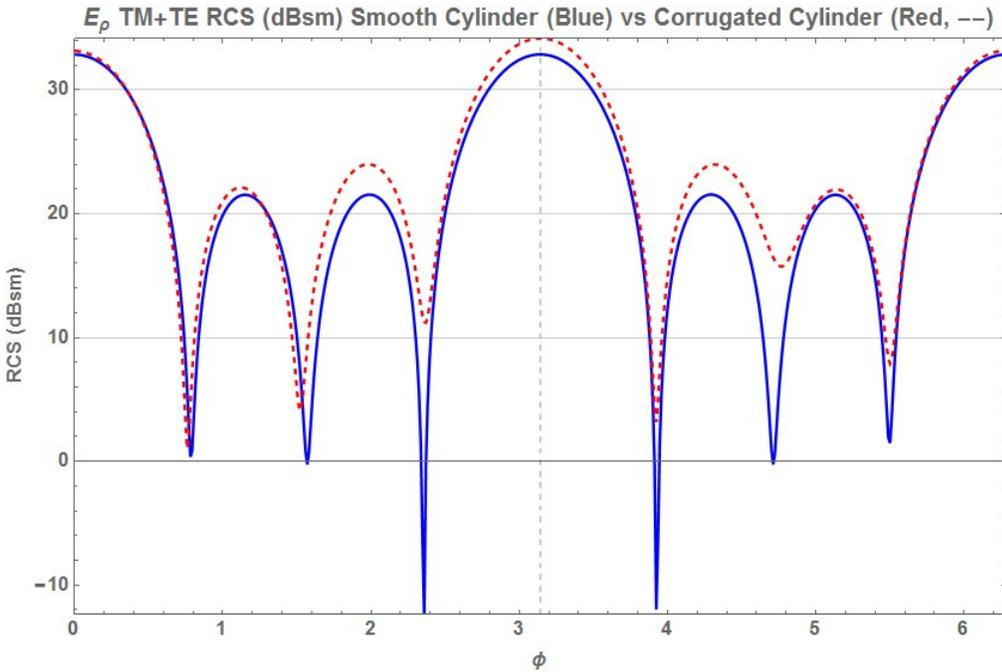


Figure 7-107 XY Plot form of RCS dBsm for E_ρ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

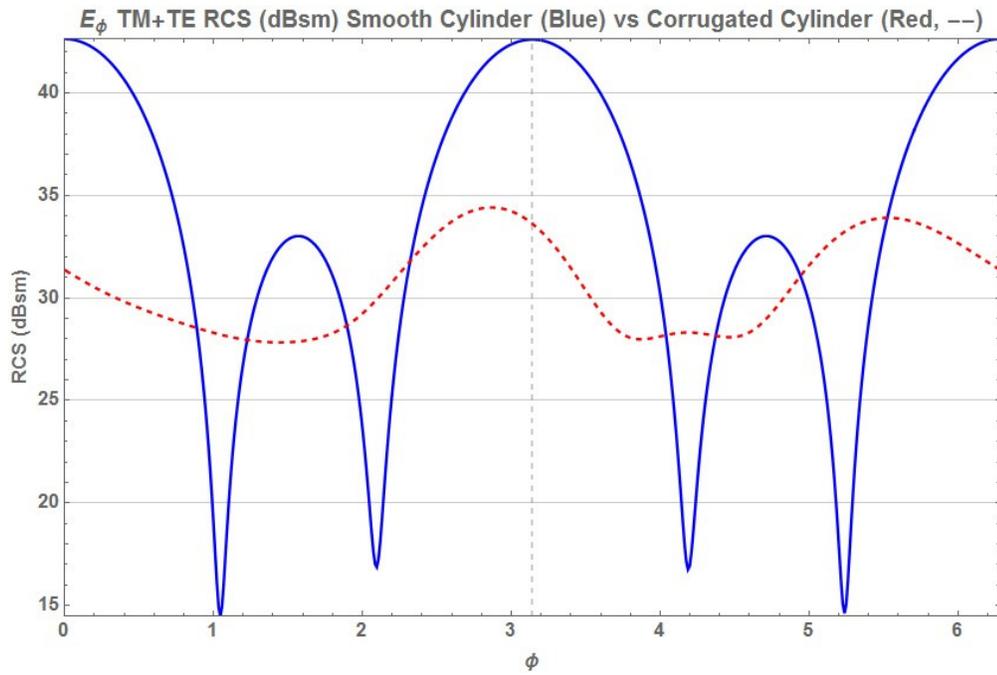


Figure 7-108 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

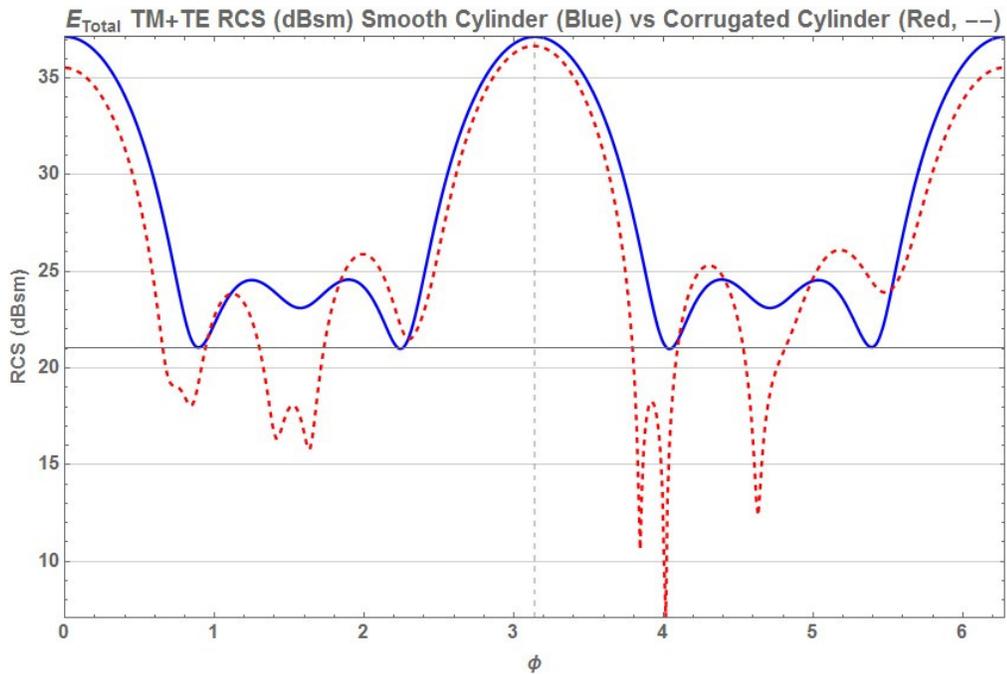


Figure 7-109 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

Table 17 Detailed parameters summary for changing ρ plots of Run a_plus_b.20.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.02λ	-	-	-	-
b	$20. \lambda$	-	-	-	-
ρ_1	19.98λ	-	-	-	-
ρ_2	$20. \lambda$	-	-	-	-
ρ range	-	17.982λ	$30. \lambda$	0.0218907λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$0.25 a \ \&\& \ 0.005 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
ϕ_i	55. Deg	-	-	-	-
ϕ_l	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.04	-	-	-	-
max allowable l	8.537	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

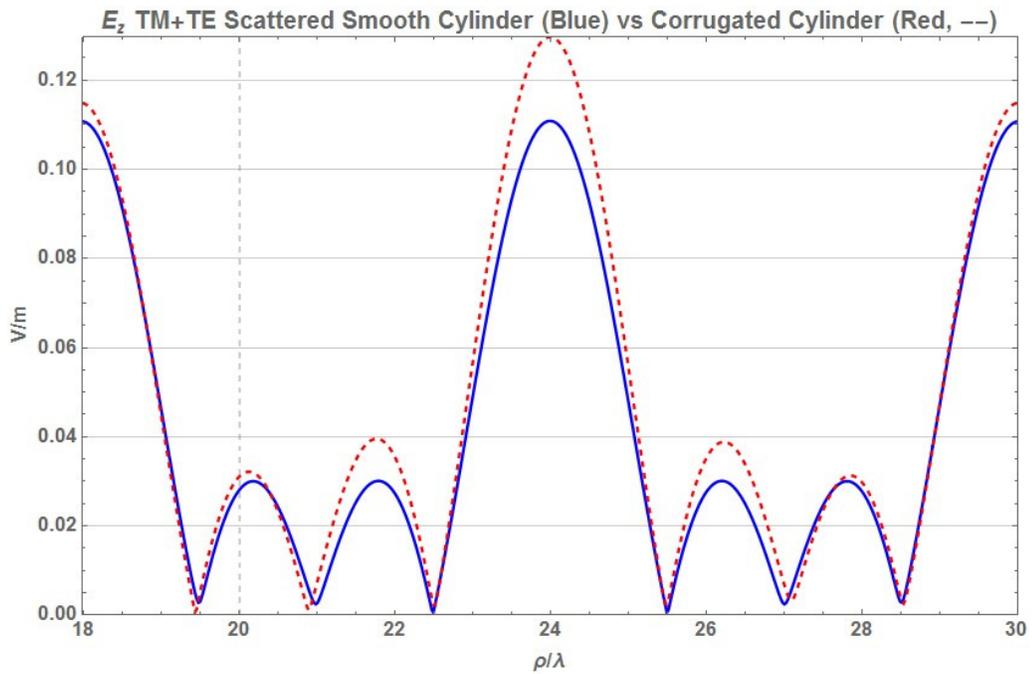


Figure 7-110 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

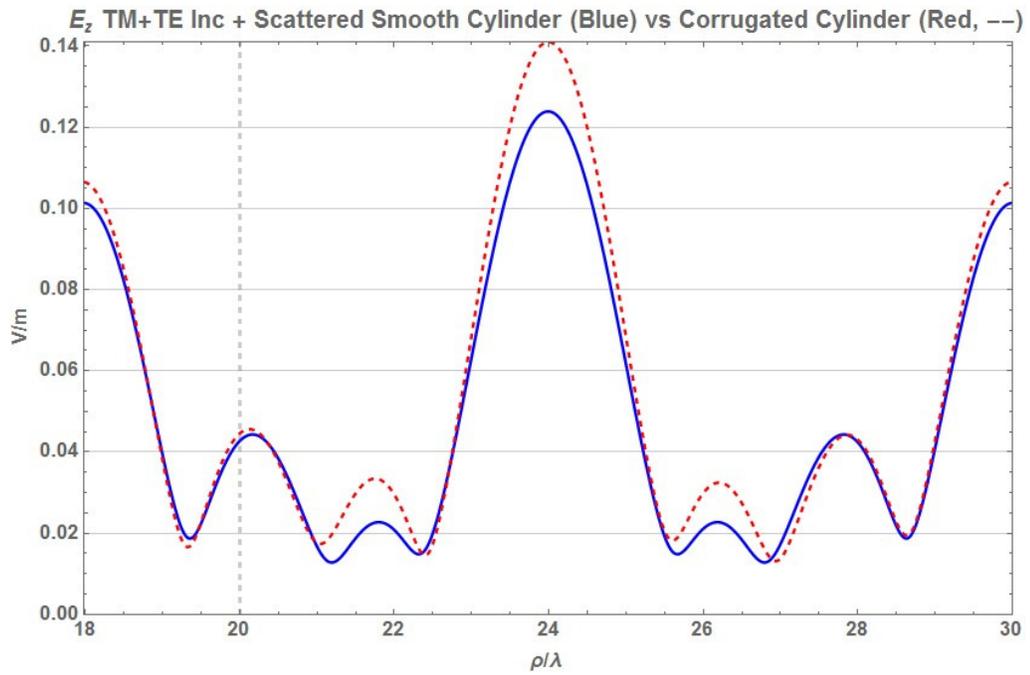


Figure 7-111 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

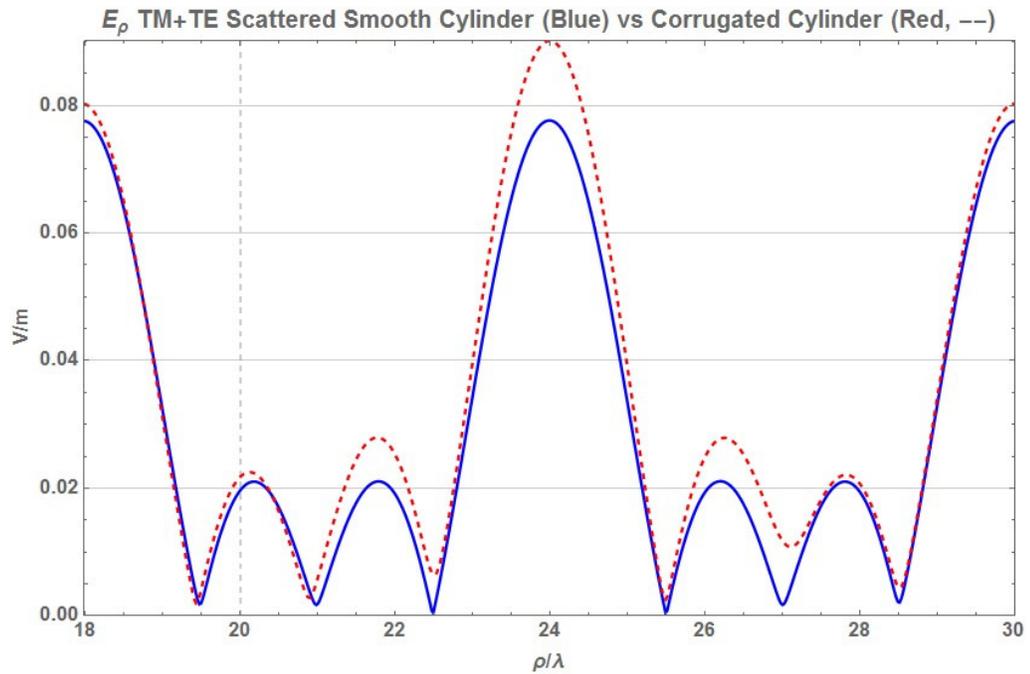


Figure 7-112 XY Plot of Scattered Field Amplitude Only, for E_p , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

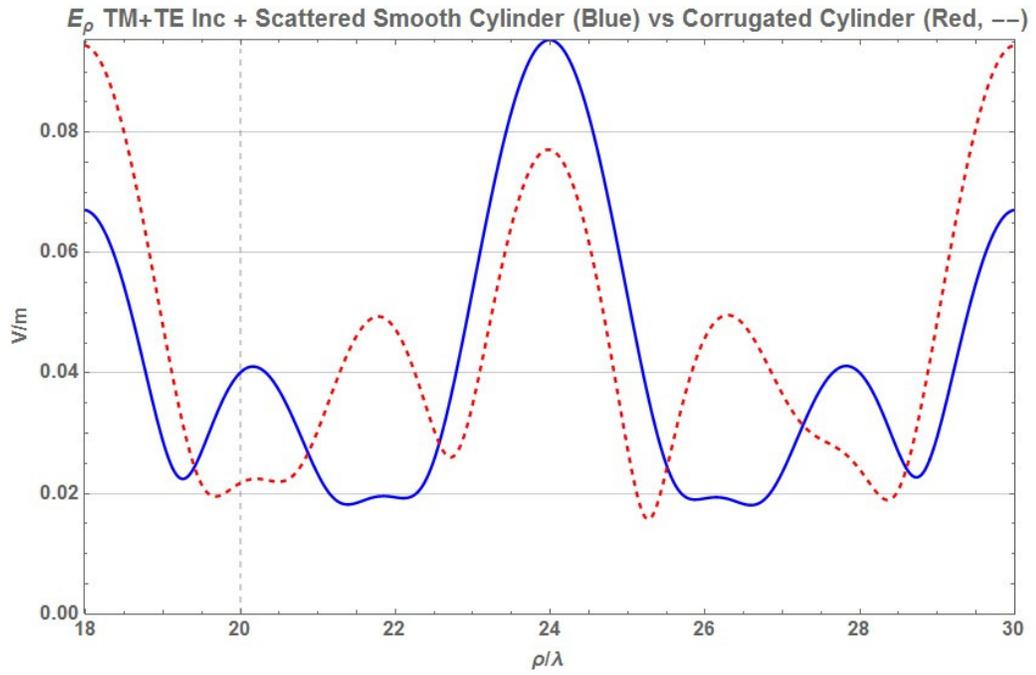


Figure 7-113 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

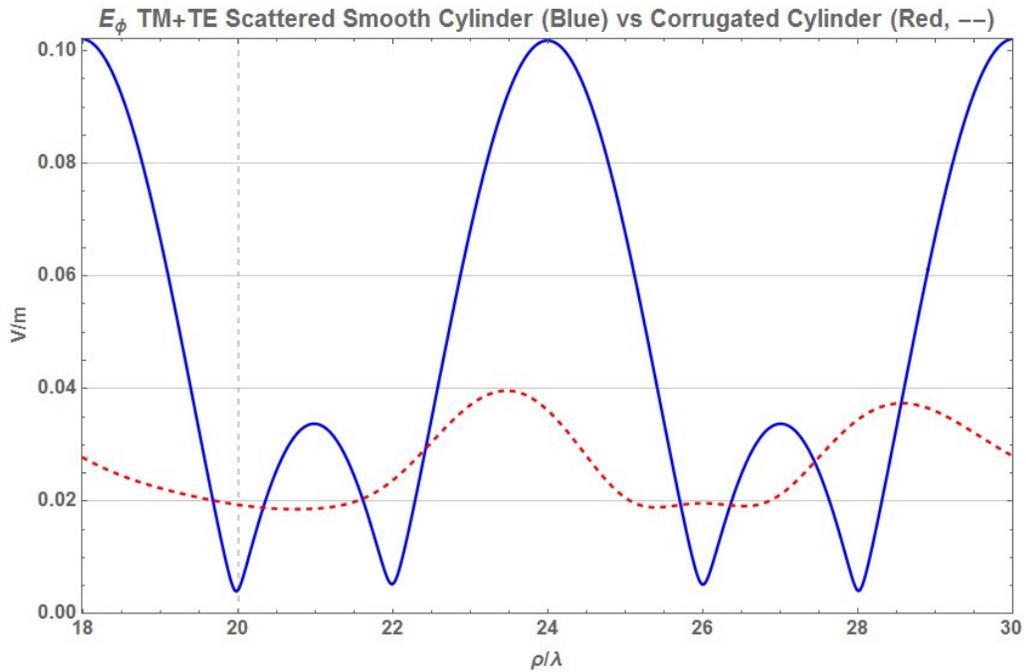


Figure 7-114 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

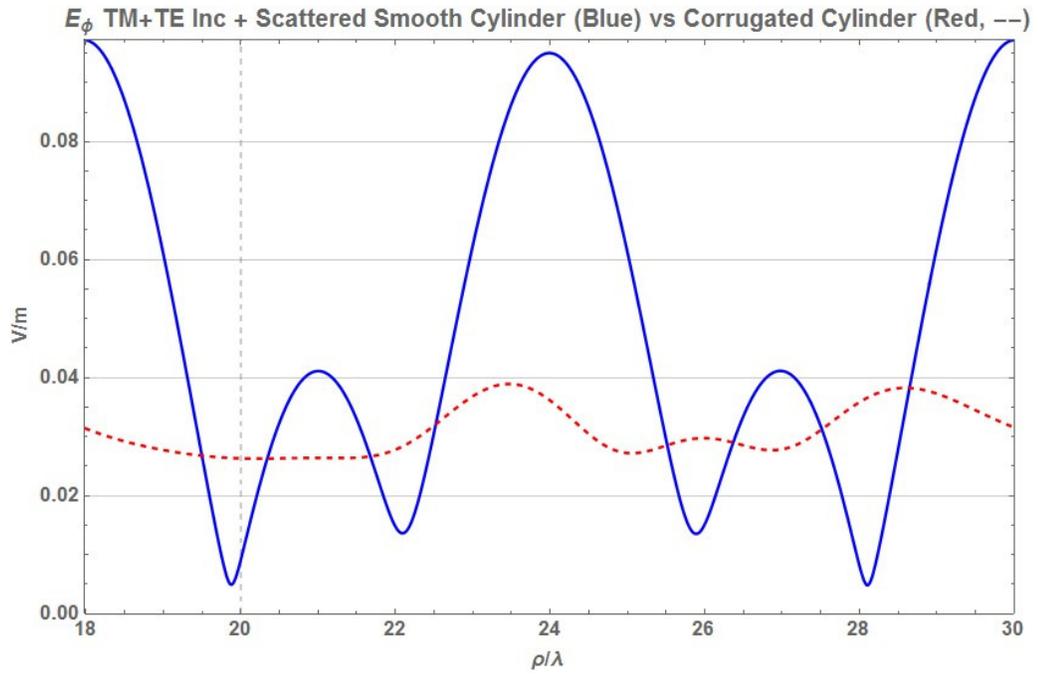


Figure 7-115 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

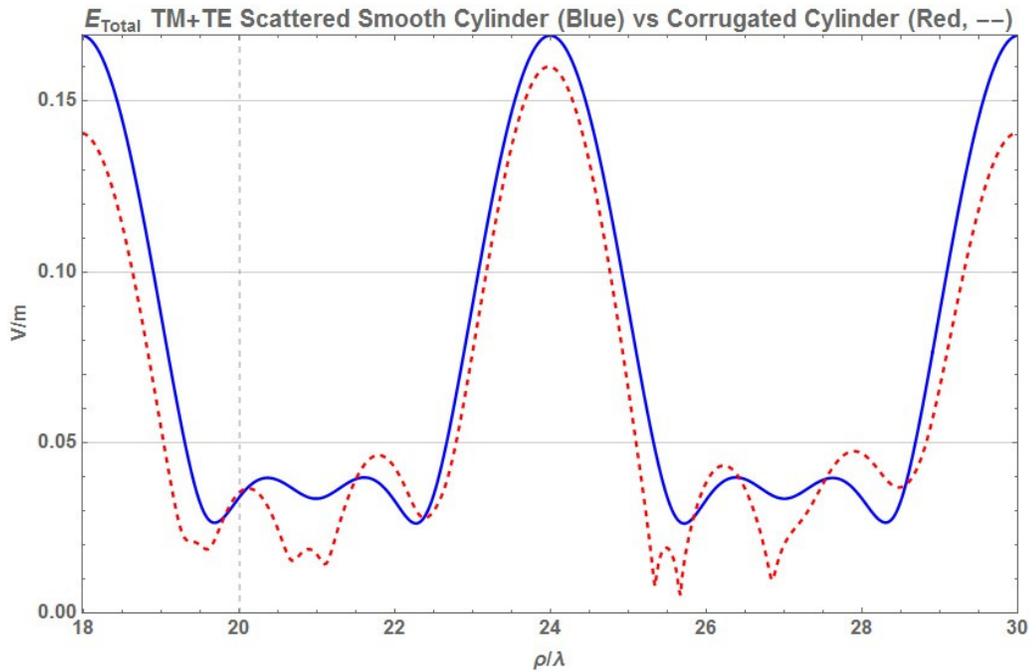


Figure 7-116 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

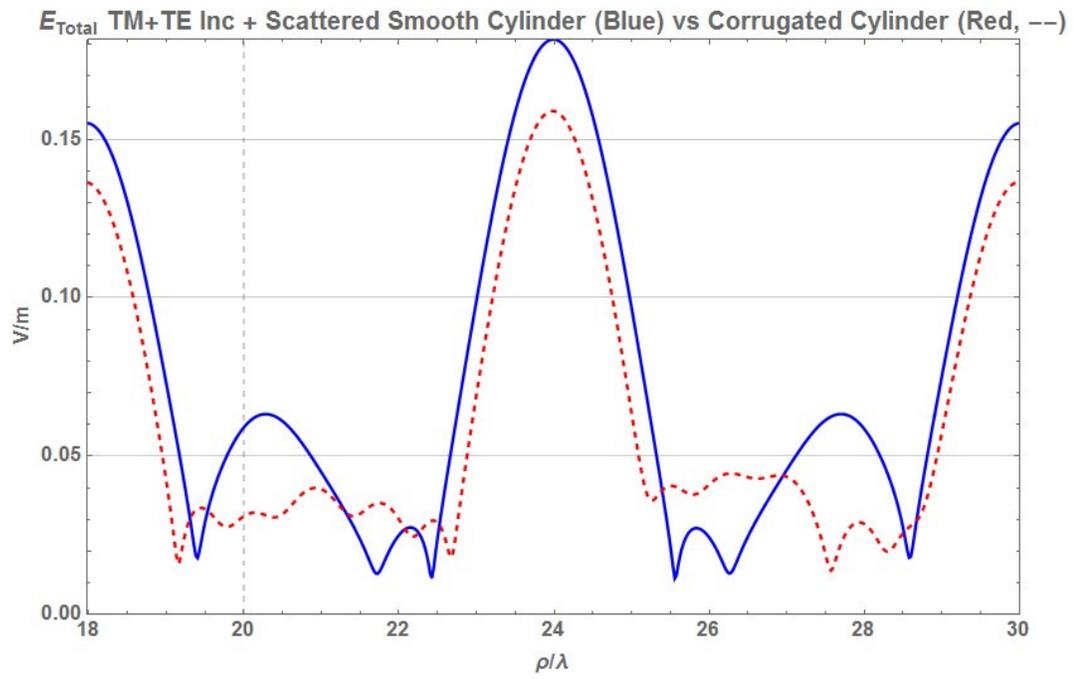


Figure 7-117 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.20.0.0

7.5.8 Run a_plus_b.2.0.0 (b=2λ, a=b*.001, ρ2=2λ, m=0)

Table 18 Detailed parameters summary for changing φ plots of Run a_plus_b.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105 × 10 ¹⁰ Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.002 λ	-	-	-	-
b	2. λ	-	-	-	-
ρ1	1.998 λ	-	-	-	-
ρ2	2. λ	-	-	-	-
φ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	20. λ	-	-	-	-
z (observed)	0.25 a & 0.0005 λ	-	-	-	-
Matching Points	-	-	-	-	7
θi	55. Deg	-	-	-	-
φi	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

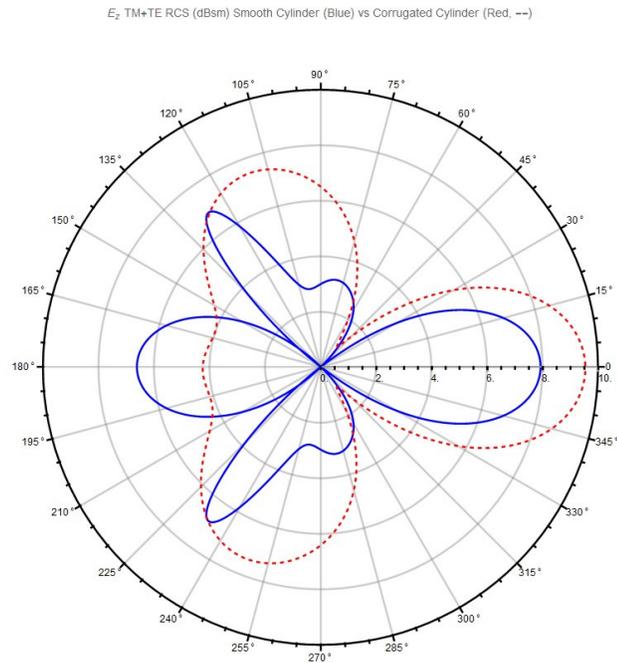


Figure 7-118 Polar Plot form of RCS dBsm for Ez of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

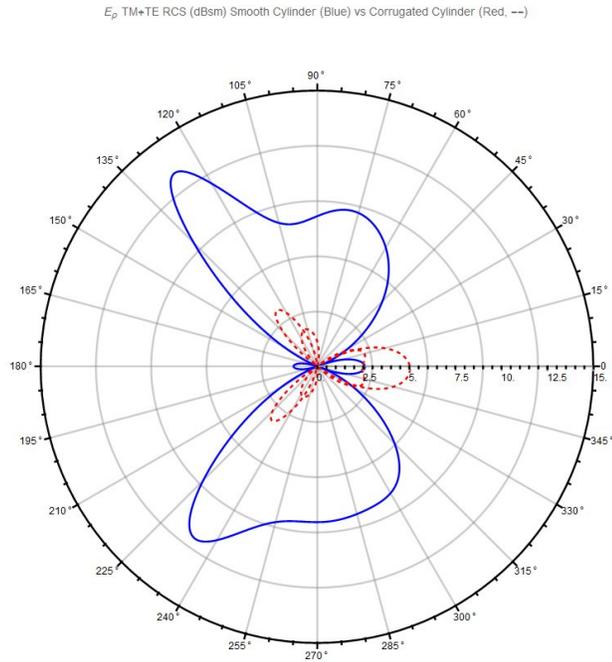


Figure 7-119 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

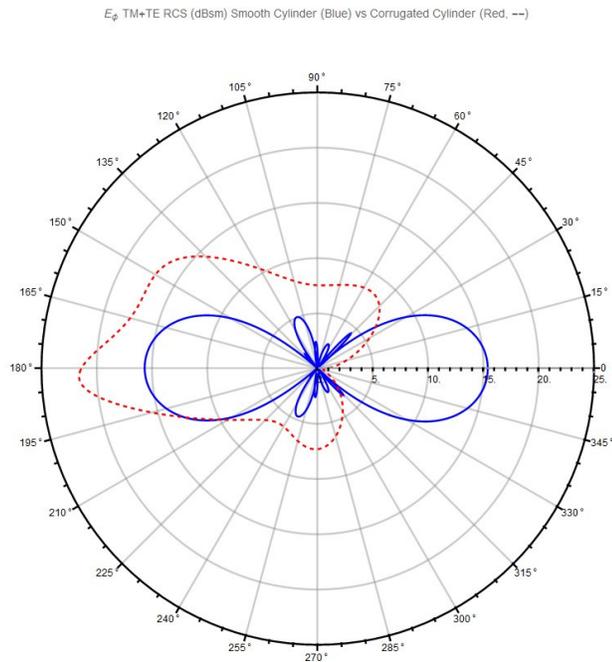


Figure 7-120 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

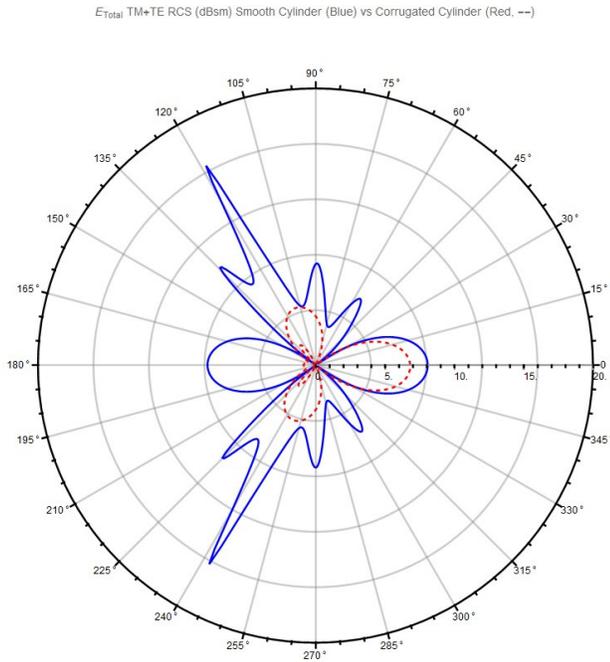


Figure 7-121 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

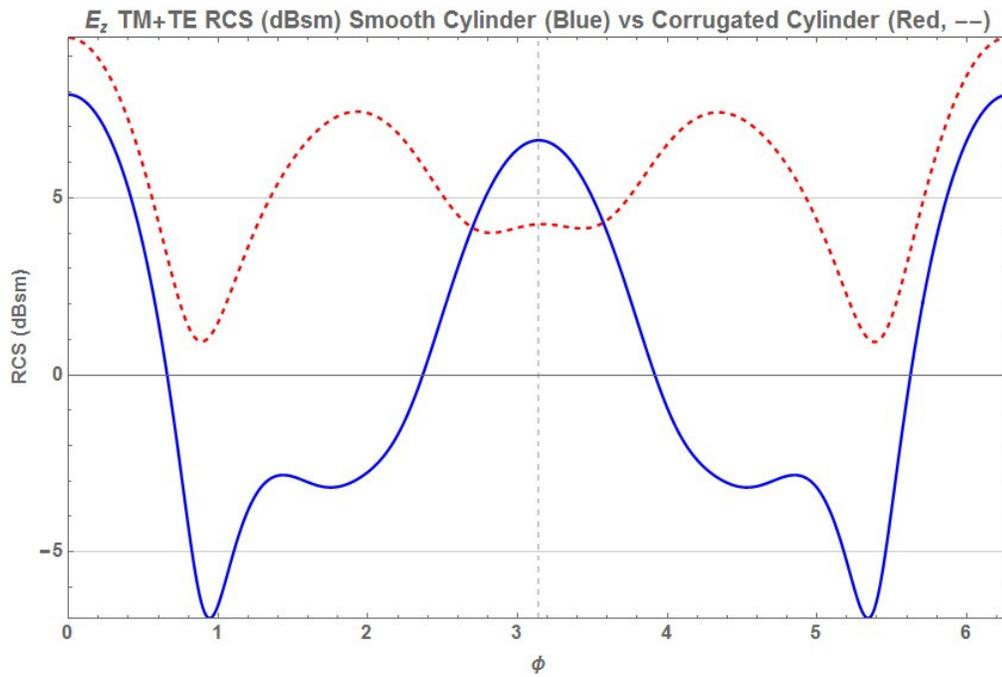


Figure 7-122 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

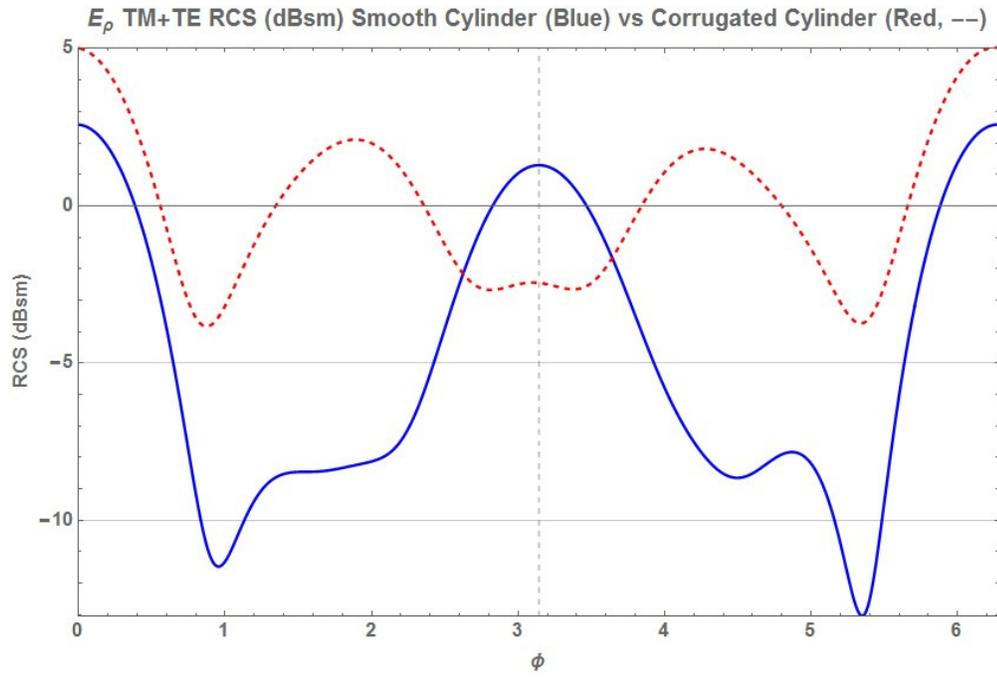


Figure 7-123 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

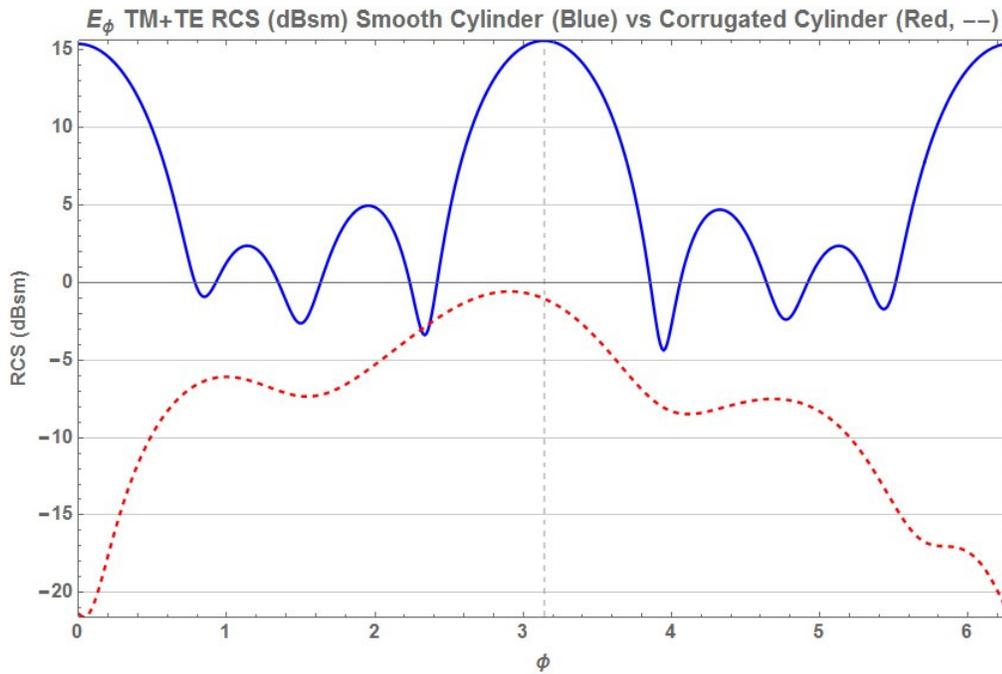


Figure 7-124 XY Plot form of RCS dBsm for E_ϕ of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

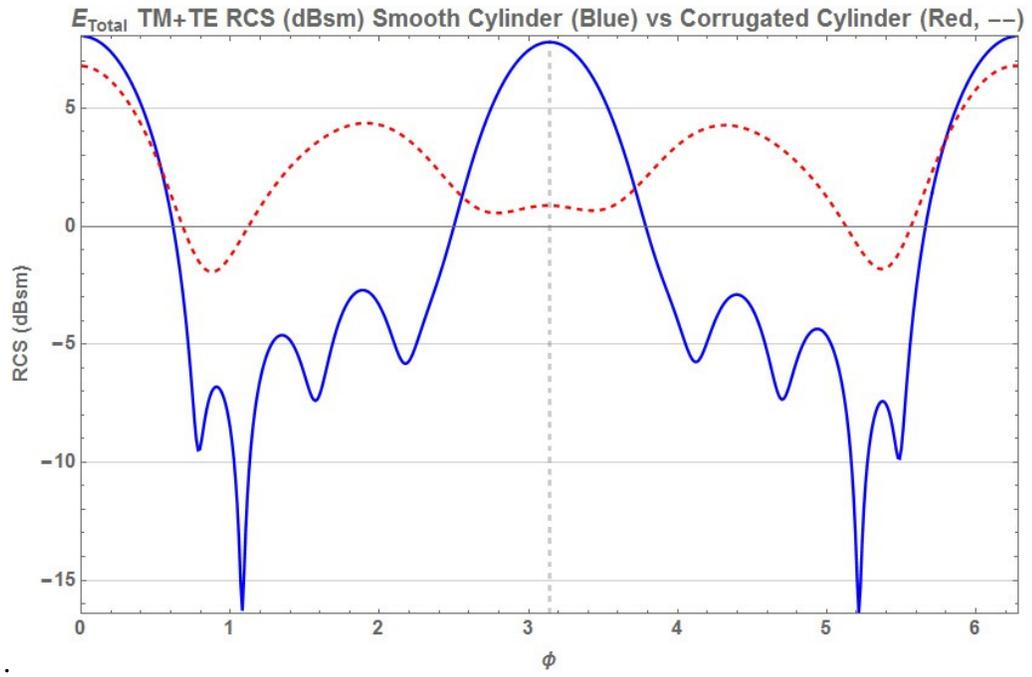


Figure 7-125 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

Table 19 Detailed parameters summary for changing ρ plots of Run a_plus_b.2.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.002λ	-	-	-	-
b	$2. \lambda$	-	-	-	-
$\rho 1$	1.998λ	-	-	-	-
$\rho 2$	$2. \lambda$	-	-	-	-
ρ range	-	1.7982λ	$12. \lambda$	0.0185825λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$0.25 a \&\& 0.0005 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θi	55. Deg	-	-	-	-
ϕi	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.004	-	-	-	-
max allowable l	0.8537	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

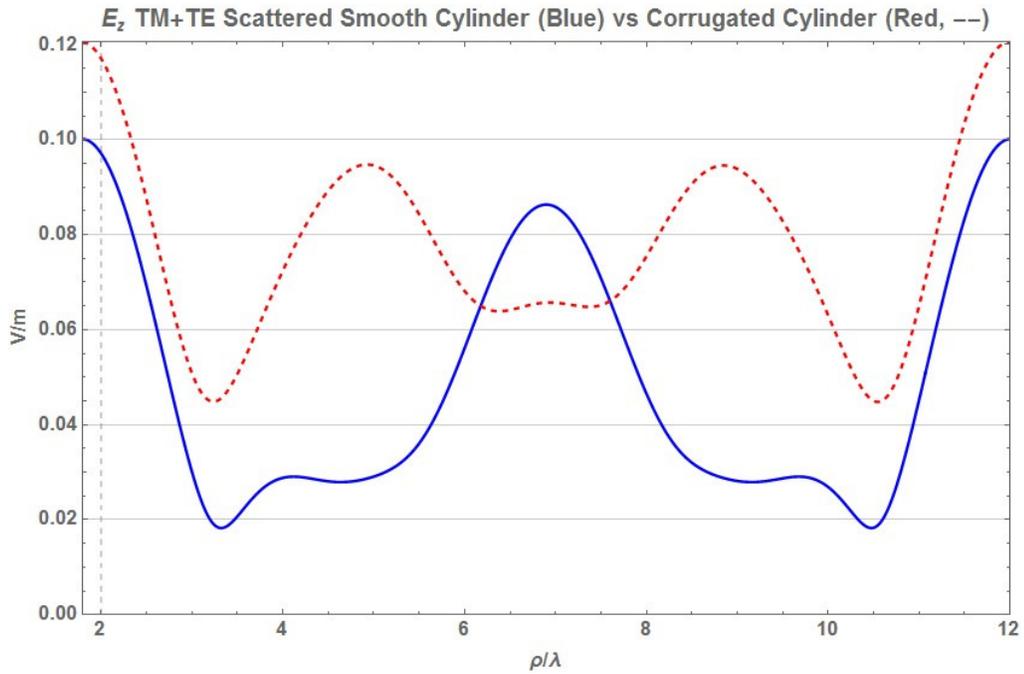


Figure 7-126 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

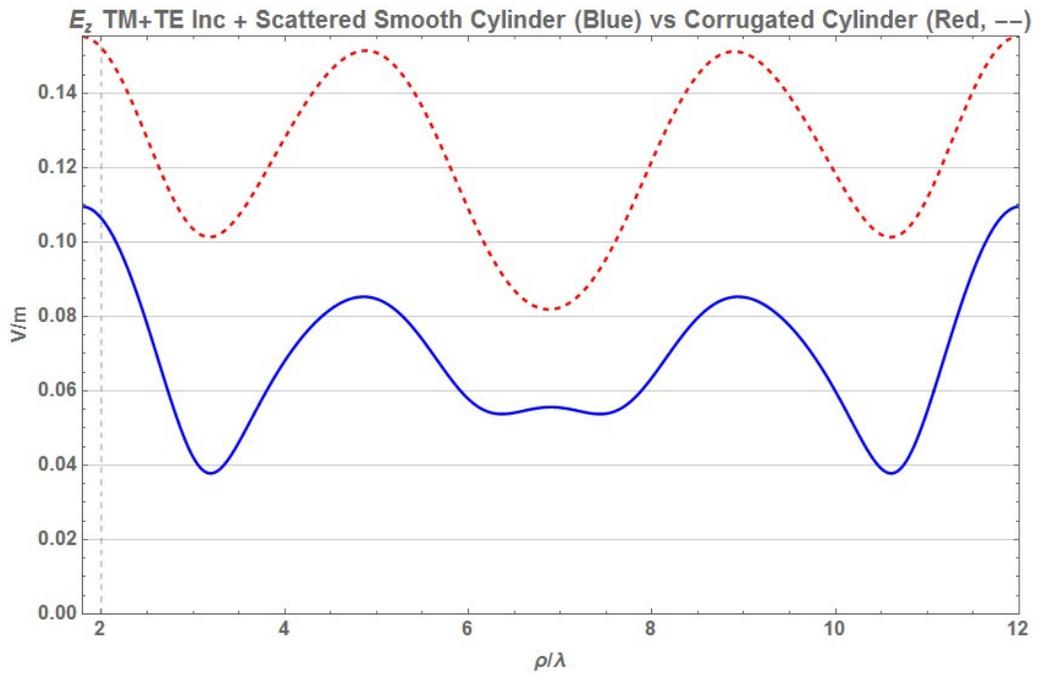


Figure 7-127 XY Plot of Scattered + Incident Field Amplitude, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

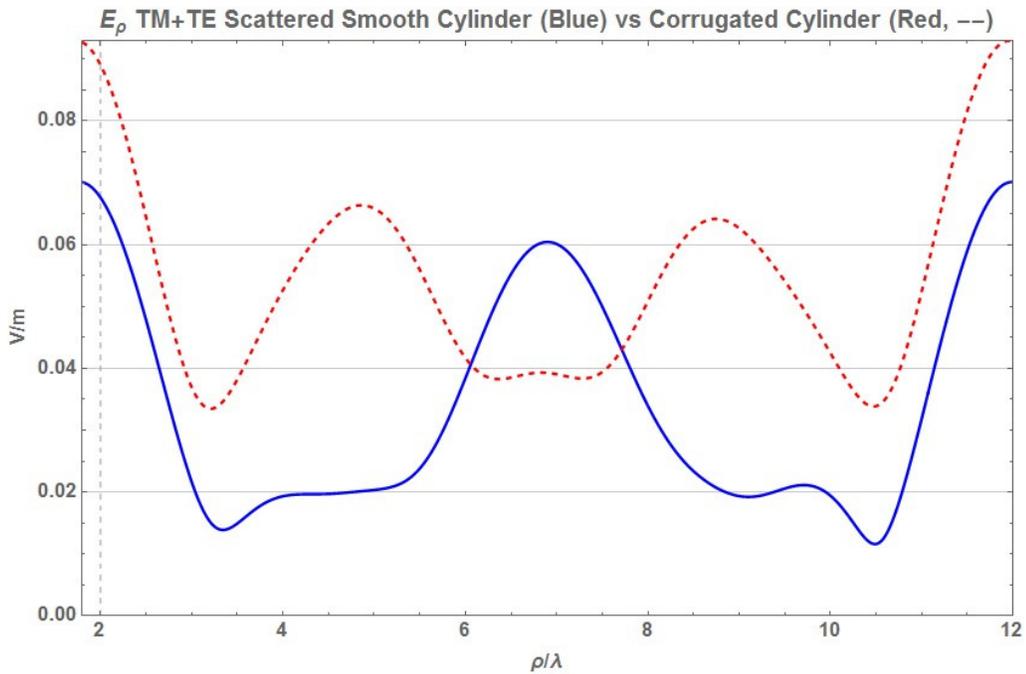


Figure 7-128 XY Plot of Scattered Field Amplitude Only, for E_p , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

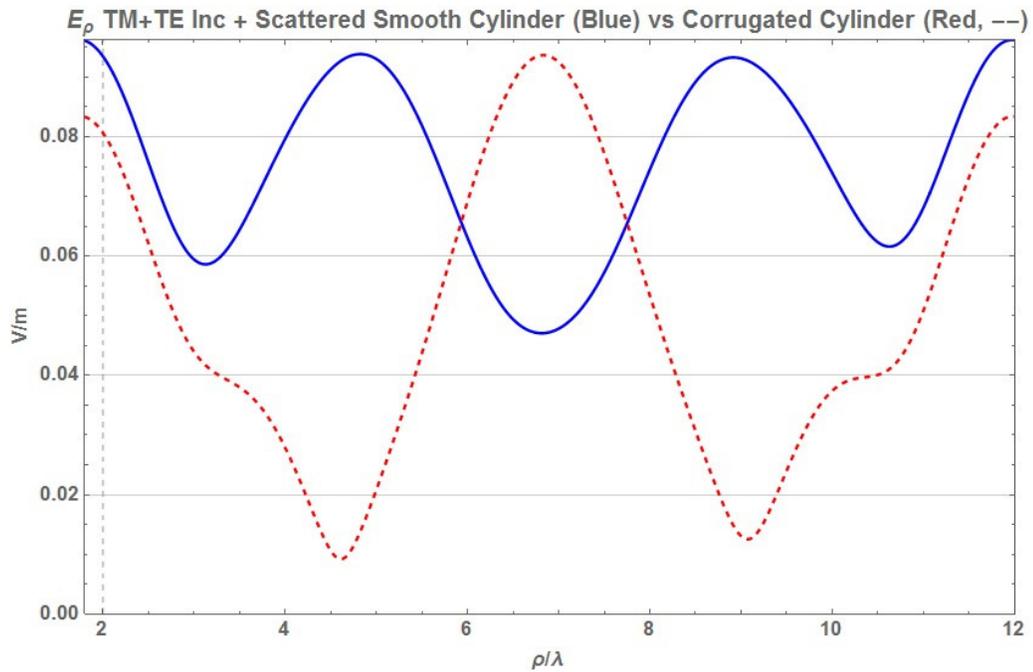


Figure 7-129 XY Plot of Scattered + Incident Field Amplitude, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

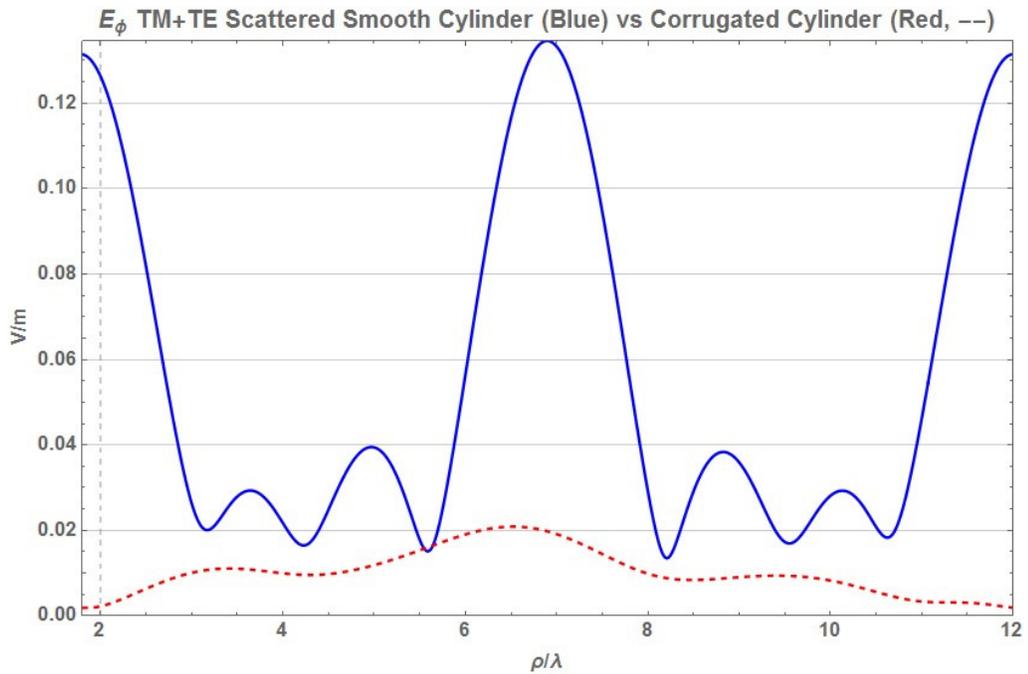


Figure 7-130 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

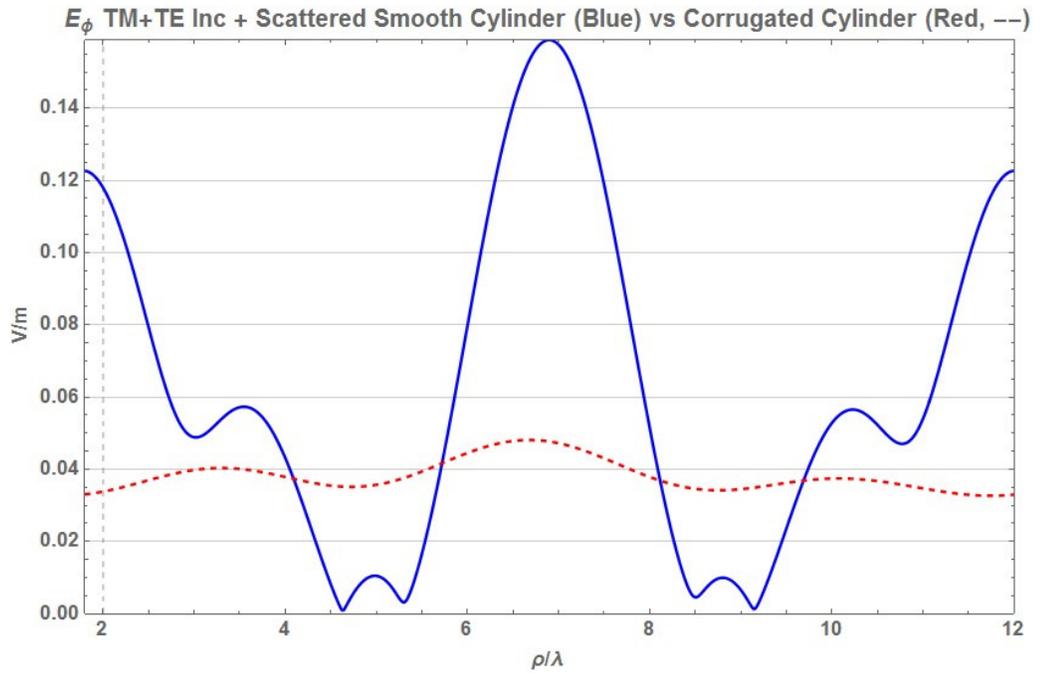


Figure 7-131 XY Plot of Scattered + Incident Field Amplitude, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

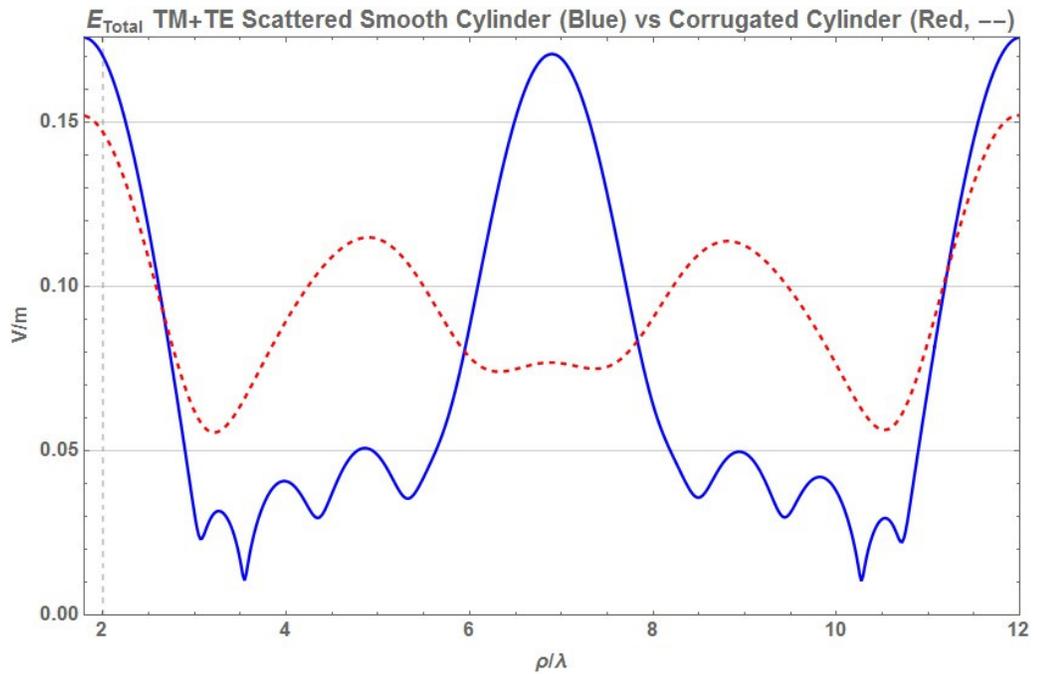


Figure 7-132 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

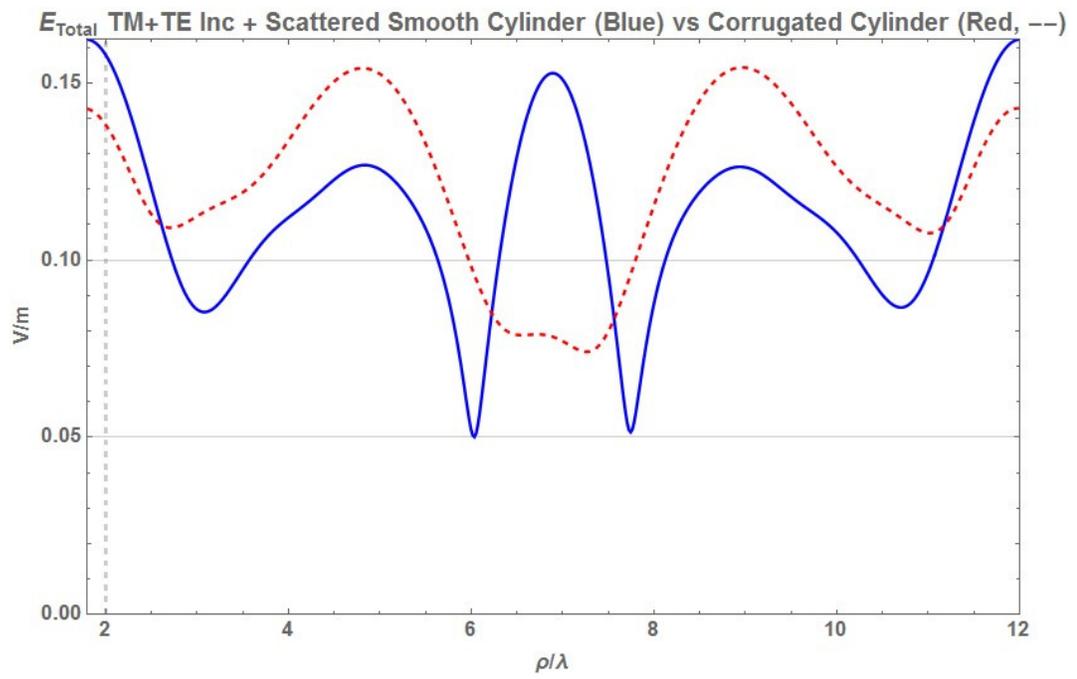


Figure 7-133 XY Plot of Scattered + Incident Field Amplitude, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.2.0.0

7.5.9 Run a_plus_b.0.1.0.0 (b=0.1λ, a=b*.001, ρ2=0.1λ, m=0)

Table 20 Detailed parameters summary for changing φ plots of Run a_plus_b.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	1.50105 × 10 ¹⁰ Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.0001 λ	-	-	-	-
b	0.1 λ	-	-	-	-
ρ1	0.0999 λ	-	-	-	-
ρ2	0.1 λ	-	-	-	-
φ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	1. λ	-	-	-	-
z (observed)	0.25 a && 0.000025 λ	-	-	-	-
Matching Points	-	-	-	-	7
θi	55. Deg	-	-	-	-
φi	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

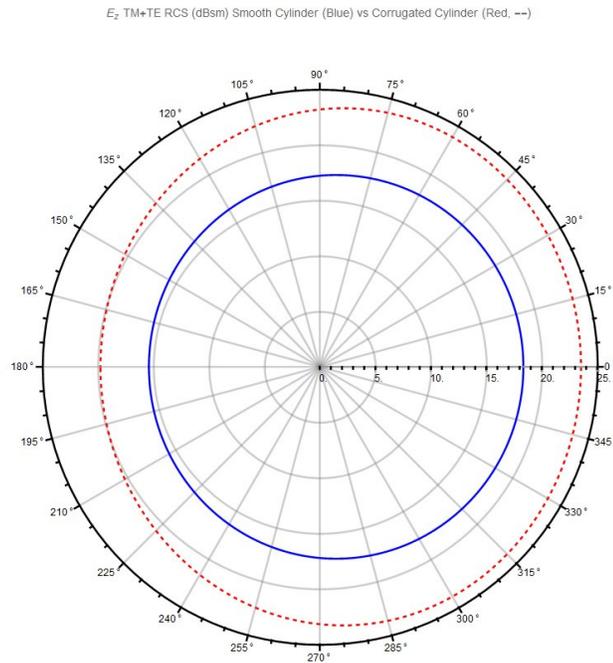


Figure 7-134 Polar Plot form of RCS dBsm for Ez of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

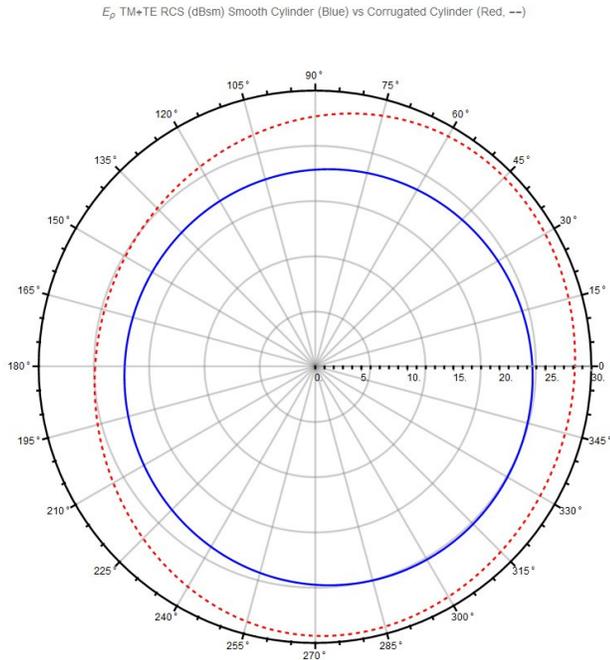


Figure 7-135 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

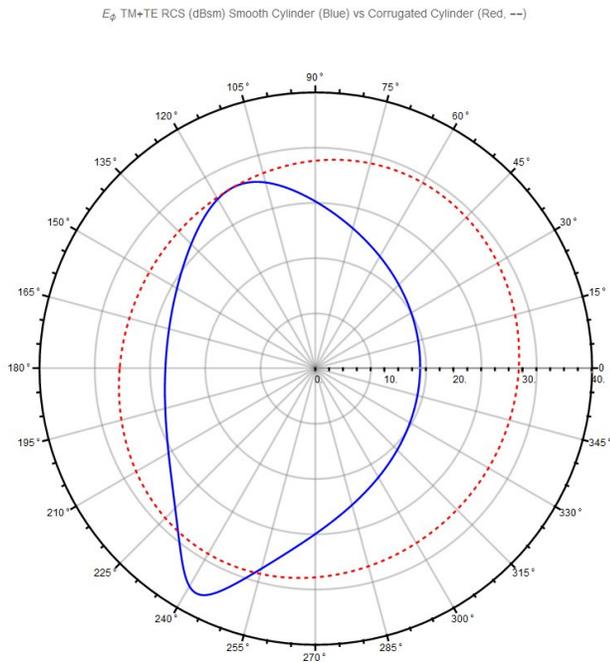


Figure 7-136 Polar Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE modes and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

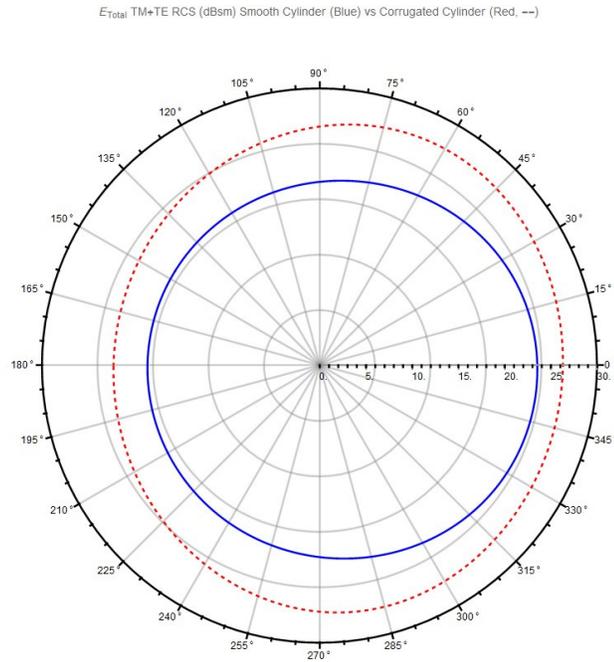


Figure 7-137 Polar Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

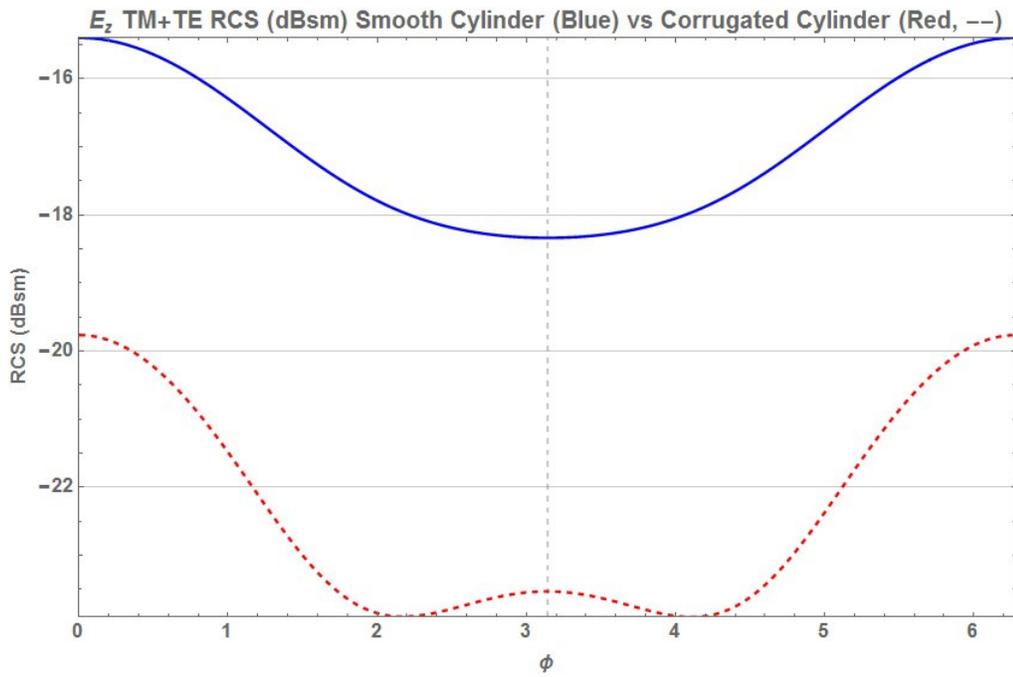


Figure 7-138 XY Plot form of RCS dBsm for E_z of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

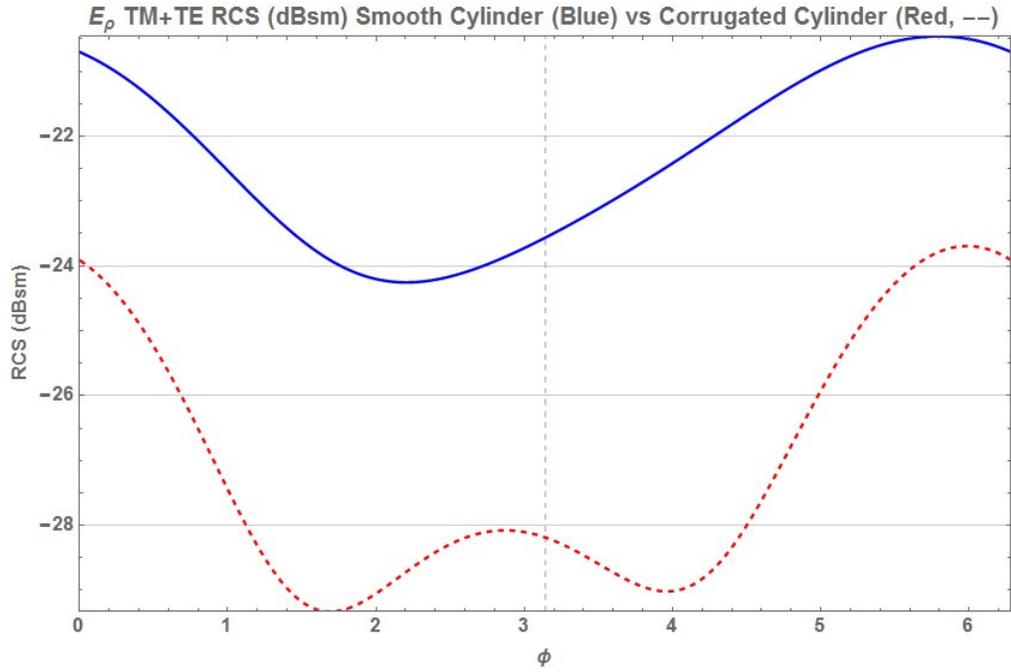


Figure 7-139 XY Plot form of RCS dBsm for E_{ρ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

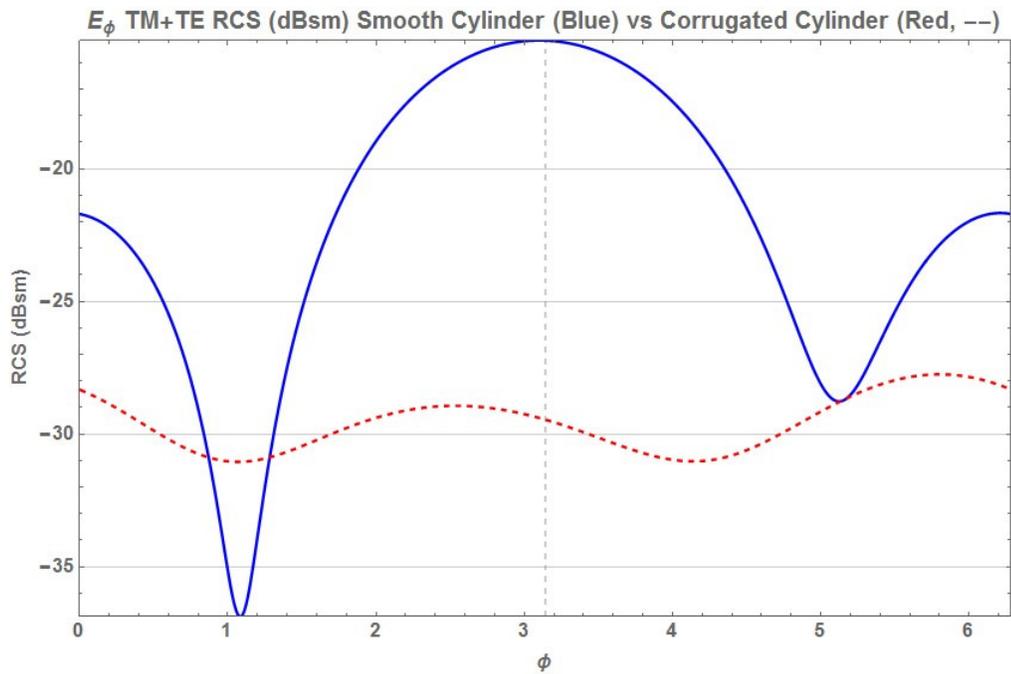


Figure 7-140 XY Plot form of RCS dBsm for E_{ϕ} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

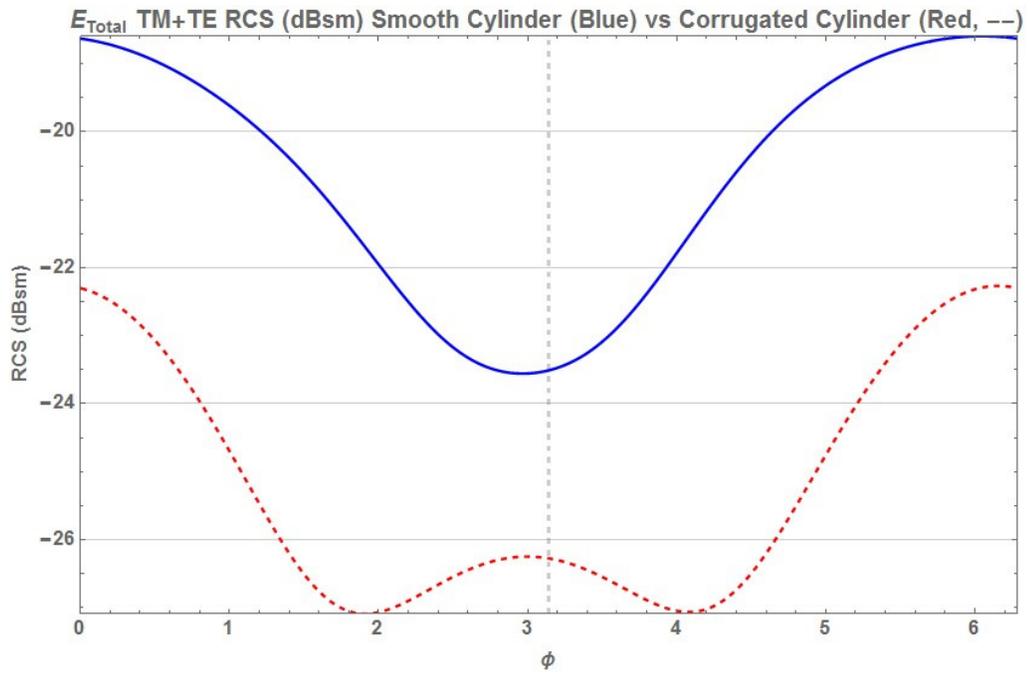


Figure 7-141 XY Plot form of RCS dBsm for E_{Total} of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.1.0.0

Table 21 Detailed parameters summary for changing ρ plots of Run a_plus_b.0.1.0.0

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	0.00265258 A/m	-	-	-	-
λ	0.019986 m	-	-	-	-
Frequency	1.50105×10^{10} Hz	-	-	-	-
a	0.0001λ	-	-	-	-
b	0.1λ	-	-	-	-
ρ_1	0.0999λ	-	-	-	-
ρ_2	0.1λ	-	-	-	-
ρ range	-	0.08991λ	10.1λ	0.0182333λ	550
ϕ (observed)	37. Deg	-	-	-	-
z (observed)	$0.25 a \&\& 0.000025 \lambda$	-	-	-	-
Matching Points	-	-	-	-	7
θ_i	55. Deg	-	-	-	-
ϕ_i	37. Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.0002	-	-	-	-
max allowable l	0.042685	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

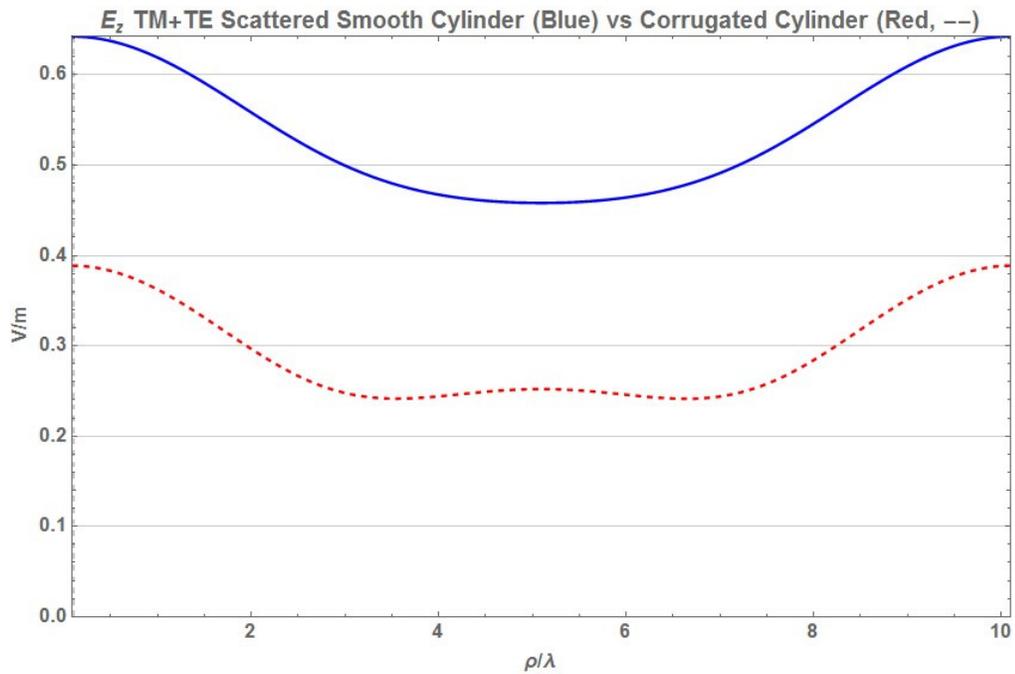


Figure 7-142 XY Plot of Scattered Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

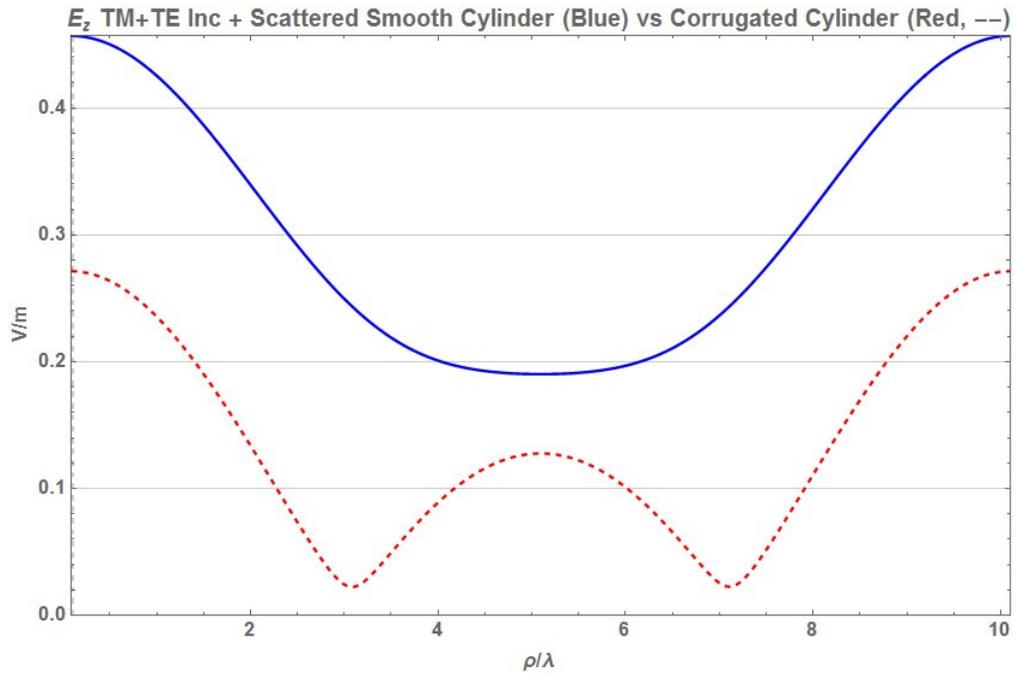


Figure 7-143 XY Plot of Scattered + Incident Field Amplitude Only, for E_z , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

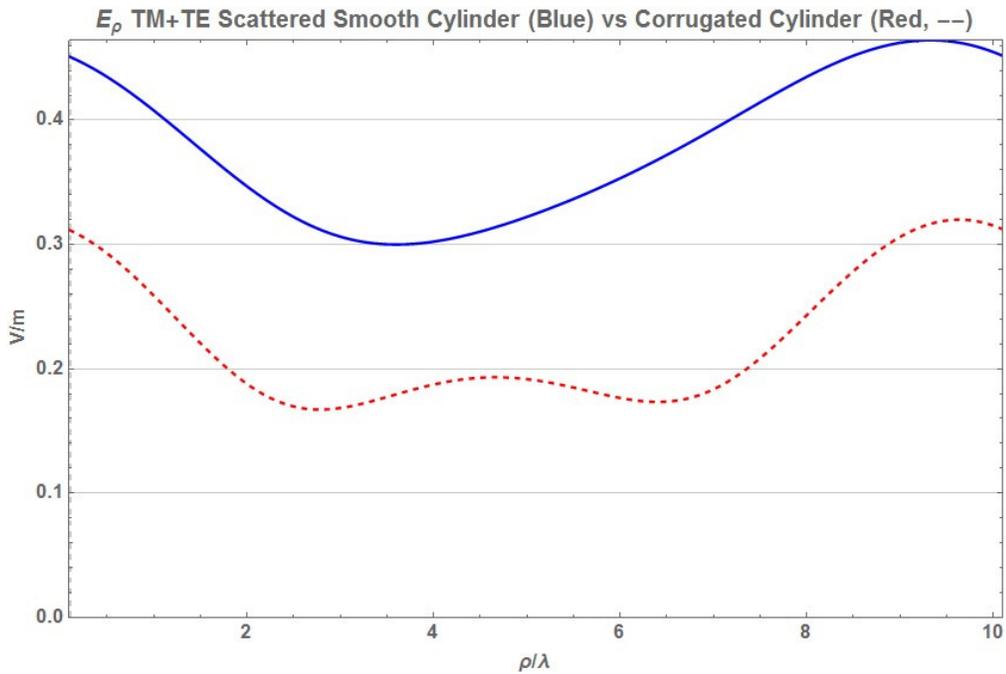


Figure 7-144 XY Plot of Scattered Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

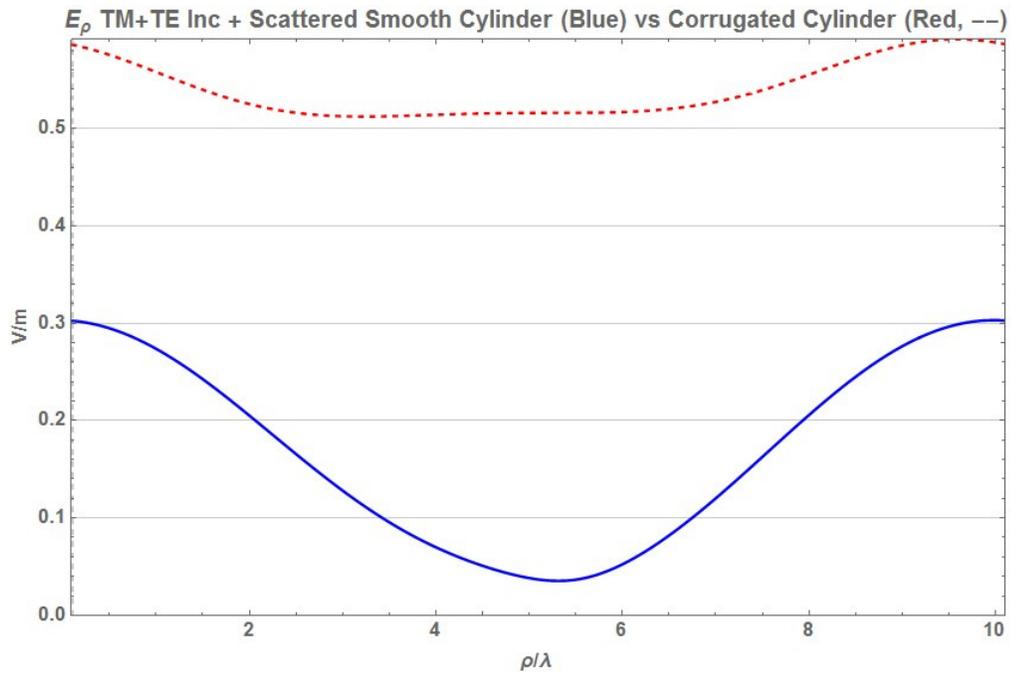


Figure 7-145 XY Plot of Scattered + Incident Field Amplitude Only, for E_ρ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

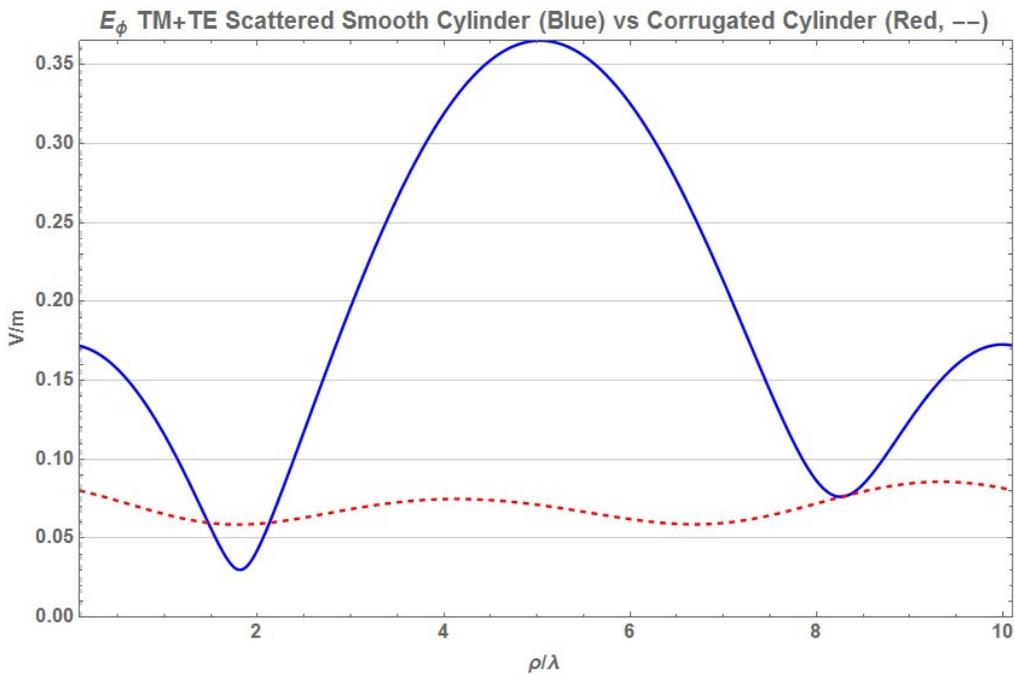


Figure 7-146 XY Plot of Scattered Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

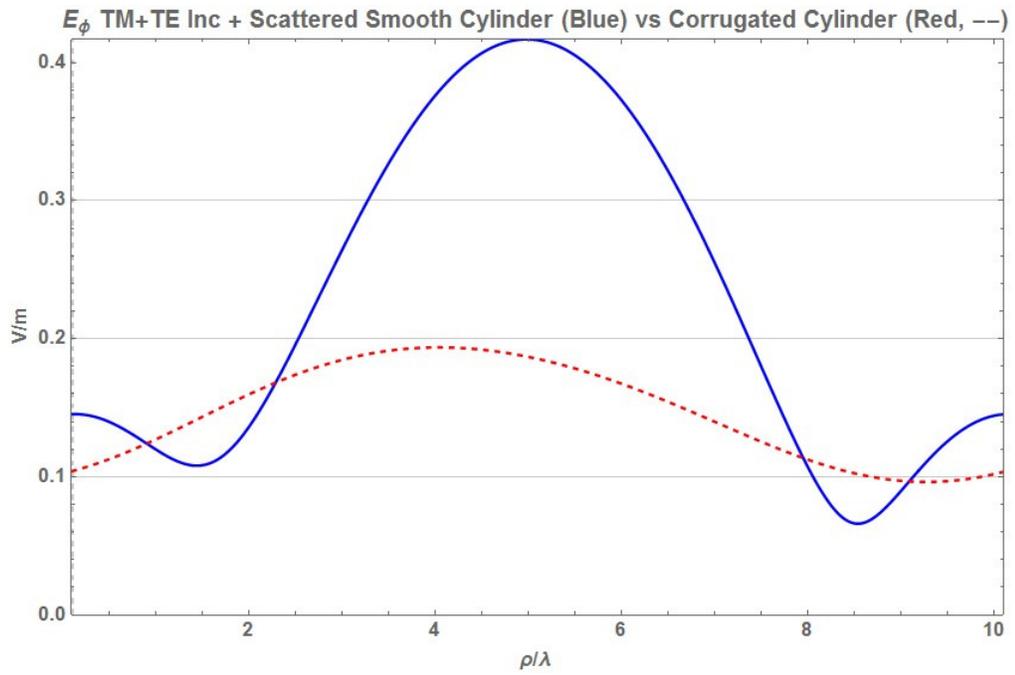


Figure 7-147 XY Plot of Scattered + Incident Field Amplitude Only, for E_ϕ , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

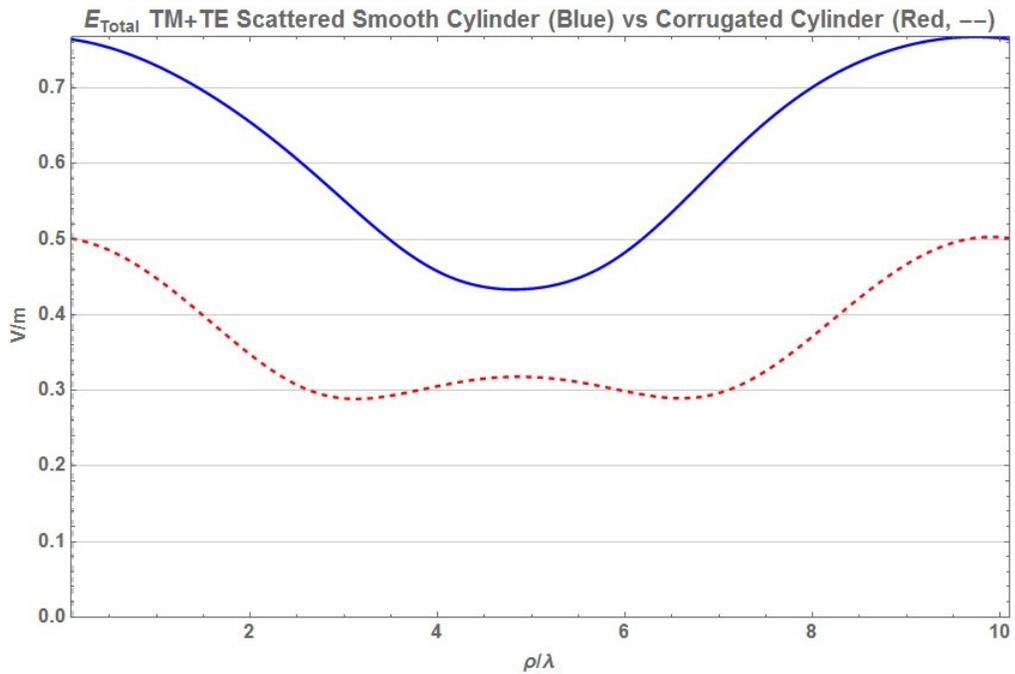


Figure 7-148 XY Plot of Scattered Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

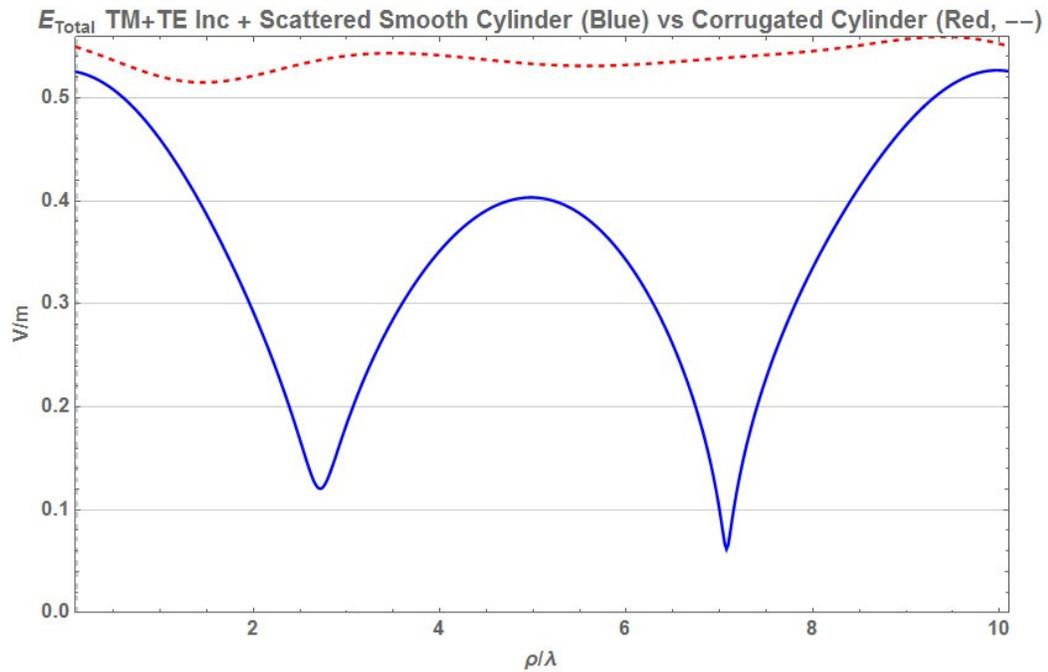


Figure 7-149 XY Plot of Scattered + Incident Field Amplitude Only, for E_{Total} , of the Smooth Cylinder TM + TE mode and Corrugated Cylinder hybrid mode for Run a_plus_b.0.10.0.0

7.5.10 Comparison to Other Corrugated Cylinder Methods

Table 22 Detailed parameters summary for changing ϕ plots of Run a_plus_b.compare

	value	min	max	delta	Qty of Points
E0	1. V/m	-	-	-	-
H0	2.65258×10^{-7} A/m	-	-	-	-
λ	1.50105×10^{10} Hz	-	-	-	-
Frequency	0.019986 m	-	-	-	-
a	0.2 λ	-	-	-	-
b	0.1 λ	-	-	-	-
$\rho 1$	0.4 λ	-	-	-	-
$\rho 2$	0.5 λ	-	-	-	-
ϕ range	-	0.327273 Deg	359.673 Deg	0.654545 Deg	550
ρ (observed)	10. λ	-	-	-	-
z (observed)	0.25 a && 0.05 λ	-	-	-	-
Matching Points	-	-	-	-	7
θi	85. Deg	-	-	-	-
ϕi	0.01 Deg	-	-	-	-
n	-	-3	3	1	7
l	-	0	0	1	1
m	-	0	0	1	1
max allowable m	0.4	-	-	-	-
max allowable l	0.273853	-	-	-	-
Boundary	Boundary a+b	-	-	-	-

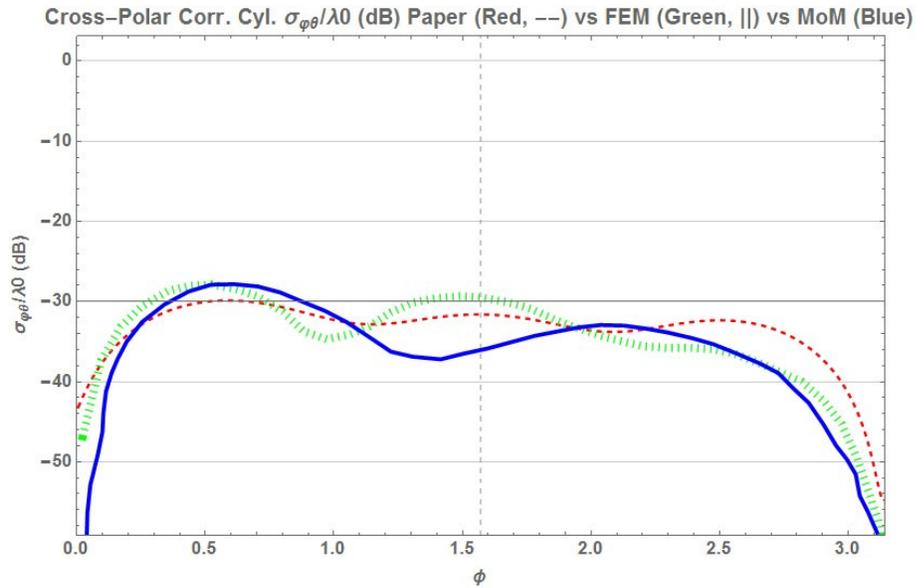


Figure 7-150 XY Plot form of Cross-Polar Corrugated Cylinder $\sigma_{\phi\theta}/\lambda_0$ (dB) for Run a_plus_b. Compared with results of the finite element method (FEM) and method of moments (MoM) from [27]

7.5.11 Varied Dielectric Constant with Comparisons

The scattered axial field (E_z for TM_z mode) vs ϕ is plotted below in Figure 7-151 for several cases of interest with a varying dielectric constant, ϵ_r , where ϵ_r is selected to be a real value only. It is evident that the corrugated cylinder with dielectric loading has a generally reduced scattered field compared to the smooth cylinder.

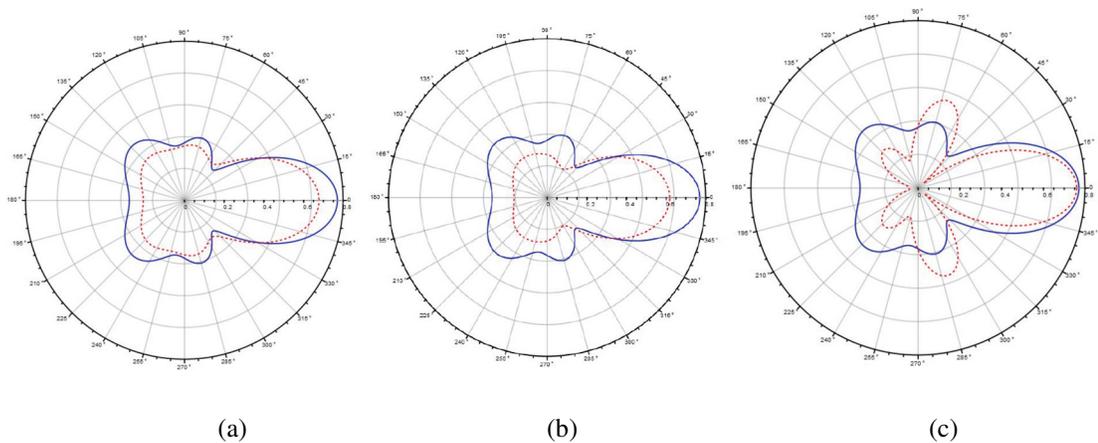


Figure 7-151 Comparison of scattered axial fields of a smooth cylinder (solid line) with the corrugated cylinder (dotted line) with lossless dielectric loading of dielectric constant: $\epsilon_r=1$ a) $\epsilon_r=4$; b) $\epsilon_r=9$; c)

Now, the case of lossy dielectric loading (ϵ_r is a complex value) is examined with results of the scattered axial field (E_z for TM_z mode) vs ϕ is plotted below in Figure 7-152 for several cases. ϵ_r .

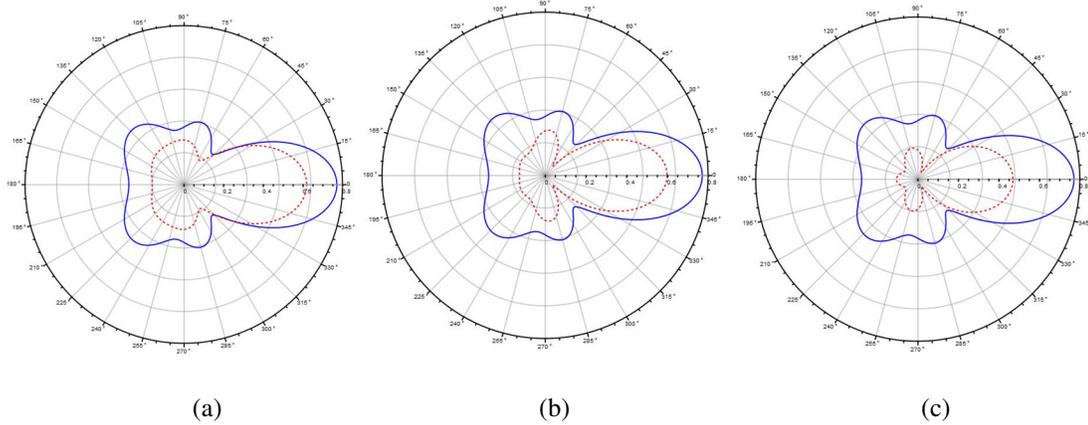


Figure 7-152 Axial scattered fields of a smooth cylinder (solid line) and corrugated cylinder (dotted line) with lossy dielectric loading. Dielectric constants: a) $\epsilon_r=4 - j1$; b) $\epsilon_r=6.29$; c) $\epsilon_r=6.29 - j1.73$

It is evident that a complex permittivity yields a generally smaller scattered field. The dielectric constants in (b) and (c) were chosen to correspond to those found in [33]. These results can also be found in [34] with some additional discussion.

7.6 Conclusions

This dissertation presented an alternate method to calculate the scattered field of a corrugated cylinder. The method of utilizing a hybrid mode of TM_z and TE_z with a radial waveguide representation of the corrugation was demonstrated.

In the comparison between the periodic corrugated cylinder model from this research and the model of a smooth cylinder, there was a lot of agreement between the fields of both models with the exception of the E_ϕ fields. There are a few reasons for this:

- This technique is an approximation and as such, will have errors

- More specifically, the corrugated cylinder is approximated to a smooth cylinder, by shrinking the ‘a’ dimension, though not eliminated, so there will be some artifacts that make it different than a smooth cylinder
- Also, the cross-polarization nature of the problem allows fields to manifest themselves between TE and TM modes

What’s important to note is what the limitations are and what the capabilities are of a given method, to know when to best apply it or to seek an alternative method.

Overall, good agreement was attained between the periodic corrugated cylinder model from this research and the model of a smooth cylinder, for small corrugation openings approximating a smooth cylinder, where the relative dimensions of the corrugated cylinder were much greater than λ (optical region as indicated in Figure 7-1). There was some agreement in this same comparison at the Rayleigh scattering region, where the relative dimensions of the corrugated cylinder were much less than λ . There was also good agreement attained between the periodic corrugated model of this research when compared to the referenced periodic corrugated cylinder FEM and MoM techniques, which was modeled in the Rayleigh scattering region.

It is concluded that the techniques discussed in this dissertation is most suitable for the optical region, where the λ of interest is much smaller than the dimensions of the periodic corrugated cylinder of interest. Also, from the results when compared to the FEM and MoM techniques, it is concluded that the Rayleigh scattering region, where the λ of interest is much larger than the dimensions of the periodic corrugated cylinder of interest, is suitable for the technique presented in this research.

7.7 Open Questions for Future Research

There were limitations discovered of the presented method that merits future research. Many challenges were faced, especially in the numerical solving of the unknown expansion coefficients which could benefit from improved methods. Also, there were many techniques that were investigated but not implemented. Here is a list of future work that can enhance or build on this research:

- Improve or replace the computationally expensive loop solve method.
- Summation truncation using the symmetry of the summation as in [12, p. 603].
- Using Poisson's sum formula to reduce any of the infinite series equations prior to truncation [34].
- Comparison models for varying the permittivity of region I, representing the dielectric loading of the periodic corrugated cylinder
- Using Eigenvalues and Eigenvectors solutions approach for solving the unknown expansion coefficients
- Using a continuous periodic function approximation to asymptotically represent the periodicity of the corrugated cylinder
- Applying the asymptotic boundary condition method, [26], for improving solution agreement in regimes where the relative dimensions of the corrugated cylinder are that of λ .
- Construction and testing of a physical model for further comparison

APPENDICES

APPENDIX A

Mathematica® code for the modeling and comparison of the scattered field of a periodic cylinder and smooth circular cylinder

Plane-wave Scattering of a Periodic Corrugated Cylinder

```

%%4770: ClearAll["Global*"]
SetDirectory["C:\Users\Hamed\Google Drive\Dissertation\FinalData"];
(* Output Directory*)
    
```

Electromagnetic Constants, Adjustable, & Calculated Parameters

```

%%4772: zerooffset = 0; (*Factor to eliminate zeros that would show up in denominators*)
    
```

Electromagnetic Constants

```

%%4773: mu0 = 4*pi/10^7;
%%4774: epsilon0 = 1/(36*pi*10^9);
%%4775: epsilon = 1/sqrt(epsilon0*mu0);
%%4776: eta0 = sqrt(mu0/epsilon0);
    
```

Incident Electric and Magnetic Field Parameters

```

%%4777: HD = 1;
%%4778: HD = eta0/eta0;
(*H0=1;*)
%%4779: lambda0 = 0.019396;
%%4780: phi = phi ->
see section 'User Inputs-Geometric Parameters' for value of incident phi, phi
    
```

```

%%4782: theta = (55*pi)/180;
theta = pi - theta; (*Balanis, p 615*)
    
```

Material Electromagnetic Parameters

```

%%4783: de1 = 1; (*Region 1 relative dielectric constant*)
%%4784: de2 = 1; (*Region 2 relative dielectric constant*)
%%4785: dm1 = 1; (*Region 1 relative permeability constant*)
%%4786: dm2 = 1; (*Region 2 relative permeability constant*)
    
```

Electromagnetic Calculated Parameters

```

%%4787: f0 = c/lambda0; (* Frequency (hertz or 1/seconds)*)
%%4788: w0 = 2*pi*f0; (* Angular velocity (rad/seconds)*)
%%4789: e1 = de1*epsilon0; (* Region 1 permittivity (farads/meter)*)
%%4790: e2 = de2*epsilon0; (* Region 2 permittivity (farads/meter)*)
%%4791: mu1 = dm1*mu0; (* Region 1 permeability (henries/meter)*)
%%4792: mu2 = dm2*mu0; (* Region 2 permeability (henries/meter)*)
%%4793: eta1 = Sqrt[mu1/e1]; (* Intrinsic impedance in regin 1 (ohm)*)
%%4794: eta2 = Sqrt[mu2/e2]; (* Intrinsic impedance in region 2 (ohm)*)
%%4795: beta0 = w0*Sqrt[mu0*epsilon0]; (* Beta (wavenumber) in free space (rad/meter)*)
%%4796: k1 = w0*Sqrt[mu1*epsilon1]; (* Wavenumber in region 1 (rad/meter)*)
%%4797: k2 = w0*Sqrt[mu2*epsilon2]; (* Wavenumber in region 2 (rad/meter)*)
%%4798: Z2 = w0*mu2/k2; (*Intrinsic Impedance of region 2 *)
    
```

Wavenumber of Fields

```

%%4799: km[m_] := N[(-m - zerooffset)*beta1/a]; (*z-axis of field in region 1*)
%%4800: km[m_] := Sqrt[k1^2 - (km[m]^2)]; (*rho-axis of field in region 1*)
%%4801: kx1[1_] := (k2*Cos(theta) + (2*pi + beta1)/(b+a)); (*z-axis of field in region 2*)
%%4802: ky1[1_] := Sqrt[k2^2 - (kx1[1]^2)]; (*rho-axis of field in region 2*)
    
```

Corrugated Cylinder Region I, II, and 'b' Equations and

Variables

Region I Fields - Equations and Variables

Equations [NOT USED]

```

%%4803: E1[Ann_] := Ann**Ann;
%%4804: E1[Ann_] := Ann**Ann;
%%4805: E1phi[Ann_, Bnm_] := (Ann**Ann) + (Ann**Ann);
%%4806: E1phi[Ann_, Bnm_] := (Ann**Ann) + (Ann**Ann);
%%4807: E1rho[Ann_, Bnm_] := (Ann**Ann) + (Ann**Ann);
%%4808: E1rho[Ann_, Bnm_] := (Ann**Ann) + (Ann**Ann);
    
```

Variables

```

%%4809: hnmJeq[theta_, x_, rho_] := e^{i*k*x} Cos[k*x] Sin[theta - x/2] km[m]
(HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho] HankelH1[n, km[m] rho1]) /
(HankelH2[n, km[m] rho1]);
%%4810: hnmJeq[theta_, x_, rho_] :=
e^{i*k*x} Sin[k*x] Sin[theta - x/2] km[m] (HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho]
(km[m] HankelH1[n-1, km[m] rho1] - n HankelH1[n, km[m] rho1])) /
(km[m] HankelH2[n-1, km[m] rho1] - n HankelH2[n, km[m] rho1]);
%%4811: kmJeq[theta_, x_, rho_] := 1/n e^{i*k*x} km[m] / km[m]^2 Cos[theta - x/2] km[m]
(HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho] HankelH1[n, km[m] rho1]) /
HankelH2[n, km[m] rho1];
%%4812: kmJeq[theta_, x_, rho_] := i*mu1*w0 e^{i*k*x} Sin[theta - x/2] km[m]
(1/2 km[m] (HankelH1[n-1, km[m] rho] - HankelH1[n+1, km[m] rho]) -
(km[m] (HankelH2[n-1, km[m] rho] - HankelH2[n+1, km[m] rho])
(km[m] HankelH1[n-1, km[m] rho1] - n HankelH1[n, km[m] rho1])) /
(2 (km[m] HankelH2[n-1, km[m] rho1] - n HankelH2[n, km[m] rho1]));
    
```

```

%%4813: omJeq[theta_, x_, rho_] := -i*epsilon0 e^{i*k*x} / km[m]^2 Cos[theta - x/2] km[m]
(1/2 km[m] (HankelH1[n-1, km[m] rho] - HankelH1[n+1, km[m] rho]) -
(km[m] (HankelH2[n-1, km[m] rho] - HankelH2[n+1, km[m] rho])
HankelH1[n, km[m] rho1]) / (2 HankelH2[n, km[m] rho1]);
%%4814: pmJeq[theta_, x_, rho_] :=
1/n e^{i*k*x} km[m] / km[m]^2 Sin[theta - x/2] km[m] (HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho]
(km[m] HankelH1[n-1, km[m] rho1] - n HankelH1[n, km[m] rho1])) /
(km[m] HankelH2[n-1, km[m] rho1] - n HankelH2[n, km[m] rho1]);
%%4815: rmJeq[theta_, x_, rho_] := -i e^{i*k*x} km[m] / km[m]^2 Cos[theta - x/2] km[m]
(1/2 km[m] (HankelH1[n-1, km[m] rho] - HankelH1[n+1, km[m] rho]) -
(km[m] (HankelH2[n-1, km[m] rho] - HankelH2[n+1, km[m] rho])
HankelH1[n, km[m] rho1]) / (2 HankelH2[n, km[m] rho1]);
%%4816: smJeq[theta_, x_, rho_] := (mu1*w0) / km[m]^2 e^{i*k*x} Sin[theta - x/2] km[m]
(HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho]
(km[m] HankelH1[n-1, km[m] rho1] - n HankelH1[n, km[m] rho1])) /
(km[m] HankelH2[n-1, km[m] rho1] - n HankelH2[n, km[m] rho1]);
%%4817: tmJeq[theta_, x_, rho_] := -w0*epsilon1 / km[m]^2 e^{i*k*x} Cos[theta - x/2] km[m]
(HankelH1[n, km[m] rho] - HankelH2[n, km[m] rho] HankelH1[n, km[m] rho1]) /
HankelH2[n, km[m] rho1];
%%4818: umJeq[theta_, x_, rho_] := -i e^{i*k*x} km[m] / km[m]^2 Sin[theta - x/2] km[m]
(1/2 km[m] (HankelH1[n-1, km[m] rho] - HankelH1[n+1, km[m] rho]) -
(km[m] (HankelH2[n-1, km[m] rho] - HankelH2[n+1, km[m] rho])
(km[m] HankelH1[n-1, km[m] rho1] - n HankelH1[n, km[m] rho1])) /
(2 (km[m] HankelH2[n-1, km[m] rho1] - n HankelH2[n, km[m] rho1]));
    
```

Region II Fields - Equations and Variables

Equations [NOT USED]

```

1944770: EIRib(Dn1b_) := bnj + (anlj**Cn1b);
1944771: EIRia(Cn1a_) := bnj + (anlj**Cn1a);
1944772: EIRib(Dn1b_) := fnj + (gnlj**Dn1b);
1944773: EIRia(Dn1a_) := fnj + (gnlj**Dn1a);
1944774: EIPIhb(Cn1b_, Dn1b_) := dnj + ((m1j**Cn1b) + (enlj**Dn1b));
1944775: EIPIha(Cn1a_, Dn1a_) := dnj + ((m1j**Cn1a) + (enlj**Dn1a));
1944776: EIPIhb(Cn1b_, Dn1b_) := mnj + ((m1j**Cn1b) + (qn1j**Dn1b));
1944777: EIPIha(Cn1a_, Dn1a_) := mnj + ((m1j**Cn1a) + (qn1j**Dn1a));
1944778: EIRIhb(Cn1b_, Dn1b_) := ynj + ((vn1j**Cn1b) + (wn1j**Dn1b));
1944779: (*Not utilized for solving unknown coeff.*);
1944780: EIRIha(Cn1a_, Dn1a_) := ynj + ((vn1j**Cn1a) + (wn1j**Dn1a));
1944781: (*Not utilized for solving unknown coeff.*);
1944782: EIRIhb(Cn1b_, Dn1b_) := dnj + ((m1j**Cn1b) + (yn1j**Dn1b));
1944783: (*Not utilized for solving unknown coeff.*);
1944784: EIRIha(Cn1a_, Dn1a_) := dnj + ((m1j**Cn1a) + (yn1j**Dn1a));
1944785: (*Not utilized for solving unknown coeff.*);
    
```

Variables

```

1944786: bnjjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} EO Sin(θ) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep in summation form. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1] *)
1944787: anljjeq(θ_, x_, ρ_) := e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n}); (*H2^+=[Dn1]-[An1][Cn1] *)
1944788: fnjjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} EO Sin(θ) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep sum. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1] *)
1944789: gnljjeq(θ_, x_, ρ_) := e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n}); (*H2^+=[Dn1]-[An1][Cn1] *)
    
```

```

1944790: dnjjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} (-EO Sin(θ) Cos(θ1) + E2 EO Cos(θ)) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep sum. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1]+[An1][Dn1] *)
1944791: cnljjeq(θ_, x_, ρ_) := 1/ρ (n + zerooffset) e^{kz} * kol[1] HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944792: (*enljjeq(θ_, x_, ρ_) := 1/ρ e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *) *)
1944793: enljjeq(θ_, x_, ρ_) := 1/ρ e^{kz} * HankelH2[n-1, kol[1] ρ] - (n + HankelH2[n, kol[1] ρ] / ρ);
1944794: (*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *) (*updated 11/12/2016*)
1944795: mnjjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} (-EO Cos(θ) - E2 EO Sin(θ)) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep sum. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1]+[An1][Dn1] *)
1944796: nnljjeq(θ_, x_, ρ_) := -E2 e^{kz} * HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ] / (2 kol[1] e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944797: qnljjeq(θ_, x_, ρ_) := 1/ρ e^{kz} (n + zerooffset) * kol[1] HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944798: yn1jjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} (EO Cos(θ) Cos(θ1) + E2 EO Sin(θ)) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep sum. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1]+[An1][Dn1] *)
1944799: vn1jjeq(θ_, x_, ρ_) := -E2 e^{kz} * (kol[1] HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ]) / (2 kol[1] e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944800: wn1jjeq(θ_, x_, ρ_) := (ρ e^{kz} / ρ) (n + zerooffset) * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944801: dnjjeq(θ_, x_, ρ_) := ∑_{n=0}^{∞} (-EO Sin(θ) - E2 EO Cos(θ) Cos(θ1)) e^{kz + Cos(θ)n} BesselJ[nl, k2 ρ Sin(θ1)] e^{nl z};
(*Keep sum. INCIDENT FIELD FROM R2^+=[Dn1]-[An1][Cn1]+[An1][Dn1] *)
    
```

```

1944802: xn1jjeq(θ_, x_, ρ_) := (ρ e^{kz} / ρ) e^{kz} (n + zerooffset) * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
1944803: yn1jjeq(θ_, x_, ρ_) := -E2 e^{kz} * (kol[1] HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ]) / (2 kol[1] e^{kz + Cos(θ)n});
(*H2^+=[Dn1]-[An1][Cn1]-[Cn1][Dn1] *)
    
```

Boundary 'b' Fields - Equations and Variables [REQUIRED FOR CODE OPERATION ONLY]

1944804: (*This section of code was implemented for a prior approach. The values and solutions of this section play no role in the final results, however, removing them without compensating for the code structure change would render the entirety of this code in operable. Therefore, this code section will remain intact and up to a future user to decide whether or not to remove this section and make the necessary code changes. It would help to have context in order to make the change, though not necessary. The associated dissertation paper would suffice [PLANE-WAVE SCATTERING OF A PERIODIC CORRUGATED CYLINDER, by Samuel Garcia, Florida Atlantic University, Boca Raton, FL, November 2016] *)

Equations [NOT USED]

```

1944805: Ehb[En1_] := Eho**En1; (*Update with correct array length later*)
1944806: Ehp1[En1_, Fn1_] := ((Eho**En1) + (Eho**Fn1)); (*Update with correct array length later*)
1944807: Ehb[Fn1_] := E2n1j**Fn1;
1944808: Ehp1[En1_, Fn1_] := ((E2n1j**En1) + (E2n1j**Fn1));
1944809: Ebrho[En1_, Fn1_] := ((E2n1j**En1) + (E2n1j**Fn1));
1944810: Ebrho[En1_, Fn1_] := ((E2n1j**En1) + (E2n1j**Fn1));
    
```

Variables [REQUIRED FOR CODE OPERATION ONLY]

```

1944811: E2n1jjeq(θ_, x_, ρ_) := e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
1944812: E3n1jjeq(θ_, x_, ρ_) := -E2 e^{kz} * HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ] / (2 kol[1] e^{kz + Cos(θ)n});
1944813: E4n1jjeq(θ_, x_, ρ_) := 1/ρ e^{kz} * kol[1] HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
    
```

```

1944814: E5n1jjeq(θ_, x_, ρ_) := -E2 e^{kz} * (kol[1] HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ]) / (2 kol[1] e^{kz + Cos(θ)n});
1944815: E6n1jjeq(θ_, x_, ρ_) := (ρ e^{kz} / ρ) e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
1944816: E7n1jjeq(θ_, x_, ρ_) := (ρ e^{kz} / ρ) e^{kz} * HankelH2[n, kol[1] ρ] / (kol[1]^2 e^{kz + Cos(θ)n});
1944817: E8n1jjeq(θ_, x_, ρ_) := -E2 e^{kz} * (kol[1] HankelH2[n-1, kol[1] ρ] - HankelH2[n+1, kol[1] ρ]) / (2 kol[1] e^{kz + Cos(θ)n});
    
```

Regular ("Smooth") Cylinder Equations

Smooth Cylinder Equations TM-Mode

```

1944818: an(θ_, x_, n1_) := -BesselJ[nl, k2 + ρ2 + Sin(θ1)] / HankelH2[nl, k2 + ρ2 + Sin(θ1)];
Ez
1944819: ErcylTMS(θ_, x_, ρ_) := ∑_{n=0}^{∞} an(θ, x, n1) * HankelH2[nl, k2 + ρ2 + Sin(θ1)] e^{nl z} / (kol[1]^2 e^{kz + Cos(θ)n});
1944820: ErcylTMI(θ_, x_, ρ_) := ∑_{n=0}^{∞} BesselJ[nl, k2 + ρ2 + Sin(θ1)] e^{nl z} / (kol[1]^2 e^{kz + Cos(θ)n});
1944821: ErcylTMSandI(θ1_, θ_, x_, ρ_) := ErcylTMS(θ, x, ρ) + ErcylTMI(θ1, x, ρ);
Erho
1944822: ErcyhoTMS(θ_, x_, ρ_) := E2 EO Cos(θ1) e^{kz + Cos(θ)n} * (∑_{n=0}^{∞} an(θ, x, n1) * (1/2 (HankelH2[-1 + n1, k2 + ρ2 + Sin(θ1)] - HankelH2[1 + n1, k2 + ρ2 + Sin(θ1)]) + e^{kz + Cos(θ)n}));
1944823: ErcyhoTMI(θ_, x_, ρ_) := E2 EO Cos(θ) e^{kz + Cos(θ)n} * (∑_{n=0}^{∞} BesselJ[nl, k2 + ρ2 + Sin(θ1)] e^{nl z} / (kol[1]^2 e^{kz + Cos(θ)n}));
    
```


Phi Value and Range

```

%PHI000: phi = da;
%PHI001: phidelta = (2*pi)/phisteps;
%PHI002: phirange = N[Range[{0.5*phidelta}, (2*pi) - (0.5*phidelta), phidelta] ];
    
```

Matching Points - z's and phi's

```

%PHI003: zsteps = jQty;
%PHI004: jsteps = jQty;

(* Matching point options *)
(* (A.) Changing z's with fixed phi *)
(* (B.) Changing phi's with fixed z *)
(* (C.) Changing z's with fixed half phi=0 and half phi=Pi/2 *)
(* (D.) Requires overdetermined matrix form.
more j's matching points than unknowns *)
(* Changing phi's with for multiple z
points based on matching point multiplier, mp *)
(* D. is not yet implemented *)

(*-----*)
(* Boundary 'b' z matching points *)
(* Boundary 'b' z matching points *)
(* Boundary 'b' z matching points *)
(* zlength=b/2; *)
(* zsteps=zlength/zsteps; *)
(* zb=N[Range[{a/2}+(0.5*zbstep), (b/2)-(a/2)-(0.5*zbstep), zbstep] ]; *)

zbstart = (a/2) + (b/zsteps);
zbstep = ((a/2) + b) - (b/zsteps);
zstep = (zbstep - zbstart) / (zsteps - 1);
zb = N[Range[zbstart, zbstep, zstep]];

(* updated matching points to negate prior matching points -
Fixed zpoint matching method for varying phi point matches *)
zb = ConstantArray[zpointb, jsteps];
(*-----*)

(* Boundary 'a' z matching points *)
(* Boundary 'a' z matching points *)
    
```

```

(* Boundary 'a' z matching points *)
(* zlength=a/2; *)
(* zsteps=zlength/zsteps; *)
(* za=N[Range[{0.5*zstep}, (a/2)-(0.5*zstep), zstep] ]; *)

zjstart = (-a/2) + ((a/zsteps));
zjstep = (a/2) - (a/zsteps);
zjstep = (zjstart - zjstart) / (zsteps - 1);
zja = N[Range[zjstart, zjstep, zjstep]];

(* updated matching points to negate prior matching points -
Fixed zpoint matching method for varying phi point matches *)
zja = ConstantArray[zpointa, jsteps];

(*-----*)
(* phi matching points, 50% phi=0 and 50% phi=Pi/2 *)
phi = ConstantArray[0, jsteps];
count = 1;
For[count = 1, count < zsteps, count++,
  If[count < 5 * zsteps,
    phi[[count]] = 0.;
    phi[[count]] = Pi/2;
  ];
];

(* updated matching points to negate prior matching points *)
(* phi=ConstantArray[phi, jsteps]; *)

(* updated matching points to negate prior matching points *)
(* matching points of 0 to 2Pi *)
phiStart = 0 - (.5 * 2 * Pi / jsteps);
phiStop = (2 * Pi) - (.5 * 2 * Pi / jsteps);
phiStep = (phiStop - phiStart) / (jsteps - 1);
phi = N[Range[phiStart, phiStop, phiStep]];

(* phi=ConstantArray[phi, jsteps]; *) (* for z matching points *)

(*-----*)
    
```

Numerical Computation of Coefficients and Fields

Setting Empty Matrices to Solve for Coefficients and Field Components

```

%PHI005: (*-----*)
(*-----*)
EMPTY MATRICES FOR ALL EQUATIONS
(*-----*)
(*-----*)

(* Empty Matrices for Eq1 set, Boundary 'b' *)
Cn1iprematrix = Array[Cn1b, {nQty, lQty}];
an1iprematrix = Array[an1jb, {nQty, lQty, jQty}];
an1jarray = ConstantArray[0, jQty];
mn1iprematrix = Array[mn1b, {jQty}];

(* Empty Matrices for Eq2 set, Boundary 'a' *)
Cn1aprematrix = Array[Cn1a, {nQty, lQty}];
an1aprematrix = Array[an1ja, {nQty, lQty, jQty}];
an1jarray = ConstantArray[0, jQty];
mn1aprematrix = Array[mn1a, {jQty}];
hm1iprematrix = Array[hm1, {nQty, lQty, jQty}];
hm1jarray = ConstantArray[0, jQty];

(* Empty Matrices for Eq3 set, Boundary 'b' *)
(* Cn1b already defined *)
Cn1biprematrix = Array[Cn1jb, {nQty, lQty, jQty}];
an1biprematrix = Array[an1jb, {nQty, lQty, jQty}];
an1barray = ConstantArray[0, jQty];
dn1biprematrix = Array[dn1jb, {jQty}];

(* Empty Matrices for Eq4 set, Boundary 'a' *)
(* Cn1a and Ann already defined *)
Cn1aiprematrix = Array[Cn1ja, {nQty, lQty, jQty}];
an1aiprematrix = Array[an1ja, {nQty, lQty, jQty}];
an1jarray = ConstantArray[0, jQty];
mn1aiprematrix = Array[mn1a, {jQty}];
hm1aprematrix = Array[hm1, {nQty, lQty, jQty}];
hm1jarray = ConstantArray[0, jQty];
lm1aiprematrix = Array[lm1a, {nQty, lQty, jQty}];
    
```

```

lm1jarray = ConstantArray[0, jQty];

(* Empty Matrices for Eq5 set, Boundary 'b' *)
fn1biprematrix = Array[fn1jb, {jQty}];
qn1biprematrix = Array[qn1jb, {nQty, lQty, jQty}];
qn1barray = ConstantArray[0, jQty];
fn1aprematrix = Array[fn1a, {nQty, lQty}];
dn1biprematrix = Array[dn1bj, {nQty, lQty, jQty}];
dn1jarray = ConstantArray[0, jQty];

(* Empty Matrices for Eq6 set, Boundary 'a' *)
fn1aiprematrix = Array[fn1ja, {jQty}];
qn1aiprematrix = Array[qn1ja, {nQty, lQty, jQty}];
qn1jarray = ConstantArray[0, jQty];
hm1aprematrix = Array[hm1, {nQty, lQty}];
lm1aiprematrix = Array[lm1a, {nQty, lQty, jQty}];
lm1jarray = ConstantArray[0, jQty];

(* Empty Matrices for Eq7 set, Boundary 'b' *)
mn1biprematrix = Array[mn1b, {jQty}];
nn1biprematrix = Array[nn1jb, {nQty, lQty, jQty}];
nn1barray = ConstantArray[0, jQty];
qn1biprematrix = Array[qn1jb, {nQty, lQty, jQty}];
qn1barray = ConstantArray[0, jQty];
En1biprematrix = Array[En1bj, {nQty, lQty}];
dn1biprematrix = Array[dn1bj, {nQty, lQty, jQty}];
dn1jarray = ConstantArray[0, jQty];
dn1aiprematrix = Array[dn1ja, {nQty, lQty, jQty}];
dn1jarray = ConstantArray[0, jQty];

(* Empty Matrices for Eq8 set, Boundary 'a' *)
mn1aiprematrix = Array[mn1ja, {jQty}];
nn1aiprematrix = Array[nn1ja, {nQty, lQty, jQty}];
nn1jarray = ConstantArray[0, jQty];
qn1aiprematrix = Array[qn1ja, {nQty, lQty, jQty}];
qn1jarray = ConstantArray[0, jQty];
om1aiprematrix = Array[om1a, {nQty, lQty, jQty}];
om1jarray = ConstantArray[0, jQty];
pm1aiprematrix = Array[pm1a, {nQty, lQty, jQty}];
pm1jarray = ConstantArray[0, jQty];
    
```

Numerically Solving for Field Components

```

%Boundary Conditions p+p2.
a/Zxxa/2+b (For Boundary 'b') and-a/Zxxa/2 (For Boundary 'a')
%Region I Equations, Incident Field Components, Boundary 'a'
bnjb[jcount] = bnjq[phi, xj[jcount]], p2];
fnjb[jcount] = fnjq[phi, xj[jcount]], p2];
dnjb[jcount] = dnjq[phi, xj[jcount]], p2];
mnjb[jcount] = mnjq[phi, xj[jcount]], p2];
%Region II Equations, Incident Field Components, Boundary 'a'
bnja[jcount] = bnjq[phi, xj[jcount]], p2];
fnja[jcount] = fnjq[phi, xj[jcount]], p2];
dnja[jcount] = dnjq[phi, xj[jcount]], p2];
mnja[jcount] = mnjq[phi, xj[jcount]], p2];
%Region I Equations, Scattered Field Components, Boundary 'b'
en1b[jcount, lcount, jcount] = en1jq[phi, xj[jcount]], p2];
gn1b[jcount, lcount, jcount] = gn1jq[phi, xj[jcount]], p2];
on1b[jcount, lcount, jcount] = on1jq[phi, xj[jcount]], p2];
en1j[jcount, lcount, jcount] = en1jq[phi, xj[jcount]], p2];
gn1j[jcount, lcount, jcount] = gn1jq[phi, xj[jcount]], p2];
on1j[jcount, lcount, jcount] = on1jq[phi, xj[jcount]], p2];
%Boundary 'b' Only
o2n1[jcount, lcount, jcount] =
o2n1jq[phi, xj[jcount]], p2]; (* boundary 'b')
o3n1[jcount, lcount, jcount] = o3n1jq[phi, xj[jcount]], p2];
    
```

```

(* boundary 'b')
o4n1[jcount, lcount, jcount] = o4n1jq[phi, xj[jcount]], p2];
(* boundary 'b')
%Region II Equations, Scattered Field Components, Boundary 'a'
en1a[jcount, lcount, jcount] = en1jq[phi, xj[jcount]], p2];
gn1a[jcount, lcount, jcount] = gn1jq[phi, xj[jcount]], p2];
on1a[jcount, lcount, jcount] = on1jq[phi, xj[jcount]], p2];
en1j[jcount, lcount, jcount] = en1jq[phi, xj[jcount]], p2];
gn1j[jcount, lcount, jcount] = gn1jq[phi, xj[jcount]], p2];
on1j[jcount, lcount, jcount] = on1jq[phi, xj[jcount]], p2];
%Region I Equations, Boundary 'a'
hnmj[jcount, lcount, jcount] =
hnmjq[phi, xj[jcount]], p2]; (* boundary 'a')
imnj[jcount, lcount, jcount] = imnjq[phi, xj[jcount]], p2]; (* boundary 'a')
kmnj[jcount, lcount, jcount] = kmnjq[phi, xj[jcount]], p2]; (* boundary 'a')
lmnj[jcount, lcount, jcount] = lmnjq[phi, xj[jcount]], p2]; (* boundary 'a')
omnj[jcount, lcount, jcount] = omnjq[phi, xj[jcount]], p2]; (* boundary 'a')
pmnj[jcount, lcount, jcount] = pmnjq[phi, xj[jcount]], p2]; (* boundary 'a')
    
```

```

%Region I Equations, Incident Field Components, Boundary 'a'
en1a[jcount] = Flatten[Part[en1jprematrix, All, All, jcount]];
gn1a[jcount] = Flatten[Part[gn1jprematrix, All, All, jcount]];
on1a[jcount] = Flatten[Part[on1jprematrix, All, All, jcount]];
en1j[jcount] = Flatten[Part[en1jprematrix, All, All, jcount]];
gn1j[jcount] = Flatten[Part[gn1jprematrix, All, All, jcount]];
on1j[jcount] = Flatten[Part[on1jprematrix, All, All, jcount]];
en1jarray[jcount] = Flatten[Part[en1jprematrix, All, All, jcount]];
gn1jarray[jcount] = Flatten[Part[gn1jprematrix, All, All, jcount]];
on1jarray[jcount] = Flatten[Part[on1jprematrix, All, All, jcount]];
en1jarrayarray[jcount] = Flatten[Part[en1jarrayprematrix, All, All, jcount]];
gn1jarrayarray[jcount] = Flatten[Part[gn1jarrayprematrix, All, All, jcount]];
on1jarrayarray[jcount] = Flatten[Part[on1jarrayprematrix, All, All, jcount]];
o2n1array[jcount] = Flatten[Part[o2n1jprematrix, All, All, jcount]];
o3n1array[jcount] = Flatten[Part[o3n1jprematrix, All, All, jcount]];
o4n1array[jcount] = Flatten[Part[o4n1jprematrix, All, All, jcount]];
hnmjarray[jcount] = Flatten[Part[hnmjprematrix, All, All, jcount]];
imnjarray[jcount] = Flatten[Part[imnjprematrix, All, All, jcount]];
kmnjarray[jcount] = Flatten[Part[kmnjprematrix, All, All, jcount]];
lmnjarray[jcount] = Flatten[Part[lmnjprematrix, All, All, jcount]];
omnjarray[jcount] = Flatten[Part[omnjprematrix, All, All, jcount]];
pmnjarray[jcount] = Flatten[Part[pmnjprematrix, All, All, jcount]];
    
```

Solve for Coefficients Cn1b, Dn1b, Fn1, and En1

```

%Region I Equations, Incident Field Components, Boundary 'a'
Cn1b = Flatten[LeastSquares[en1jarray, -bnjprematrix]];
Dn1b = Flatten[LeastSquares[gn1jarray, -dnjprematrix - cn1jarray.Cn1b]];
Fn1 = Flatten[LeastSquares[o2n1array, fnjprematrix - gn1jarray.Dn1b]];
En1 = Flatten[LeastSquares[o3n1array,
(mnjprematrix - n1jarray.Cn1b - q1jarray.Dn1b) - o4n1array.Fn1]];
    
```

Solve for Coefficients Cn1a, Dn1a, Ann, and Bnm - Loop Method

```

%Region I Equations, Incident Field Components, Boundary 'a'
AnnTemp = FullSimplify[Flatten[PseudoInverse[Annjarray,
bnjprematrix - (n1jarray.Flatten[Cn1aprematrix])]];
BnmTemp = FullSimplify[Flatten[PseudoInverse[Bnmjarray,
fnjprematrix - (q1jarray.Flatten[Dn1aprematrix])]];
    
```

```

%Region I Equations, Incident Field Components, Boundary 'a'
Cn1aTemp = FullSimplify[
Flatten[PseudoInverse[Cn1jarray, ((kmjarray.AnnTemp) + (lmjarray.BnmTemp) -
dnjprematrix - (n1jarray.Flatten[Dn1aprematrix])]];
%Region I Equations, Incident Field Components, Boundary 'a'
Cn1aTemp2 = Solve[Flatten[PseudoInverse[Reduce[Cn1aTemp == Flatten[Cn1aprematrix],
Flatten[Cn1aprematrix]]], Flatten[Cn1aprematrix]];
%Region I Equations, Incident Field Components, Boundary 'a'
AnnTemp2 = Flatten[FullSimplify[AnnTemp / Cn1aTemp2]];
%Region I Equations, Incident Field Components, Boundary 'a'
Cn1aTemp3 = Flatten[FullSimplify[Cn1aTemp / Cn1aTemp2]];
%Region I Equations, Incident Field Components, Boundary 'a'
Dn1aTemp = FullSimplify[Flatten[
PseudoInverse[Dn1jarray, ((omnjarray.AnnTemp2) + (pmnjarray.BnmTemp) -
mnjprematrix - (n1jarray.Cn1aTemp3)]];
%Region I Equations, Incident Field Components, Boundary 'a'
ncount = 1;
lcount = 1;
Dn1aTemp2 = ConstantArray[0, jqty];
Dn1aSol = ConstantArray[0, jqty];
For[ncount = 1, ncount <= jqty, ncount++,
For[lcount = 1, lcount <= lqty, lcount++,
index = (ncount - 1) * lqty + lcount;
If[index == 1,
(*TRUE*)
Dn1aTemp2[[index]] = Solve[Dn1aTemp[[index]] ==
Flatten[Dn1aprematrix[[index]], Flatten[Dn1aprematrix[[index]]];
Dn1aSol = Flatten[Dn1aTemp2[[index]]];
(*FALSE*)
Dn1aTemp = Dn1aTemp / Dn1aSol;
Dn1aTemp2[[index]] =
Solve[Dn1aTemp[[index]] == Flatten[Dn1aprematrix[[index]]] / Dn1aSol,
Flatten[Dn1aprematrix[[index]]];
Dn1aSol = Flatten[Append[Flatten[Dn1aSol], Dn1aTemp2[[index]]];
];
];
    
```



```

(*Incident + Scattered Solution*)
SolEr = N[Abs[Ertemp]];
dataEr = Transpose[{rhorange/lambda0, SolEr}];

SolEphi = N[Abs[Ephitemp]];
dataEphi = Transpose[{rhorange/lambda0, SolEphi}];

SolErho = N[Abs[Erhitemp]];
dataErho = Transpose[{rhorange/lambda0, SolErho}];

SolEAllSandI = N[Abs[Sqrt[(Erhitemp + Cos[e] - (Ephitemp + Sin[e])^2 +
(Erhitemp + Sin[e] - (Ephitemp + Cos[e])^2 + (Ertemp)^2)]];
dataEAllSandI = Transpose[{rhorange/lambda0, SolEAllSandI}];

(*Scattered Only Solutions*)
SolErS = N[Abs[ErtempS]];
dataErS = Transpose[{rhorange/lambda0, SolErS}];

SolEphiS = N[Abs[EphitempS]];
dataEphiS = Transpose[{rhorange/lambda0, SolEphiS}];

SolErhoS = N[Abs[ErhitempS]];
dataErhoS = Transpose[{rhorange/lambda0, SolErhoS}];

SolEAllS = N[Abs[Sqrt[(ErhitempS + Cos[e] - EphitempS + Sin[e])^2 +
(ErhitempS + Sin[e] - EphitempS + Cos[e])^2 + (ErtempS)^2]];
dataEAllS = Transpose[{rhorange/lambda0, SolEAllS}];
    
```

Solution for Plots - Regular "Smooth" Cylinder

```

(*Incident*)
d = da; (*scattered field d, possibly incident d as well*)
(*e1=d*)
d1 = d1value; (*Only if considered unique and distinct from scattered field*)
    
```

TM Mode Solutions

```

(*Incident + Scattered Solution*)
SolEregcyITMSandI = N[Abs[EregcyITMSandI]];
dataEregcyITMSandI = Transpose[{rhorange/lambda0, SolEregcyITMSandI}];

SolEhoregcyITMSandI = N[Abs[EhoregcyITMSandI]];
dataEhoregcyITMSandI = Transpose[{rhorange/lambda0, SolEhoregcyITMSandI}];

SolEphiregcyITMSandI = N[Abs[EphiregcyITMSandI]];
dataEphiregcyITMSandI = Transpose[{rhorange/lambda0, SolEphiregcyITMSandI}];

SolEAllTMSandI =
N[Abs[Sqrt[(EhoregcyITMSandI + Cos[e] - (EphiregcyITMSandI + Sin[e])^2 +
(EhoregcyITMSandI + Sin[e] - (EphiregcyITMSandI + Cos[e])^2 +
(EregcyITMSandI)^2)]];
dataEAllTMSandI = Transpose[{rhorange/lambda0, SolEAllTMSandI}];

(*Scattered Only Solutions*)
SolEregcyITMS = N[Abs[EregcyITMS]];
dataEregcyITMS = Transpose[{rhorange/lambda0, SolEregcyITMS}];

SolEhoregcyITMS = N[Abs[EhoregcyITMS]];
dataEhoregcyITMS = Transpose[{rhorange/lambda0, SolEhoregcyITMS}];

SolEphiregcyITMS = N[Abs[EphiregcyITMS]];
dataEphiregcyITMS = Transpose[{rhorange/lambda0, SolEphiregcyITMS}];

SolEAllTMS = N[Abs[Sqrt[(EhoregcyITMS + Cos[e] - EphiregcyITMS + Sin[e])^2 +
(EhoregcyITMS + Sin[e] - EphiregcyITMS + Cos[e])^2 + (EregcyITMS)^2]];
dataEAllTMS = Transpose[{rhorange/lambda0, SolEAllTMS}];
    
```

TE Mode Solutions

```

(*Incident + Scattered Solution*)
SolEregcyITESandI = N[Abs[EregcyITESandI]];
dataEregcyITESandI = Transpose[{rhorange/lambda0, SolEregcyITESandI}];

SolEhoregcyITESandI = N[Abs[EhoregcyITESandI]];
dataEhoregcyITESandI = Transpose[{rhorange/lambda0, SolEhoregcyITESandI}];

SolEphiregcyITESandI = N[Abs[EphiregcyITESandI]];
dataEphiregcyITESandI = Transpose[{rhorange/lambda0, SolEphiregcyITESandI}];

SolEAllTESandI =
N[Abs[Sqrt[(EhoregcyITESandI + Cos[e] - (EphiregcyITESandI + Sin[e])^2 +
(EhoregcyITESandI + Sin[e] - (EphiregcyITESandI + Cos[e])^2 +
(EregcyITESandI)^2)]];
dataEAllTESandI = Transpose[{rhorange/lambda0, SolEAllTESandI}];

(*Scattered Only Solutions*)
SolEregcyITES = N[Abs[EregcyITES]];
dataEregcyITES = Transpose[{rhorange/lambda0, SolEregcyITES}];

SolEhoregcyITES = N[Abs[EhoregcyITES]];
dataEhoregcyITES = Transpose[{rhorange/lambda0, SolEhoregcyITES}];

SolEphiregcyITES = N[Abs[EphiregcyITES]];
dataEphiregcyITES = Transpose[{rhorange/lambda0, SolEphiregcyITES}];

SolEAllTES = N[Abs[Sqrt[(EhoregcyITES + Cos[e] - EphiregcyITES + Sin[e])^2 +
(EhoregcyITES + Sin[e] - EphiregcyITES + Cos[e])^2 + (EregcyITES)^2]];
dataEAllTES = Transpose[{rhorange/lambda0, SolEAllTES}];
    
```

TM + TE Mode Solutions

```

(*Incident + Scattered Solution*)
SolEregcyITMplusTESandI = N[Abs[EregcyITMplusTESandI]];
dataEregcyITMplusTESandI = Transpose[{rhorange/lambda0, SolEregcyITMplusTESandI}];

SolEhoregcyITMplusTESandI = N[Abs[EhoregcyITMplusTESandI]];
dataEhoregcyITMplusTESandI = Transpose[{rhorange/lambda0, SolEhoregcyITMplusTESandI}];

SolEphiregcyITMplusTESandI = N[Abs[EphiregcyITMplusTESandI]];
dataEphiregcyITMplusTESandI = Transpose[{rhorange/lambda0, SolEphiregcyITMplusTESandI}];

SolEAllTMplusTESandI =
N[Abs[Sqrt[(EhoregcyITMplusTESandI + Cos[e] - (EphiregcyITMplusTESandI + Sin[e])^2 +
(EhoregcyITMplusTESandI + Sin[e] - (EphiregcyITMplusTESandI + Cos[e])^2 +
(EregcyITMplusTESandI)^2)]];
dataEAllTMplusTESandI = Transpose[{rhorange/lambda0, SolEAllTMplusTESandI}];

(*Scattered Only Solutions*)
SolEregcyITMplusTES = N[Abs[EregcyITMplusTES]];
dataEregcyITMplusTES = Transpose[{rhorange/lambda0, SolEregcyITMplusTES}];

SolEhoregcyITMplusTES = N[Abs[EhoregcyITMplusTES]];
dataEhoregcyITMplusTES = Transpose[{rhorange/lambda0, SolEhoregcyITMplusTES}];

SolEphiregcyITMplusTES = N[Abs[EphiregcyITMplusTES]];
dataEphiregcyITMplusTES = Transpose[{rhorange/lambda0, SolEphiregcyITMplusTES}];

SolEAllTMplusTES = N[Abs[Sqrt[(EhoregcyITMplusTES + Cos[e] -
(EphiregcyITMplusTES + EphiregcyITMplusTES + Sin[e])^2 +
(EhoregcyITMplusTES + EphiregcyITMplusTES + Sin[e] - (EphiregcyITMplusTES +
EphiregcyITMplusTES + Cos[e])^2 + (EregcyITMplusTES)^2)]];
dataEAllTMplusTES = Transpose[{rhorange/lambda0, SolEAllTMplusTES}];
    
```

Changing Rho XY Plots

Table of Parameters

```

%%10000 tableValues = {[N[80] "V/m", "-", "-", "-", "-"], [N[80] "A/m", "-", "-", "-", "-"],
    (lambda0 "m", "-", "-", "-", "-"), (f0 "Hz", "-", "-", "-", "-"),
    {a/lambda0 "A", "-", "-", "-", "-"}, {b/lambda0 "A", "-", "-", "-", "-"},
    {c1/lambda0 "A", "-", "-", "-", "-"}, {c2/lambda0 "A", "-", "-", "-", "-"},
    {"-", rhomin/lambda0 "A", rhomax/lambda0 "A", rhodelta/lambda0 "A",
    Length[rhomaxepi]}, [N[6] {180/deg}] "Deg", "-", "-", "-", "-"},
    {point / a "m" s4 sunit/lambda0 "A", "-", "-", "-", "-"},
    {"-", "-", "-", "-", "Qty"}, [N[6] {180/deg}] "Deg", "-", "-", "-", "-"},
    [N[6] {180/deg}] "Deg", "-", "-", "-", "-"},
    {"-", "min", "max", "l", "qty"}, {"-", "lmin", "lmax", "l", "qty"},
    {lmaxcheck, "-", "-", "-", "-"}, {boundarycheck, "-", "-", "-", "-"}];
tablecheading = {"R0", "R0", "R0", "frequency", "a", "b", "c1", "c2",
    "p range", "s (observed)", "s (observed)", "Matching Points", "s1",
    "s1", "s1", "s1", "max allowable m", "max allowable m", "Boundary"};
tablecheading = {"value", "min", "max", "delta", "Qty of Points"};

%%10001 ChangingRhoTable = TableForm[tableValues, TableHeadings={tablecheading, tablecheading}];
%%10002 ChangingRhoTable = Grid[ArrayFlatten[{{{{" "}}}], {tablecheading}];
    (List /@ tablecheading, ArrayFlatten[tableValues]);
ItemStyle -> {Bold, 20}, Frame -> All, Background -> {LightGray}, {LightGray}];

%%10003 Export[ToString[StringForm["", RhoTable]], ChangingRhoTable]
    
```

Corrugated Cylinder Plots

Plot Ez (Scattered)

```

%%10000 ErcorrS = ListLinePlot[dataEzS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEzS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot Ez (Inc + Scattered)

```

%%10001 ErcorrSandI = ListLinePlot[dataEz,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEzI]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "Ez Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot Erho (Scattered)

```

%%10002 ErhoCorrS = ListLinePlot[dataErhoS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolErhoS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Erho Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot Erho (Inc + Scattered)

```

%%10003 ErhoCorrSandI = ListLinePlot[dataErho,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolErhoI]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "Erho Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot Ephi (Scattered)

```

%%10004 EphiCorrS = ListLinePlot[dataEphiS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEphiS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Ephi Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot Ephi (Inc + Scattered)

```

%%10005 EphiCorrSandI = ListLinePlot[dataEphi,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEphiI]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "Ephi Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot EAll (Scattered)

```

%%10006 EAllCorrS = ListLinePlot[dataEAllS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEAllS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "EAll Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Plot EAll (Inc + Scattered)

```

%%10007 EAllCorrSandI = ListLinePlot[dataEAllSandI,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEAllSandI]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "EAll Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"p/A", "V/m"},
    GridLines -> {{{p2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM Plots

```

%%10008 GraphicsGrid[{{ErcorrS, ErcorrSandI}, {ErhoCorrS, ErhoCorrSandI},
    {EphiCorrS, EphiCorrSandI}, {EAllCorrS, EAllCorrSandI}],
    Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TM Plots

Ez (TM Scattered)

```

%%1010 EzRegCylTMS = ListLinePlot[dataEzregcylTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzregcylTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TM Inc + Scattered)

```

%%1010 EzRegCylTMSandI = ListLinePlot[dataEzregcylTMSandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzregcylTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM Scattered)

```

%%1010 ErhoRegCylTMS = ListLinePlot[dataErhoregcyTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoregcyTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM Inc + Scattered)

```

%%1010 ErhoRegCylTMSandI = ListLinePlot[dataErhoregcyTMSandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoregcyTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM Scattered)

```

%%1010 EphiRegCylTMS = ListLinePlot[dataEphiregcyTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiregcyTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM Inc + Scattered)

```

%%1010 EphiRegCylTMSandI = ListLinePlot[dataEphiregcyTMSandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiregcyTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM Scattered)

```

%%1010 EAllRegCylTMS = ListLinePlot[dataEAllTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM Inc + Scattered)

```

%%1010 EAllRegCylTMSandI = ListLinePlot[dataEAllTMSandI,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM Plots

```

GraphicsGrid[{{EzRegCylTMS, EzRegCylTMSandI}, {ErhoRegCylTMS, ErhoRegCylTMSandI},
  {EphiRegCylTMS, EphiRegCylTMSandI}, {EAllRegCylTMS, EAllRegCylTMSandI}},
  Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TE Plots

Ez (TE Scattered)

```

%%1010 EzRegCylTES = ListLinePlot[dataEzregcylTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzregcylTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TE Inc + Scattered)

```

%%1010 EzRegCylTESandI = ListLinePlot[dataEzregcylTESandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzregcylTESandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TE Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TE Scattered)

```

%%1010 ErhoRegCylTES = ListLinePlot[dataErhoregcyTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoregcyTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TE Inc + Scattered)

```

%%1010 ErhoRegCylTESandI = ListLinePlot[dataErhoregcyTESandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoregcyTESandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/A", "V/m"},
  GridLines -> {{{[ρ2/lambda0, {Thick, Gray, Dashed}]}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TE Scattered)

```

EphiRegCylTES = ListLinePlot[dataEphiRegCylTES,
PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TE Inc + Scattered)

```

EphiRegCylTESandI = ListLinePlot[dataEphiRegCylTESandI, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TE Scattered)

```

EAllRegCylTES = ListLinePlot[dataEAllTES,
PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TE Inc + Scattered)

```

EAllRegCylTESandI = ListLinePlot[dataEAllTESandI,
PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TE Plots

```

GraphicsGrid[{{EphiRegCylTES, EphiRegCylTESandI},
{EphiRegCylTES, EphiRegCylTESandI},
{EAllRegCylTES, EAllRegCylTESandI}}, Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TM + TE Plots

Ez (TM+TE Scattered)

```

EzRegCylTMplusTES = ListLinePlot[dataEzRegCylTMplusTES, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzRegCylTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TM+TE Inc + Scattered)

```

EzRegCylTMplusTESandI = ListLinePlot[dataEzRegCylTMplusTESandI, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEzRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM+TE Scattered)

```

ErhoRegCylTMplusTES = ListLinePlot[dataErhoRegCylTMplusTES, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM+TE Inc + Scattered)

```

ErhoRegCylTMplusTESandI = ListLinePlot[dataErhoRegCylTMplusTESandI, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM+TE Scattered)

```

EphiRegCylTMplusTES = ListLinePlot[dataEphiRegCylTMplusTES, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM+TE Inc + Scattered)

```

EphiRegCylTMplusTESandI = ListLinePlot[dataEphiRegCylTMplusTESandI, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM+TE Scattered)

```

EAllRegCylTMplusTES = ListLinePlot[dataEAllTMplusTES,
PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM+TE Inc + Scattered)

```

EAllRegCylTMplusTESandI = ListLinePlot[dataEAllTMplusTESandI, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
Background -> White, ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM+TE Plots

```

GraphicsGrid[{{EzRegCylTMplusTES, EzRegCylTMplusTESandI},
{ErhoRegCylTMplusTES, ErhoRegCylTMplusTESandI},
{EphiRegCylTMplusTES, EphiRegCylTMplusTESandI},
{EAllRegCylTMplusTES, EAllRegCylTMplusTESandI}},
Spacings -> {Scaled[0], Scaled[0]}];
    
```


Scattered Only Arrays (TM and TE)

```

%Region I
EregcyITMS = ConstantArray(0, Length[phirange]];
EhoregcyITMS = ConstantArray(0, Length[phirange]];
EphiregcyITMS = ConstantArray(0, Length[phirange]];
EregcyITES = ConstantArray(0, Length[phirange]];
EhoregcyITES = ConstantArray(0, Length[phirange]];
EphiregcyITES = ConstantArray(0, Length[phirange]];
    
```

Incident Only Arrays (TM and TE)

```

%Region I
EregcyITMI = ConstantArray(0, Length[phirange]];
EhoregcyITMI = ConstantArray(0, Length[phirange]];
EphiregcyITMI = ConstantArray(0, Length[phirange]];
EregcyITEI = ConstantArray(0, Length[phirange]];
EhoregcyITEI = ConstantArray(0, Length[phirange]];
EphiregcyITEI = ConstantArray(0, Length[phirange]];
    
```

Changing Phi Do Loop Calculation

Do Loop

```

%Region I
ncount = 1;
%Region II
lcount = 1;
jcount = 1;
rho = rho; (*Observation rho for use in polar plots*)

Do[
  (*phi = phi;*)
  phi = phi; (*Only if considered unique and distinct from scattered fields*)

  (*Region II temp variables, Scattered Field Component*)
  EIistemp = 0;
  EIiphitemp = 0;
  EIirhotemp = 0;

  HIistemp = 0;
    
```

```

HIiphitemp = 0;
HIirhotemp = 0;

(*Region II temp variables, Incident Field Component*)
HIistemp = 0;
EIiphitemp = 0;
EIirhotemp = 0;
HIirhotemp = 0;

(*Region II temp variables, Total Field*)
HIistemp = 0;
HIiphitemp = 0;
HIistemp = 0;
EIirhotemp = 0;
EIirhotemp = 0;

(*Region I temp variables*)
EIistemp = 0;
EIiphitemp = 0;
EIistemp = 0;
EIiphitemp = 0;
EIirhotemp = 0;
EIirhotemp = 0;

(*Smooth Cylinder*)
If[rho < rho2,
  (*THDR*)
  EregcyITMSandI[[count]] = 0;
  EregcyITMS[[count]] = 0;
  EregcyITMI[[count]] = 0;
  EhoregcyITMSandI[[count]] = 0;
  EhoregcyITMS[[count]] = 0;
  EhoregcyITMI[[count]] = 0;
  EphiregcyITMSandI[[count]] = 0;
  EphiregcyITMS[[count]] = 0;
  EphiregcyITMI[[count]] = 0;
  EregcyITESandI[[count]] = 0;
  EregcyITES[[count]] = 0;
  EregcyITEI[[count]] = 0;
  EhoregcyITESandI[[count]] = 0;
  EhoregcyITES[[count]] = 0;
  EphiregcyITESandI[[count]] = 0;
    
```

```

EphiregcyITES[[count]] = 0;
EphiregcyITEI[[count]] = 0;
(*FALSE*)
EregcyITMSandI[[count]] = EregcyITMSandI[phi, theta, x, rho];
EregcyITMS[[count]] = EregcyITMS[phi, x, rho];
EregcyITMI[[count]] = EregcyITMI[phi, x, rho];

EhoregcyITMSandI[[count]] = EhoregcyITMSandI[phi, theta, x, rho];
EhoregcyITMS[[count]] = EhoregcyITMS[phi, x, rho];
EhoregcyITMI[[count]] = EhoregcyITMI[phi, x, rho];

EphiregcyITMSandI[[count]] = EphiregcyITMSandI[phi, theta, x, rho];
EphiregcyITMS[[count]] = EphiregcyITMS[phi, x, rho];
EphiregcyITMI[[count]] = EphiregcyITMI[phi, x, rho];

EregcyITESandI[[count]] = EregcyITESandI[phi, theta, x, rho];
EregcyITES[[count]] = EregcyITES[phi, x, rho];
EregcyITEI[[count]] = EregcyITEI[phi, x, rho];

EhoregcyITESandI[[count]] = EhoregcyITESandI[phi, theta, x, rho];
EhoregcyITES[[count]] = EhoregcyITES[phi, x, rho];
EhoregcyITEI[[count]] = EhoregcyITEI[phi, x, rho];

EphiregcyITESandI[[count]] = EphiregcyITESandI[phi, theta, x, rho];
EphiregcyITES[[count]] = EphiregcyITES[phi, x, rho];
EphiregcyITEI[[count]] = EphiregcyITEI[phi, x, rho];

};

If[rho > rho1, (*Check to see if inside conductor or not*)
  If[-a/2 <= x <= a/2, (*Check to see if in boundary 'a' or boundary 'b'*)
    (*-----IF TRUE-----*)
    (* In boundary 'a' but still need to determine if in Region I or II*)
    boundarycheck = "boundary a";
    If[rho < rho2, (*Region I fields, boundary 'a'*)
      (*Region I fields, boundary 'a'*)
      For[ncount = 1, ncount <= nqty, ncount++,
        n = nrange[[ncount]];
        For[lcount = 1, lcount <= lqty, lcount++,
          l = lrange[[lcount]];
          m = mrange[[lcount]];
        ];
      ];
    ];
  ];
  (*Add Incident and Scattered Fields*)
  EIistemp = h0jeq[phi, x, rho] + EIistemp;
  EIiphitemp = d0jeq[phi, x, rho] + EIiphitemp;
  EIistemp = f0jeq[phi, x, rho] + EIistemp;
  EIiphitemp = m0jeq[phi, x, rho] + EIiphitemp;
  EIirhotemp = r0jeq[phi, x, rho] + EIirhotemp;
  HIirhotemp = g0jeq[phi, x, rho] + HIirhotemp;

  (*Incident Fields Only*)
    
```

```

index = ((ncount - 1) * (lqty) + lcount);
EIistemp = EIistemp + (h0jeq[phi, x, rho] + Ann[[index]]);
EIiphitemp = EIiphitemp + (m0jeq[phi, x, rho] + Ann[[index]]);
HIistemp = HIistemp + (r0jeq[phi, x, rho] + Ann[[index]]);
HIiphitemp = HIiphitemp + (g0jeq[phi, x, rho] + Ann[[index]]);
EIirhotemp = EIirhotemp + (r0jeq[phi, x, rho] + Ann[[index]] +
  sm0jeq[phi, x, rho] + Ann[[index]]);
HIirhotemp = HIirhotemp + (tm0jeq[phi, x, rho] + Ann[[index]] +
  um0jeq[phi, x, rho] + Ann[[index]]);
};
};
(*Region II fields, boundary 'a'*)
For[ncount = 1, ncount <= nqty, ncount++,
  n = nrange[[ncount]];
  For[lcount = 1, lcount <= lqty, lcount++,
    l = lrange[[lcount]];
    m = mrange[[lcount]];
    index = ((ncount - 1) * (lqty) + lcount);
    (*Scattered Field Portion First*)
    HIistemp = HIistemp + an1jeq[phi, x, rho] + Dn1a[[index]];
    EIiphitemp = EIiphitemp + (cn1jeq[phi, x, rho] + Dn1a[[index]]);
    HIistemp = HIistemp + gn1jeq[phi, x, rho] + Dn1a[[index]];
    HIiphitemp = HIiphitemp + (un1jeq[phi, x, rho] + Dn1a[[index]]);
    EIirhotemp = EIirhotemp + (vn1jeq[phi, x, rho] + Dn1a[[index]] +
      wn1jeq[phi, x, rho] + Dn1a[[index]]);
    HIirhotemp = HIirhotemp + (an1jeq[phi, x, rho] + Dn1a[[index]] +
      yn1jeq[phi, x, rho] + Dn1a[[index]]);
  ];
];
];
(*Add Incident and Scattered Fields*)
EIistemp = h0jeq[phi, x, rho] + EIistemp;
EIiphitemp = d0jeq[phi, x, rho] + EIiphitemp;
EIistemp = f0jeq[phi, x, rho] + EIistemp;
EIiphitemp = m0jeq[phi, x, rho] + EIiphitemp;
EIirhotemp = r0jeq[phi, x, rho] + EIirhotemp;
HIirhotemp = g0jeq[phi, x, rho] + HIirhotemp;

(*Incident Fields Only*)
    
```

```

Extemp[[count]] = bnjqeq[phi, x, rho];
Ephitemp[[count]] = dnjqeq[phi, x, rho];
Erhotemp[[count]] = ynjqeq[phi, x, rho];

(*Scattered Field Only*)
EIistemp = EIistemp;
EIiphitemp = EIiphitemp;
EIirhotemp = EIirhotemp;
];

(*-----IF FALSE-----*) (* In boundary '
b' but still need to determine if in Cylinder or Region II*)
boundarycheck = "boundary b";
If[a < rho, (*In Cylinder, boundary 'b'*)
  Ertemp[[count]] = Ertemp[[count]] + 0;
  Ephiitemp[[count]] = Ephiitemp[[count]] + 0;
  Erhotemp[[count]] = Erhotemp[[count]] + 0;

  Extemp[[count]] = Extemp[[count]] + 0;
  Ephitemp[[count]] = Ephitemp[[count]] + 0;
  Erhotemp[[count]] = Erhotemp[[count]] + 0;

  Hstemp[[count]] = Hstemp[[count]] + 0;
  Hphiitemp[[count]] = Hphiitemp[[count]] + 0;
  Hrhohitemp[[count]] = Hrhohitemp[[count]] + 0;
  (*Region II fields, boundary 'b'*)
  For[icount = 1, icount < lqty, icount++,
    n = nrange[[icount]];
    For[icount = 1, icount < lqty, icount++,
      l = lrange[[icount]];
      n = nrange[[icount]];
      index = [[icount - 1], {lqty} - icount];
      (*Scattered Field Portion First*)
      EIistemp = EIistemp + anljjeq[phi, x, rho] + Cn1b[[index]];
      EIiphitemp = EIiphitemp +
        (cn1jqeq[phi, x, rho] + Cn1b[[index]] + enljjeq[phi, x, rho] + Dn1b[[index]]);
      EIirhotemp = EIirhotemp + gn1jqeq[phi, x, rho] + Dn1b[[index]];
      EIiphitemp = EIiphitemp +
        (cn1jqeq[phi, x, rho] + Cn1b[[index]] + enljjeq[phi, x, rho] + Dn1b[[index]]);
      EIirhotemp = EIirhotemp + (vn1jqeq[phi, x, rho] + Cn1b[[index]] +
        vn1jqeq[phi, x, rho] + Dn1b[[index]]);
      EIirhotemp = EIirhotemp + (xn1jqeq[phi, x, rho] + Cn1b[[index]] +
        xn1jqeq[phi, x, rho] + Cn1b[[index]]);
    ];
  ];

```

Printed by Wolfram Mathematica Student Edition

```

yn1jqeq[phi, x, rho] + Dn1b[[index]]];
];
(*Add Incident and Scattered Fields*)
EIistemp = bnjqeq[phi, x, rho] + EIistemp;
EIiphitemp = dnjqeq[phi, x, rho] + EIiphitemp;
EIirhotemp = fnjqeq[phi, x, rho] + EIirhotemp;
EIiphitemp = mnjqeq[phi, x, rho] + EIiphitemp;
EIirhotemp = ynjqeq[phi, x, rho] + EIirhotemp;
EIirhotemp = gnjqeq[phi, x, rho] + EIirhotemp;

(*Incident Fields Only*)
Ertemp[[count]] = bnjqeq[phi, x, rho];
Ephiitemp[[count]] = dnjqeq[phi, x, rho];
Erhotemp[[count]] = ynjqeq[phi, x, rho];

(*Scattered Field Only*)
EIistemp = EIistemp;
EIiphitemp = EIiphitemp;
EIirhotemp = EIirhotemp;
];

(*END IF STATEMENT*).
Ertemp[[count]] = Ertemp[[count]] + 0;
Ephiitemp[[count]] = Ephiitemp[[count]] + 0;
Erhotemp[[count]] = Erhotemp[[count]] + 0;

Extemp[[count]] = Extemp[[count]] + 0;
Ephitemp[[count]] = Ephitemp[[count]] + 0;
Erhotemp[[count]] = Erhotemp[[count]] + 0;

Hstemp[[count]] = Hstemp[[count]] + 0;
Hphiitemp[[count]] = Hphiitemp[[count]] + 0;
Hrhohitemp[[count]] = Hrhohitemp[[count]] + 0;

(*All E-Fields zeros*)
];

Ertemp[[count]] = Ertemp[[count]];
Ephiitemp[[count]] = Ephiitemp[[count]];
Erhotemp[[count]] = Erhotemp[[count]];

```

Printed by Wolfram Mathematica Student Edition

```

Extemp[[count]] = Extemp[[count]] + EIistemp;
Ephitemp[[count]] = Ephitemp[[count]] + EIiphitemp;
Erhotemp[[count]] = Erhotemp[[count]] + EIirhotemp;

Hstemp[[count]] = Hstemp[[count]];
Hphiitemp[[count]] = Hphiitemp[[count]];
Hrhohitemp[[count]] = Hrhohitemp[[count]];

count = count + 1;
{phi, phirange[[1]], phirange[[Length[phirange]], phidelta];
(*Close of 'do loop'*)

Solution for Plots - Corrugated Cylinder

(*Incident + Scattered Solutions*)
SolEz = N[Abs[Ertemp]];
dataEz = Transpose[{phirange, SolEz}];

SolEphi = N[Abs[Ephiitemp]];
dataEphi = Transpose[{phirange, SolEphi}];

SolErho = N[Abs[Erhotemp]];
dataErho = Transpose[{phirange, SolErho}];

SolEAllSandI =
  N[Abs[Sqrt[(Erhotemp + Cos[phirange] - (Ephitemp + Sin[phirange])^2 +
    (Erhotemp + Sin[phirange] + (Ephitemp + Cos[phirange])^2 - (Ertemp)^2)]];
  dataEAllSandI = Transpose[{phirange, SolEAllSandI}];

(*Scattered Only Solutions*)
SolEzS = N[Abs[Extemp]];
dataEzS = Transpose[{phirange, SolEzS}];

SolEphiS = N[Abs[Ephitemp]];
dataEphiS = Transpose[{phirange, SolEphiS}];

SolErhoS = N[Abs[Erhotemp]];
dataErhoS = Transpose[{phirange, SolErhoS}];

SolEAllS = N[Abs[Sqrt[(Erhotemp + Cos[phirange] - Ephitemp + Sin[phirange])^2 +
  (Erhotemp + Sin[phirange] + Ephitemp + Cos[phirange])^2 - (Ertemp)^2]];
  dataEAllS = Transpose[{phirange, SolEAllS}];

```

Printed by Wolfram Mathematica Student Edition

```

(*RCS Solution*)
RCSsolEz = (4 * Pi * (rho^2) * ((Abs[Extemp]^2) / (Abs[Ertemp]^2)));
RCSdataEz = Transpose[{phirange, RCSsolEz}];

RCSsolErho = (4 * Pi * (rho^2) * ((Abs[Erhotemp]^2) / (Abs[Erhotemp]^2)));
RCSdataErho = Transpose[{phirange, RCSsolErho}];

RCSsolEphi = (4 * Pi * (rho^2) * ((Abs[Ephiitemp]^2) / (Abs[Ephiitemp]^2)));
RCSdataEphi = Transpose[{phirange, RCSsolEphi}];

RCSsolEAllS = Sqrt[(Erhotemp + Cos[phirange] - Ephitemp + Sin[phirange])^2 +
  (Erhotemp + Sin[phirange] + Ephitemp + Cos[phirange])^2 - (Ertemp)^2];
RCSsolEAllI = Sqrt[(Erhotemp + Cos[phirange] - Ephitemp + Sin[phirange])^2 +
  (Erhotemp + Sin[phirange] + Ephitemp + Cos[phirange])^2 - (Ertemp)^2];
RCSsolEAll = (4 * Pi * (rho^2) * ((Abs[RCSsolEAllS]^2) / (Abs[RCSsolEAllI]^2)));
RCSdataEAll = Transpose[{phirange, RCSsolEAll}];

(*RCS Solution - in dB*)
RCSdataEzdB = Transpose[{phirange, 10 * Log10[RCSsolEz]}];
RCSdataErhoDB = Transpose[{phirange, 10 * Log10[RCSsolErho]}];
RCSdataEphiDB = Transpose[{phirange, 10 * Log10[RCSsolEphi]}];
RCSdataEAllDB = Transpose[{phirange, 10 * Log10[RCSsolEAll]}];

Solution for Plots - Regular "Smooth" Cylinder

TM Mode Solutions

(*Incident + Scattered Solutions*)
SolEzregcyTMSandI = N[Abs[EzregcyTMSandI]];
dataEzregcyTMSandI = Transpose[{phirange, SolEzregcyTMSandI}];

SolEhoregcyTMSandI = N[Abs[EhoregcyTMSandI]];
dataEhoregcyTMSandI = Transpose[{phirange, SolEhoregcyTMSandI}];

SolEphiregcyTMSandI = N[Abs[EphiregcyTMSandI]];
dataEphiregcyTMSandI = Transpose[{phirange, SolEphiregcyTMSandI}];

SolEAllTMS =
  N[Abs[Sqrt[(EhoregcyTMS + Cos[phirange] - EphiregcyTMS + Sin[phirange])^2 +
    (EhoregcyTMS + Sin[phirange] + EphiregcyTMS + Cos[phirange])^2 -
    (EzregcyTMS)^2]];
  dataEAllTMS = Transpose[{phirange, SolEAllTMS}];

```

Printed by Wolfram Mathematica Student Edition


```

RCSolEregoylTmplusTEAll = (4 * Pi * [sigma^2] *
  ((Abs[RCSolEregoylTmplusTEAllS]^2) / (Abs[RCSolEregoylTmplusTEAll]^2)));
RCSDataEregoylTmplusTEAll = Transpose[{phiRange, RCSolEregoylTmplusTEAll}];

(*RCS Solution - in dB*)
RCSDataEregoylTmplusTEdB =
  Transpose[{phiRange, 10 * Log10[RCSolEregoylTmplusTE]}];
RCSDataEhoregoylTmplusTEdB =
  Transpose[{phiRange, 10 * Log10[RCSolEhoregoylTmplusTE]}];
RCSDataEphiregoylTmplusTEdB =
  Transpose[{phiRange, 10 * Log10[RCSolEphiregoylTmplusTE]}];
RCSDataEregoylTmplusTEAlldB =
  Transpose[{phiRange, 10 * Log10[RCSolEregoylTmplusTEAll]}];

```

Export Data [Changing Rho Data]

```

data2 = {a, b, a2, p1, EstempS, EstempI, ErhotempS, ErhotempI, EphitempS, EphitempI,
  EaregoylTES, EaregoylTMS, EaregoylTEI, EaregoylTMI, EaregoylTES, EaregoylTMS,
  EaregoylTEI, EaregoylTMI, EphiregoylTES, EphiregoylTMS, EphiregoylTEI,
  EphiregoylTMI, rhoRange, rho, Lambda0, phi, d, ED, ED, ED, rhoMin, rhoMax,
  rhoDelta, spoint, jqty, ei, min, emax, rqty, lmin, lmax, lqty, mmin, emax, lqty,
  mmaxcheck, lmaxcheck, boundarycheck, Estemp, Ephitemp, Erhotemp, sa, ovalvalue};

Export[ToString[StringForm["", mx, rhoFileName]], data2]

```

Changing Phi Polar Plots

Table of Parameters

```

tableValues = {{N[RD] "m", "-", "-", "-", "-", "-"},
  {N[RD] "m", "-", "-", "-", "-", "-"}, {FO "m", "-", "-", "-", "-", "-"},
  {Lambda0 "m", "-", "-", "-", "-", "-"}, {a / Lambda0 "lambda", "-", "-", "-", "-", "-"},
  {b / Lambda0 "lambda", "-", "-", "-", "-", "-"}, {sigma / Lambda0 "lambda", "-", "-", "-", "-", "-"},
  {a2 / Lambda0 "lambda", "-", "-", "-", "-", "-"}, {"-", N[phiRange[1]] * (180 / Pi)] "Deg",
  N[phiRange[Length[phiRange]]] * (180 / Pi)] "Deg",
  N[phiDelta * (180 / Pi)] "Deg", Length[phiRange]}, {rho / Lambda0 "lambda", "-",
  "-", "-", "-"}, {spoint / a "a" & spoint / Lambda0 "lambda", "-", "-", "-", "-"},
  {"-", "-", "-", "-", "jqty", N[ei * (180 / Pi)] "Deg", "-", "-", "-", "-"},
  {N[ei * (180 / Pi)] "Deg", "-", "-", "-", "-", "-"},
  {"-", mmin, emax, "l", rqty}, {"-", lmin, lmax, "l", lqty},
  {"-", mmin, emax, "l", lqty}, {mmaxcheck, "-", "-", "-", "-"},
  {lmaxcheck, "-", "-", "-", "-"}, {boundarycheck, "-", "-", "-", "-"}];
tableRowHeading = {"EO", "HO", "lambda", "Frequency", "a", "b", "a2", "rho2",
  "d range", "d (observed)", "sa (observed)", "Matching Points", "ei",
  "d1", "n", "l", "m", "max allowable m", "max allowable l", "Boundary"};
tableColHeading = {"value", "min", "max", "delta", "Qty of Points"};

ChangingPhiTable = Grid[ArrayFlatten[{{{{" "}}}, {tableColHeading}],
  {List[tableRowHeading, ArrayFlatten[tableValues]}],
  ItemStyle -> {Bold, 20}, Frame -> All, Background -> {LightGray, {LightGray}}];

Export[ToString[StringForm["", ".jpg", PhiTableName]], ChangingPhiTable]

```

Corrugated Cylinder Plots

Plot Ez (Scattered)

```

EzCorrS = ListPolarPlot[dataEzS, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Corrugated Cylinder (Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzS]}];

```

Plot Ez (Inc + Scattered)

```

EzCorrSandI = ListPolarPlot[dataEz, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Corrugated Cylinder (Incident + Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzI]}];

```

Plot Erho (Scattered)

```

ErhoCorrS = ListPolarPlot[dataErhoS, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Corrugated Cylinder (Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoS]}];

```

Plot Erho (Inc + Scattered)

```

ErhoCorrSandI = ListPolarPlot[dataErho, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Corrugated Cylinder (Incident + Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoI]}];

```

Plot Ephi (Scattered)

```

EphiCorrS = ListPolarPlot[dataEphiS, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Corrugated Cylinder (Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphiS]}];

```

Plot Ephi (Inc + Scattered)

```

EphiCorrSandI = ListPolarPlot[dataEphi, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Corrugated Cylinder (Incident + Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphiI]}];

```

Plot EAll (Scattered)

```

EAllCorrS = ListPolarPlot[dataEAllS, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Corrugated Cylinder (Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllS]}];

```

Plot EAll (Inc + Scattered)

```

EAllCorrSandI =
  ListPolarPlot[dataEAllSandI, Joined -> True, PolarGridLines -> Automatic,
  PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Corrugated Cylinder (Incident + Scattered Field)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllSandI]}];

```

Summary Corrugated Cylinder Plots

```

GraphicsGrid[
  {{EzCorrS, EzCorrSandI}, {ErhoCorrS, ErhoCorrSandI}}, {EphiCorrS, EphiCorrSandI},
  {EAllCorrS, EAllCorrSandI}], Spacings -> {Scaled[0], Scaled[0]}];

```



```
RCSzCorr = ListPolarPlot[RCSdataz, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez, Corrugated Cylinder (RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRz]};
```

Plot Erho

```
RCSzErhoCorr = ListPolarPlot[RCSdatazErho, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Erho, Corrugated Cylinder (RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErho]};
```

Plot Ephi

```
RCSzEphiCorr = ListPolarPlot[RCSdatazEphi, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ephi, Corrugated Cylinder (RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphi]};
```

Plot EAll

```
RCSzAllCorr = ListPolarPlot[RCSdatazAll, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Etotal, Corrugated Cylinder (RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolAll]};
```

Summary Corrugated Cylinder Plots

```
GraphicsGrid[{{RCSzCorr}, {RCSzErhoCorr}, {RCSzEphiCorr}, {RCSzAllCorr}},
  Spacings -> {Scaled[0], Scaled[0]}];
```

Smooth Cylinder Plots - TM Plots

Ez (TM RCS)

```
RCSzRegCylTM = ListPolarPlot[RCSdatazRegCylTM, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez, Smooth Cylinder (TM RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRegCylTM]};
```

Erho (TM RCS)

```
%%RCSzErhoRegCylTM = ListPolarPlot[RCSdatazErhoRegCylTM, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Erho, Smooth Cylinder (TM RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErhoRegCylTM]};
```

Ephi (TM RCS)

```
%%RCSzEphiRegCylTM = ListPolarPlot[RCSdatazEphiRegCylTM, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ephi, Smooth Cylinder (TM RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphiRegCylTM]};
```

EAll (TM RCS)

```
%%RCSzAllRegCylTM = ListPolarPlot[RCSdatazRegCylTMAll, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Etotal, Smooth Cylinder (TM RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRegCylTMAll]};
```

Summary TM Plots

```
%%RCSzRegCylTM = GraphicsGrid[{{RCSzRegCylTM}, {RCSzErhoRegCylTM}, {RCSzEphiRegCylTM},
  {RCSzAllRegCylTM}}, Spacings -> {Scaled[0], Scaled[0]}];
```

Smooth Cylinder Plots - TE Plots

Ez (TE RCS) - DOES NOT EXIST

Erho (TE RCS)

```
%%RCSzErhoRegCylTE = ListPolarPlot[RCSdatazErhoRegCylTE, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Erho, Smooth Cylinder (TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErhoRegCylTE]};
```

Ephi (TE RCS)

```
%%RCSzEphiRegCylTE = ListPolarPlot[RCSdatazEphiRegCylTE, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ephi, Smooth Cylinder (TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphiRegCylTE]};
```

EAll (TE RCS)

```
%%RCSzAllRegCylTE = ListPolarPlot[RCSdatazRegCylTEAll, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Etotal, Smooth Cylinder (TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRegCylTEAll]};
```

Summary TE Plots

```
%%RCSzRegCylTE = GraphicsGrid[{{RCSzErhoRegCylTE}, {RCSzEphiRegCylTE}, {RCSzAllRegCylTE}},
  Spacings -> {Scaled[0], Scaled[0]}];
```

Smooth Cylinder Plots - TM + TE Plots

Ez (TM + TE RCS)

```
%%RCSzRegCylTMplusTE = ListPolarPlot[RCSdatazRegCylTMplusTE, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez, Smooth Cylinder (TM + TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRegCylTMplusTE]};
```

Erho (TM + TE RCS)

```
%%RCSzErhoRegCylTMplusTE = ListPolarPlot[RCSdatazErhoRegCylTMplusTE, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Erho, Smooth Cylinder (TM + TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErhoRegCylTMplusTE]};
```

Ephi (TM + TE RCS)

```
%%RCSzEphiRegCylTMplusTE = ListPolarPlot[RCSdatazEphiRegCylTMplusTE, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ephi, Smooth Cylinder (TM + TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphiRegCylTMplusTE]};
```

EAll (TM + TE RCS)

```
%%RCSzAllRegCylTMplusTE = ListPolarPlot[RCSdatazRegCylTMplusTEAll, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Etotal, Smooth Cylinder (TM + TE RCS m²)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolRegCylTMplusTEAll]};
```

Summary TM + TE Plots

```
GraphicsGrid[
  {{RCSERegCylTMplusTE}, {RCSERhoRegCylTMplusTE}, {RCSERphiRegCylTMplusTE},
  {RCSERAllRegCylTMplusTE}}, Spacings -> {Scaled[0], Scaled[0]};

```

Compare (Regular vs Corrugated) Plots

TM, TE, and TM+TE Compare

```
PHI:RCSERhoPolarPlots =
GraphicsGrid[{{ListPolarPlot[RCSdataEregCylTM, RCSdataE], Joined - True,
  PolarGridLines - Automatic, PolarTicks - {"Degrees", Automatic},
  PlotStyle -> {Blue, {Red, Dashed}},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
  "E, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[RCSERhoRegCylTM, RCSERhoE]}],
  "E TE Does Not Exist"
},
ListPolarPlot[RCSdataEregCylTMplusTE, RCSdataE],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTE, RCSERhoE]}],
{ListPolarPlot[RCSdataEregCylTM, RCSdataErho],
  Joined - True, PolarGridLines - Automatic,
  PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
  "E, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[RCSERhoRegCylTM, RCSERhoE]}],
  ListPolarPlot[RCSdataEregCylTMplusTE, RCSdataErho],
  Joined - True, PolarGridLines - Automatic,
  PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
  "E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTE, RCSERhoE]}],
  ListPolarPlot[RCSdataEregCylTMAll, RCSdataEAll],
  Joined - True, PolarGridLines - Automatic,
  PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
  "E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
  PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTEAll, RCSERhoEAll]}],
  }
}
Export[ToString[StringForm["", PHI:RCSERhoPolarPlots]], PHI:RCSERhoPolarPlots];

```

```
"E, TE RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes - True, PolarAxesOrigin - {0, Max[RCSERhoRegCylTM, RCSERhoE]}],
},
ListPolarPlot[RCSdataEregCylTMplusTE, RCSdataErho],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTE, RCSERhoE]}],
},
ListPolarPlot[RCSdataEregCylTM, RCSdataEphi],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"E, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes - True, PolarAxesOrigin - {0, Max[RCSERhoRegCylTM, RCSERhoPhi]}],
},
ListPolarPlot[RCSdataEregCylTMplusTE, RCSdataEphi],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTE, RCSERhoPhi]}],
},
{ListPolarPlot[RCSdataEregCylTMAll, RCSdataEAll],
  Joined - True, PolarGridLines - Automatic,
  PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
  BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
  "E, TM+TE RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
  PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTEAll, RCSERhoEAll]}],
  }
}
Export[ToString[StringForm["", PHI:RCSERhoPolarPlots]], PHI:RCSERhoPolarPlots];

```

```
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "E, TM RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMAll, RCSERhoEAll]}],
},
ListPolarPlot[RCSdataEregCylTMAll, RCSdataEAll],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "E, TM RCS (m²) Smooth Cylinder (Blue) vs
  Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMAll, RCSERhoEAll]}],
},
ListPolarPlot[RCSdataEregCylTMplusTEAll, RCSdataEAll],
Joined - True, PolarGridLines - Automatic,
PolarTicks - {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "E, TM+TE RCS (m²) Smooth Cylinder (Blue)
  vs Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes - True,
PolarAxesOrigin - {0, Max[RCSERhoRegCylTMplusTEAll, RCSERhoEAll]}],
}
}
Export[ToString[StringForm["", PHI:RCSERhoPolarPlots]], PHI:RCSERhoPolarPlots];

```

Changing Phi RCS dB Polar Plots

Corrugated Cylinder Plots

Plot Ez

```
PHI:RCSERhoCorrDB = ListPolarPlot[RCSdataEzDB, Joined - True,
  PolarGridLines - Automatic, PolarTicks - {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "E, Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[Abs[10 * Log10[RCSERhoE]]]};

```

Plot Erho

```
RCSERhoCorrDB = ListPolarPlot[RCSdataErhoDB, Joined - True,
  PolarGridLines - Automatic, PolarTicks - {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "E, Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[Abs[10 * Log10[RCSERhoE]]]};

```

Plot Ephi

```
RCSERphiCorrDB = ListPolarPlot[RCSdataEphiDB, Joined - True,
  PolarGridLines - Automatic, PolarTicks - {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "E, Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[Abs[10 * Log10[RCSERphiE]]]};

```

Plot EAll

```
RCSERAllCorrDB = ListPolarPlot[RCSdataEAllDB, Joined - True,
  PolarGridLines - Automatic, PolarTicks - {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "E, Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes - True, PolarAxesOrigin - {0, Max[Abs[10 * Log10[RCSERAllE]]]};

```

Summary Corrugated Cylinder Plots

```
PHI:RCSERhoCorrDB = {RCSERhoCorrDB}, {RCSERrhoCorrDB}, {RCSERAllCorrDB},
Spacings -> {Scaled[0], Scaled[0]};

```

Smooth Cylinder Plots - TM Plots

Ez (TM RCS)

```

%%100760 RCSEzRegCylTMdB = ListPolarPlot[RCSEzDataEzregCylTMdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEzSolEzregCylTM]]]}];
  
```

Erho (TM RCS)

```

%%100761 RCSErhoRegCylTMdB = ListPolarPlot[RCSErhoDataErhoRegCylTMdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TM RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSErhoSolErhoRegCylTM]]]}];
  
```

Ephi (TM RCS)

```

%%100762 RCSEphiRegCylTMdB = ListPolarPlot[RCSEphiDataEphiRegCylTMdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEphiSolEphiRegCylTM]]]}];
  
```

EAll (TM RCS)

```

%%100763 RCSEAllRegCylTMdB = ListPolarPlot[RCSEAllDataEregCylTMAlldB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Eall Smooth Cylinder (TM RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEAllSolEregCylTMAll]]]}];
  
```

Summary TM Plots

```

%%100764 GraphicsGrid[{{RCSEzRegCylTMdB}, {RCSErhoRegCylTMdB}, {RCSEphiRegCylTMdB}},
  {RCSEAllRegCylTMdB}], Spacings -> {Scaled[0], Scaled[0]};
  
```

Printed by Wolfram Mathematica Student Edition

Smooth Cylinder Plots - TE Plots

Ez (TE RCS) - DOES NOT EXIST

Erho (TE RCS)

```

%%100765 RCSErhoRegCylTEdB = ListPolarPlot[RCSErhoDataErhoRegCylTEdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSErhoSolErhoRegCylTE]]]}];
  
```

Ephi (TE RCS)

```

%%100766 RCSEphiRegCylTEdB = ListPolarPlot[RCSEphiDataEphiRegCylTEdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEphiSolEphiRegCylTE]]]}];
  
```

EAll (TE RCS)

```

%%100767 RCSEAllRegCylTEdB = ListPolarPlot[RCSEAllDataEregCylTEAlldB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Eall Smooth Cylinder (TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEAllSolEregCylTEAll]]]}];
  
```

Summary TE Plots

```

%%100768 GraphicsGrid[{{RCSErhoRegCylTEdB}, {RCSEphiRegCylTEdB}, {RCSEAllRegCylTEdB}},
  Spacings -> {Scaled[0], Scaled[0]};
  
```

Printed by Wolfram Mathematica Student Edition

Smooth Cylinder Plots - TM + TE Plots

Ez (TM + TE RCS)

```

%%100769 RCSEzRegCylTMplusTEdB = ListPolarPlot[RCSEzDataEzregCylTMplusTEdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEzSolEzregCylTMplusTE]]]}];
  
```

Erho (TM + TE RCS)

```

%%100770 RCSErhoRegCylTMplusTEdB = ListPolarPlot[RCSErhoDataErhoRegCylTMplusTEdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TM + TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSErhoSolErhoRegCylTMplusTE]]]}];
  
```

Ephi (TM + TE RCS)

```

%%100771 RCSEphiRegCylTMplusTEdB = ListPolarPlot[RCSEphiDataEphiRegCylTMplusTEdB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM + TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEphiSolEphiRegCylTMplusTE]]]}];
  
```

EAll (TM + TE RCS)

```

%%100772 RCSEAllRegCylTMplusTEdB = ListPolarPlot[RCSEAllDataEregCylTMplusTEAlldB, Joined -> True,
  PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Eall Smooth Cylinder (TM + TE RCS dBm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSEAllSolEregCylTMplusTEAll]]]}];
  
```

Printed by Wolfram Mathematica Student Edition

Summary TM + TE Plots

```

%%100773 GraphicsGrid[
  {{RCSEzRegCylTMplusTEdB}, {RCSErhoRegCylTMplusTEdB}, {RCSEphiRegCylTMplusTEdB},
  {RCSEAllRegCylTMplusTEdB}], Spacings -> {Scaled[0], Scaled[0]};
  
```

Compare (Regular vs Corrugated) Plots

TM, TE, and TM+TE Compare

```

%%100774 PhiRCSdBPlot =
  GraphicsGrid[
    {ListPolarPlot[{{RCSEzDataEzregCylTMdB, RCSEzDataErho},
      Joined -> True,
      PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
      PlotStyle -> {Blue, Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
      PlotMarkers -> None, PlotLabel -> "Ez TM RCS (dBm) Smooth
      Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
      ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
      PolarAxes -> True, PolarAxesOrigin ->
      {0, Max[Abs[10 * Log10[RCSEzSolEzregCylTM]]}, Abs[10 * Log10[RCSEzSolEz]}]}],
      "Ez, TE Does Not Exist"
    },
    {ListPolarPlot[{{RCSEphiDataEphiRegCylTMplusTEdB, RCSEzDataErho},
      Joined -> True,
      PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
      PlotStyle -> {Blue, Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
      PlotMarkers -> None, PlotLabel -> "Ez TM+TE RCS (dBm) Smooth
      Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
      ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
      PolarAxes -> True, PolarAxesOrigin ->
      {0, Max[Abs[10 * Log10[RCSEphiSolEphiRegCylTMplusTE]]}, Abs[10 * Log10[RCSEzSolEz]}]}],
      "Ez, TE Does Not Exist"
    },
    {ListPolarPlot[{{RCSErhoDataErhoRegCylTMplusTEdB, RCSEzDataErho},
      Joined -> True,
      PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
      PlotStyle -> {Blue, Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
      PlotMarkers -> None, PlotLabel -> "Erho TM RCS (dBm) Smooth
      Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
      ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
      PolarAxes -> True, PolarAxesOrigin ->
      {0, Max[Abs[10 * Log10[RCSErhoSolErhoRegCylTMplusTE]]}, Abs[10 * Log10[RCSErhoSolErho]}]}],
      "Erho, TE Does Not Exist"
    },
    {ListPolarPlot[{{RCSEAllDataEregCylTMplusTEAlldB, RCSEzDataErho},
      Joined -> True,
      PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
      PlotStyle -> {Blue, Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
      PlotMarkers -> None, PlotLabel -> "Eall TM RCS (dBm) Smooth
      Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
      ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
      PolarAxes -> True, PolarAxesOrigin ->
      {0, Max[Abs[10 * Log10[RCSEAllSolEregCylTMplusTEAll]]}, Abs[10 * Log10[RCSEzSolEz]}]}],
      "Eall, TE Does Not Exist"
    }
  ]
  
```

Printed by Wolfram Mathematica Student Edition

```

PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez TE RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin ->
{0, Max[Abs[10*Log10[RCSsolEzHoregcy1TM]], Abs[10*Log10[RCSsolEzHo]]]}],
,
ListPolarPlot[{RCSdataEzHoregcy1TMplusTEdB, RCSdataEzHdB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez TE RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[
Abs[10*Log10[RCSsolEzHoregcy1TMplusTE]], Abs[10*Log10[RCSsolEzHo]]]}],
},
,
ListPolarPlot[{RCSdataEzHoregcy1TMDb, RCSdataEzHdB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez TM RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin ->
{0, Max[Abs[10*Log10[RCSsolEzHoregcy1TM]], Abs[10*Log10[RCSsolEzHphi]]]}],
,
ListPolarPlot[{RCSdataEzHoregcy1TEdB, RCSdataEzHdB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez TE RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin ->
{0, Max[Abs[10*Log10[RCSsolEzHoregcy1TE]], Abs[10*Log10[RCSsolEzHphi]]]}],
,
ListPolarPlot[{RCSdataEzHoregcy1TMplusTEdB, RCSdataEzHdB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez TM RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[
Abs[10*Log10[RCSsolEzHoregcy1TMplusTE]], Abs[10*Log10[RCSsolEzHphi]]]}],
}

```

```

},
{ListPolarPlot[{RCSdataEzRegcy1TMAlldB, RCSdataEzAlldB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal TM RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin ->
{0, Max[Abs[10*Log10[RCSsolEzRegcy1TMAlldB]], Abs[10*Log10[RCSsolEzAlldB]]]}],
,
ListPolarPlot[{RCSdataEzRegcy1TEAlldB, RCSdataEzAlldB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal TE RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin ->
{0, Max[Abs[10*Log10[RCSsolEzRegcy1TEAlldB]], Abs[10*Log10[RCSsolEzAlldB]]]}],
,
ListPolarPlot[{RCSdataEzRegcy1TMplusTEAlldB, RCSdataEzAlldB}, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal TM+TE RCS (dBsm) Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, -)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[
Abs[10*Log10[RCSsolEzRegcy1TMplusTEAlldB]], Abs[10*Log10[RCSsolEzAlldB]]]}],
}
}
Export[ToString[StringForm["", jpp], PhiRCSdB[PolarPlotsName]], PhiRCSdB[PolarPlots]

```

Changing Phi RCS dB XY Plots

Corrugated Cylinder Plots

Plot Ez

```

RCSERCorrDBey = ListLinePlot[RCSdataERdB,
PlotRange -> {{0, 2 Pi}, {Min[10*Log10[RCSsolERz]], Max[10*Log10[RCSsolERz]]}},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Plot Erho
RCSERCorrDBey = ListLinePlot[RCSdataERhodb, PlotRange ->
{{0, 2 Pi}, {Min[10*Log10[RCSsolERho]], Max[10*Log10[RCSsolERho]]}},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Plot Ephi
RCSERCorrDBey = ListLinePlot[RCSdataERhodb, PlotRange ->
{{0, 2 Pi}, {Min[10*Log10[RCSsolERphi]], Max[10*Log10[RCSsolERphi]]}},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Plot Eall
RCSERCorrDBey = ListLinePlot[RCSdataERalldB, PlotRange ->
{{0, 2 Pi}, {Min[10*Log10[RCSsolERall]], Max[10*Log10[RCSsolERall]]}},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal Corrugated Cylinder (RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Summary Corrugated Cylinder Plots
GraphicsGrid[{{RCSERCorrDBey}, {RCSERCorrDBey}, {RCSERCorrDBey},
{RCSERallCorrDBey}}, Spacings -> {Scaled[0], Scaled[0]}];

```

Smooth Cylinder Plots - TM Plots

Ez (TM RCS)

```

RCSERRegcy1TMDbey = ListLinePlot[RCSdataEzRegcy1TMDb, PlotRange -> {{0, 2 Pi},
{Min[10*Log10[RCSsolEzRegcy1TM]], Max[10*Log10[RCSsolEzRegcy1TM]]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Erho (TM RCS)
RCSERRegcy1TMDbey = ListLinePlot[RCSdataEzRegcy1TMDb, PlotRange -> {{0, 2 Pi},
{Min[10*Log10[RCSsolEzRegcy1TM]], Max[10*Log10[RCSsolEzRegcy1TM]]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Ephi (TM RCS)
RCSERRegcy1TMDbey = ListLinePlot[RCSdataEzRegcy1TMDb, PlotRange -> {{0, 2 Pi},
{Min[10*Log10[RCSsolEzRegcy1TM]], Max[10*Log10[RCSsolEzRegcy1TM]]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

Eall (TM RCS)
RCSERRegcy1TMDbey = ListLinePlot[RCSdataEzRegcy1TMAlldB, PlotRange -> {{0, 2 Pi},
{Min[10*Log10[RCSsolEzRegcy1TMAlldB]], Max[10*Log10[RCSsolEzRegcy1TMAlldB]]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal Smooth Cylinder (TM RCS dBsm)",
Frame -> True, FrameLabel -> {"φ", "RCS (dBsm)"},
GridLines -> {{{Pi}, {Thick, Gray, Dashed}}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];

```


Plane-wave Scattering of a Periodic Corrugated Cylinder - Boundary a+b

```

%101 ClearAll["Global.*"]
SetDirectory["C:\Users\Hansel\Google Drive\Disertation\FinalData"];
(*Output Directory*)

```

Import Data [Changing Rho Data]

Boundary 'a' Data

```

%102 dataa = Import["rho_outa.mx"];
%103 a = dataa[[1]];
%104 b = dataa[[2]];
%105 p2 = dataa[[3]];
%106 p1 = dataa[[4]];
%107 ExtempSa = dataa[[5]];
%108 EshotempSa = dataa[[6]];
%109 ErhotempSa = dataa[[7]];
%110 EphitempSa = dataa[[8]];
%111 EphitempSa = dataa[[9]];
%112 EphitempSa = dataa[[10]];
%113 EregoylTMSa = dataa[[11]];
%114 EregoylTMSa = dataa[[12]];
%115 EregoylTMSa = dataa[[13]];
%116 EregoylTMSa = dataa[[14]];
%117 ErhoregoylTMSa = dataa[[15]];
%118 ErhoregoylTMSa = dataa[[16]];
%119 ErhoregoylTMSa = dataa[[17]];

```

Printed by Wolfram Mathematica Student Edition

2 | PhD Research Garcia_Boundary_a_plus_b.nb

```

%101 ErhoregoylTMSa = dataa[[18]];
%102 EphiregoylTMSa = dataa[[19]];
%103 EphiregoylTMSa = dataa[[20]];
%104 EphiregoylTMSa = dataa[[21]];
%105 EphiregoylTMSa = dataa[[22]];
%106 rhorange = dataa[[23]]; (*rho range*)
%107 rho = dataa[[24]];
%108 lambda0 = dataa[[25]];
%109 ei = dataa[[26]];
%110 theta = dataa[[27]];
%111 R0 = dataa[[28]];
%112 R0 = dataa[[29]];
%113 R0 = dataa[[30]];
%114 rhomin = dataa[[31]];
%115 rhomax = dataa[[32]];
%116 rhodelta = dataa[[33]];
%117 spoint = dataa[[34]];
%118 jqty = dataa[[35]];
%119 ei = dataa[[36]];
%120 rmin = dataa[[37]];
%121 rmax = dataa[[38]];
%122 regy = dataa[[39]];
%123 lmin = dataa[[40]];
%124 lmax = dataa[[41]];
%125 lqty = dataa[[42]];
%126 rmin = dataa[[43]];
%127 rmax = dataa[[44]];
%128 lqty = dataa[[45]];
%129 lmaxcheck = dataa[[46]];
%130 lmaxcheck = dataa[[47]];
%131 boundarycheck = dataa[[48]];
%132 (*Extemp=dataa[[49]];
%133 Ephitemp=dataa[[50]];
%134 Eshotemp=dataa[[51]]; *)
%135 theta = dataa[[52]];
%136 eiValue = dataa[[53]];

```

Printed by Wolfram Mathematica Student Edition

PHD Research Garcia_Boundary_a_plus_b.nb | 3

Boundary 'b' Data

```

%102 datab = Import["rho_outb.mx"];
%103 a = datab[[1]];
%104 b = datab[[2]];
%105 p2 = datab[[3]];
%106 p1 = datab[[4]];
%107 ExtempSb = datab[[5]];
%108 EshotempSb = datab[[6]];
%109 ErhotempSb = datab[[7]];
%110 EphitempSb = datab[[8]];
%111 EphitempSb = datab[[9]];
%112 EregoylTMSb = datab[[11]];
%113 EregoylTMSb = datab[[12]];
%114 EregoylTMSb = datab[[13]];
%115 EregoylTMSb = datab[[14]];
%116 ErhoregoylTMSb = datab[[15]];
%117 ErhoregoylTMSb = datab[[16]];
%118 ErhoregoylTMSb = datab[[17]];
%119 ErhoregoylTMSb = datab[[18]];
%120 EphiregoylTMSb = datab[[19]];
%121 EphiregoylTMSb = datab[[20]];
%122 EphiregoylTMSb = datab[[21]];
%123 EregoylTMSb = datab[[22]];
%124 (*Extemp=datab[[49]];
%125 Ephitemp=datab[[50]];
%126 Eshotemp=datab[[51]]; *)

```

Printed by Wolfram Mathematica Student Edition

4 | PhD Research Garcia_Boundary_a_plus_b.nb

Equations [Changing Rho Data]

```

(*Combining of Boundar 'a' and Boundar 'b' fields*)
Extemp = ExtempSa + ExtempSb;
EtempI = ExtempIa;
EshotempI = EshotempSa + EshotempSb;
ErhotempI = ErhotempSa;
EphitempI = EphitempSa + EphitempSb;
EphitempI = EphitempIa;
EregoylTMS = EregoylTMSa + EregoylTMSb;
EregoylTMS = EregoylTMSa + EregoylTMSb;
EregoylTEI = EregoylTEIa;
EregoylTMI = EregoylTMIa;
ErhoregoylTMS = ErhoregoylTMSa + ErhoregoylTMSb;
ErhoregoylTMS = ErhoregoylTMSa + ErhoregoylTMSb;
ErhoregoylTEI = ErhoregoylTEIa;
ErhoregoylTMI = ErhoregoylTMIa;
EphiregoylTMS = EphiregoylTMSa + EphiregoylTMSb;
EphiregoylTMS = EphiregoylTMSa + EphiregoylTMSb;
EphiregoylTEI = EphiregoylTEIa;
EphiregoylTMI = EphiregoylTMIa;

```

```

(*Changing rho XY plot specific equations*)
EregoylTMSandI = EregoylTMS + EregoylTMI;
ErhoregoylTMSandI = ErhoregoylTMS + ErhoregoylTMI;
EphiregoylTMSandI = EphiregoylTMS + EphiregoylTMI;
EregoylTMSandI = EregoylTMS + EregoylTMI;
ErhoregoylTMSandI = ErhoregoylTMS + ErhoregoylTMI;
EphiregoylTMSandI = EphiregoylTMS + EphiregoylTMI;

```

```

Etemp = EtempI + ExtempS;
Eshotemp = EshotempI + EshotempS;
Ephitemp = EphitempI + EphitempS;

```

Printed by Wolfram Mathematica Student Edition

Changing Rho Plot Calculations

Solution for Plots - Corrugated Cylinder

```

θ = θa; (*scattered field θ, possibly incident θ as well*)
(*θi=θ*)
θi = θvalue; (*Only if considered unique and distinct from scattered field*)
(*Incident + Scattered Solution*)
SolEz = N[Abs[Eztemp]];
dataEz = Transpose[{rhorange/lambda0, SolEz}];

SolEphi = N[Abs[Ephitemp]];
dataEphi = Transpose[{rhorange/lambda0, SolEphi}];

SolErho = N[Abs[Erhitemp]];
dataErho = Transpose[{rhorange/lambda0, SolErho}];

SolEallSandI = N[Abs[Sqrt[(Erhitemp * Cos[θ] - Ephitemp * Sin[θ])^2 +
    (Ehitemp * Sin[θ] + Eritemp * Cos[θ])^2 * (Eztemp)^2]]];
dataEallSandI = Transpose[{rhorange/lambda0, SolEallSandI}];

(*Scattered Only Solution*)
SolEs = N[Abs[Estemp]];
dataEs = Transpose[{rhorange/lambda0, SolEs}];

SolEphis = N[Abs[EphitempS]];
dataEphis = Transpose[{rhorange/lambda0, SolEphis}];

SolErhoS = N[Abs[ErhitempS]];
dataErhoS = Transpose[{rhorange/lambda0, SolErhoS}];

SolEallIS = N[Abs[Sqrt[(ErhitempS * Cos[θ] - EphitempS * Sin[θ])^2 +
    (EhitempS * Sin[θ] + EritempS * Cos[θ])^2 * (EstempS)^2]]];
dataEallIS = Transpose[{rhorange/lambda0, SolEallIS}];
    
```

Solution for Plots - Regular "Smooth" Cylinder

```

θ = θa; (*scattered field θ, possibly incident θ as well*)
(*θi=θ*)
θi = θvalue; (*Only if considered unique and distinct from scattered field*)
    
```

Printed by Wolfram Mathematica Student Edition

TM Mode Solutions

```

(*Incident + Scattered Solution*)
SolEzregoylTMSandI = N[Abs[EzregoylTMSandI]];
dataEzregoylTMSandI = Transpose[{rhorange/lambda0, SolEzregoylTMSandI}];

SolEhoregoylTMSandI = N[Abs[EhoregoylTMSandI]];
dataEhoregoylTMSandI = Transpose[{rhorange/lambda0, SolEhoregoylTMSandI}];

SolEphiregoylTMSandI = N[Abs[EphiregoylTMSandI]];
dataEphiregoylTMSandI = Transpose[{rhorange/lambda0, SolEphiregoylTMSandI}];

SolEallTMSandI =
    N[Abs[Sqrt[(EhoregoylTMSandI * Cos[θ] - EphiregoylTMSandI * Sin[θ])^2 +
    (EzregoylTMSandI * Sin[θ] + EhoregoylTMSandI * Cos[θ])^2 *
    (EzregoylTMSandI)^2]]];
dataEallTMSandI = Transpose[{rhorange/lambda0, SolEallTMSandI}];

(*Scattered Only Solution*)
SolEzregoylTMS = N[Abs[EzregoylTMS]];
dataEzregoylTMS = Transpose[{rhorange/lambda0, SolEzregoylTMS}];

SolEhoregoylTMS = N[Abs[EhoregoylTMS]];
dataEhoregoylTMS = Transpose[{rhorange/lambda0, SolEhoregoylTMS}];

SolEphiregoylTMS = N[Abs[EphiregoylTMS]];
dataEphiregoylTMS = Transpose[{rhorange/lambda0, SolEphiregoylTMS}];

SolEallTMS = N[Abs[Sqrt[(EhoregoylTMS * Cos[θ] - EphiregoylTMS * Sin[θ])^2 +
    (EzregoylTMS * Sin[θ] + EhoregoylTMS * Cos[θ])^2 * (EzregoylTMS)^2]]];
dataEallTMS = Transpose[{rhorange/lambda0, SolEallTMS}];
    
```

Printed by Wolfram Mathematica Student Edition

TE Mode Solutions

```

(*Incident + Scattered Solution*)
SolEzregoylTESandI = N[Abs[EzregoylTESandI]];
dataEzregoylTESandI = Transpose[{rhorange/lambda0, SolEzregoylTESandI}];

SolEhoregoylTESandI = N[Abs[EhoregoylTESandI]];
dataEhoregoylTESandI = Transpose[{rhorange/lambda0, SolEhoregoylTESandI}];

SolEphiregoylTESandI = N[Abs[EphiregoylTESandI]];
dataEphiregoylTESandI = Transpose[{rhorange/lambda0, SolEphiregoylTESandI}];

SolEallTESandI =
    N[Abs[Sqrt[(EhoregoylTESandI * Cos[θ] - EphiregoylTESandI * Sin[θ])^2 +
    (EzregoylTESandI * Sin[θ] + EhoregoylTESandI * Cos[θ])^2 *
    (EzregoylTESandI)^2]]];
dataEallTESandI = Transpose[{rhorange/lambda0, SolEallTESandI}];

(*Scattered Only Solution*)
SolEzregoylTES = N[Abs[EzregoylTES]];
dataEzregoylTES = Transpose[{rhorange/lambda0, SolEzregoylTES}];

SolEhoregoylTES = N[Abs[EhoregoylTES]];
dataEhoregoylTES = Transpose[{rhorange/lambda0, SolEhoregoylTES}];

SolEphiregoylTES = N[Abs[EphiregoylTES]];
dataEphiregoylTES = Transpose[{rhorange/lambda0, SolEphiregoylTES}];

SolEallTES = N[Abs[Sqrt[(EhoregoylTES * Cos[θ] - EphiregoylTES * Sin[θ])^2 +
    (EzregoylTES * Sin[θ] + EhoregoylTES * Cos[θ])^2 * (EzregoylTES)^2]]];
dataEallTES = Transpose[{rhorange/lambda0, SolEallTES}];
    
```

Printed by Wolfram Mathematica Student Edition

TM + TE Mode Solutions

```

(*Incident + Scattered Solution*)
SolEzregoylTMplusTESandI = N[Abs[EzregoylTMplusTESandI]];
dataEzregoylTMplusTESandI = Transpose[{rhorange/lambda0, SolEzregoylTMplusTESandI}];

SolEhoregoylTMplusTESandI = N[Abs[EhoregoylTMplusTESandI]];
dataEhoregoylTMplusTESandI = Transpose[{rhorange/lambda0, SolEhoregoylTMplusTESandI}];

SolEphiregoylTMplusTESandI = N[Abs[EphiregoylTMplusTESandI]];
dataEphiregoylTMplusTESandI = Transpose[{rhorange/lambda0, SolEphiregoylTMplusTESandI}];

SolEallTMplusTESandI =
    N[Abs[Sqrt[(EhoregoylTMplusTESandI * Cos[θ] - EphiregoylTMplusTESandI * Sin[θ])^2 +
    (EzregoylTMplusTESandI * Sin[θ] + EhoregoylTMplusTESandI * Cos[θ])^2 *
    (EzregoylTMplusTESandI)^2]]];
dataEallTMplusTESandI = Transpose[{rhorange/lambda0, SolEallTMplusTESandI}];

(*Scattered Only Solution*)
SolEzregoylTMplusTES = N[Abs[EzregoylTMplusTES]];
dataEzregoylTMplusTES = Transpose[{rhorange/lambda0, SolEzregoylTMplusTES}];

SolEhoregoylTMplusTES = N[Abs[EhoregoylTMplusTES]];
dataEhoregoylTMplusTES = Transpose[{rhorange/lambda0, SolEhoregoylTMplusTES}];

SolEphiregoylTMplusTES = N[Abs[EphiregoylTMplusTES]];
dataEphiregoylTMplusTES = Transpose[{rhorange/lambda0, SolEphiregoylTMplusTES}];

SolEallTMplusTES = N[Abs[Sqrt[(EhoregoylTMplusTES * Cos[θ] - EphiregoylTMplusTES * Sin[θ])^2 +
    (EzregoylTMplusTES * Sin[θ] + EhoregoylTMplusTES * Cos[θ])^2 *
    (EzregoylTMplusTES)^2]]];
dataEallTMplusTES = Transpose[{rhorange/lambda0, SolEallTMplusTES}];
    
```

Printed by Wolfram Mathematica Student Edition

Changing Rho XY Plots

Table of Parameters

```

%%1070: tablevalues = {[N(H0) "V/m", "-", "-", "-", "-"], [N(H0) "A/m", "-", "-", "-", "-"]},
    (lambda0 "m", "-", "-", "-", "-"), (f0 "Hz", "-", "-", "-", "-"),
    (a/lambda0 "lambda", "-", "-", "-", "-"), (b/lambda0 "lambda", "-", "-", "-", "-"),
    (rho/lambda0 "lambda", "-", "-", "-", "-"), (rho2/lambda0 "lambda", "-", "-", "-", "-"),
    ["-", rhomin/lambda0 "lambda", rhomax/lambda0 "lambda", rhodelta/lambda0 "lambda",
    Length(rhorange)], [N(a * (180/Pi)) "Deg", "-", "-", "-", "-"],
    (rho1/a "m" is rho1at/lambda0 "lambda", "-", "-", "-", "-"),
    ["-", "-", "-", "-", "deg"], [N(a1 * (180/Pi)) "Deg", "-", "-", "-", "-"],
    ["-", "min", "max", "l", "qty"], ["-", "lmin", "lmax", "l", "qty"],
    ["-", "min", "max", "l", "qty"], (smaxcheck, "-", "-", "-", "-"),
    [lmaxcheck, "-", "-", "-", "-"], ["Boundary sub", "-", "-", "-", "-"];
tablecheading = ("E0", "H0", "rho", "rho2", "Frequency", "a1", "b1", "rho1", "rho2",
    "a range", "a0 (observed)", "a (observed)", "Matching Points", "a0",
    "a1", "a", "l", "m", "max allowable m", "max allowable l", "Boundary");
tablecheading = ("value", "min", "max", "delta", "Qty of Points");
%%1071: ChangingRhoTable = Grid(ArrayFlatten({{" " }}, tablecheading));
%%1072: ItemStyle = {Bold, 20, Frame = All, Background = {LightGray}, LightGray}};
%%1073: Export(Totting(StringForm{" ".jpg", RhoTablename}), ChangingRhoTable)

```

Corrugated Cylinder Plots

Plot Ez (Scattered)

```

%%1074: EzCorrS = ListLinePlot[dataEzS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEzS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot Ez (Inc + Scattered)

```

%%1075: EzCorrSandI = ListLinePlot[dataEz, PlotStyle -> {Red, Dashed},
    AbsoluteThickness[2], PlotMarkers -> None,
    PlotLabel -> "Ez Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot Erho (Scattered)

```

%%1076: ErhoCorrS = ListLinePlot[dataErhoS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolErhoS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Erho Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot Erho (Inc + Scattered)

```

%%1077: ErhoCorrSandI = ListLinePlot[dataErho,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolErho]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "Erho Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot Ephi (Scattered)

```

%%1078: EphiCorrS = ListLinePlot[dataEphiS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEphiS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
    PlotMarkers -> None, PlotLabel -> "Ephi Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot Ephi (Inc + Scattered)

```

%%1079: EphiCorrSandI = ListLinePlot[dataEphi,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEphi]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "Ephi Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot EAll (Scattered)

```

%%1080: EAllCorrS = ListLinePlot[dataEAllS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEAllS]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "EAll Corrugated Cylinder (Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Plot EAll (Inc + Scattered)

```

%%1081: EAllCorrSandI = ListLinePlot[dataEAllSandI,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEAllSandI]}},
    PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2], PlotMarkers ->
    None, PlotLabel -> "EAll Corrugated Cylinder (Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Summary TM Plots

```

%%1082: GraphicsGrid[{{EzCorrS, EzCorrSandI}, {ErhoCorrS, ErhoCorrSandI}},
    {EphiCorrS, EphiCorrSandI}, {EAllCorrS, EAllCorrSandI}],
    Spacings -> {Scaled[0], Scaled[0]};

```

Smooth Cylinder Plots - TM Plots

Ez (TM Scattered)

```

%%1083: EzRegCylTMS = ListLinePlot[dataEzregCylTMS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEzregCylTMS]}},
    PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
    PlotLabel -> "Ez Smooth Cylinder (TM Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Ez (TM Inc + Scattered)

```

%%1084: EzRegCylTMSandI = ListLinePlot[dataEzregCylTMSandI, PlotRange ->
    {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolEzregCylTMSandI]}},
    PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
    PlotLabel -> "Ez Smooth Cylinder (TM Incident + Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Erho (TM Scattered)

```

%%1085: ErhoRegCylTMS = ListLinePlot[dataErhoRegCylTMS,
    PlotRange -> {{rhomin/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTMS]}},
    PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
    PlotLabel -> "Erho Smooth Cylinder (TM Scattered Field)",
    Frame -> True, FrameLabel -> {"rho/lambda", "V/m"},
    GridLines -> {{{rho2/lambda0}, {Thick, Gray, Dashed}}, Automatic},
    Background -> White, ImageSize -> 700,
    BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"};

```

Erho (TM Inc + Scattered)

```

14198 ErhoRegCylTMSandI = ListLinePlot[dataErhoRegCylTMSandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Ephi (TM Scattered)

```

14199 EphiRegCylTMS = ListLinePlot[dataEphiRegCylTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Ephi (TM Inc + Scattered)

```

14200 EphiRegCylTMSandI = ListLinePlot[dataEphiRegCylTMSandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Printed by Wolfram Mathematica Student Edition

EAll (TM Scattered)

```

14201 EAllRegCylTMS = ListLinePlot[dataEAllTMS,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMS]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Smooth Cylinder (TM Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

EAll (TM Inc + Scattered)

```

14202 EAllRegCylTMSandI = ListLinePlot[dataEAllTMSandI,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTMSandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Smooth Cylinder (TM Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Summary TM Plots

```

14203 GraphicsGrid[{{ERegCylTMS, ERegCylTMSandI},
  {ErhoRegCylTMS, ErhoRegCylTMSandI}, {EphiRegCylTMS, EphiRegCylTMSandI},
  {EAllRegCylTMS, EAllRegCylTMSandI}}, Spacings -> {Scaled[0], Scaled[0]}];
  
```

Smooth Cylinder Plots - TE Plots

Ez (TE Scattered)

```

14204 ERegCylTES = ListLinePlot[dataEregCylTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEregCylTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Printed by Wolfram Mathematica Student Edition

Ez (TE Inc + Scattered)

```

14205 ERegCylTESandI = ListLinePlot[dataEregCylTESandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEregCylTESandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Erho (TE Scattered)

```

14206 ErhoRegCylTES = ListLinePlot[dataErhoRegCylTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Erho (TE Inc + Scattered)

```

14207 ErhoRegCylTESandI = ListLinePlot[dataErhoRegCylTESandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolErhoRegCylTESandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Erho Smooth Cylinder (TE Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Printed by Wolfram Mathematica Student Edition

Ephi (TE Scattered)

```

14208 EphiRegCylTES = ListLinePlot[dataEphiRegCylTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Ephi (TE Inc + Scattered)

```

14209 EphiRegCylTESandI = ListLinePlot[dataEphiRegCylTESandI, PlotRange ->
  {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEphiRegCylTESandI]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ephi Smooth Cylinder (TE Incident + Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

EAll (TE Scattered)

```

14210 EAllRegCylTES = ListLinePlot[dataEAllTES,
  PlotRange -> {{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllTES]}},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "EAll Smooth Cylinder (TE Scattered Field)",
  Frame -> True, FrameLabel -> {"ρ/λ", "V/m"},
  GridLines -> {{{ρ2/lambda0, {Thick, Gray, Dashed}}}, Automatic},
  Background -> White, ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
  
```

Printed by Wolfram Mathematica Student Edition


```
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[ErhoRegCylTESandI, ErhoCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTESandI, SolErho]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TE Inc + Scattered Smooth Cylinder (Blue) vs Corrugated
Cylinder (Red, --)"]; Show[ErhoRegCylTMplusTESandI,
ErhoCorrSandI, PlotRange -> {{rhomIn/lambda0, rhomax/lambda0},
{0, Max[SolEhoregCylTMplusTESandI, SolErho]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM-TE Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

[Show[EphiRegCylTMS, EphiCorrS, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEhoregCylTMS, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM Scattered Smooth Cylinder (Blue)
vs Corrugated Cylinder (Red, --)"];
Show[EphiRegCylTES, EphiCorrS, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTES, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TE Scattered Smooth Cylinder (Blue)
vs Corrugated Cylinder (Red, --)"];
Show[EphiRegCylTMplusTES, EphiCorrS, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTMplusTES, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM-TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

[Show[EphiRegCylTMSandI, EphiCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTMSandI, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EphiRegCylTESandI, EphiCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTESandI, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EphiRegCylTMplusTESandI, EphiCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEhoregCylTMplusTESandI, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM-TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

Printed by Wolfram Mathematica Student Edition
```

```
PlotLabel -> "E_r, TE Inc + Scattered Smooth Cylinder (Blue) vs Corrugated
Cylinder (Red, --)"]; Show[EphiRegCylTMplusTESandI,
EphiCorrSandI, PlotRange -> {{rhomIn/lambda0, rhomax/lambda0},
{0, Max[SolEhoregCylTMplusTESandI, SolEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r, TM-TE Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

[Show[EAllRegCylTMS, EAllCorrS, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllS, SolEAllTMS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EAllRegCylTES, EAllCorrS, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEAllS, SolEAllTES]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EAllRegCylTMplusTES, EAllCorrS, PlotRange ->
{{rhomIn/lambda0, rhomax/lambda0}, {0, Max[SolEAllS, SolEAllTMplusTES]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM-TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

[Show[EAllRegCylTMSandI, EAllCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEAllTMSandI, SolEAllSandI]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EAllRegCylTESandI, EAllCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEAllTMplusTESandI, SolEAllSandI]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM-TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];
Show[EAllRegCylTMplusTESandI, EAllCorrSandI, PlotRange -> {{rhomIn/lambda0,
rhomax/lambda0}, {0, Max[SolEAllTMplusTESandI, SolEAllSandI]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM-TE Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"];

Printed by Wolfram Mathematica Student Edition
```

```
Frame -> True, FrameLabel -> {"p/A", "V/m"},
PlotLabel -> "E_r,all TM-TE Inc + Scattered Smooth
Cylinder (Blue) vs Corrugated Cylinder (Red, --)"];
}];
Export[ToString[StringForm["", RhoXYPLOTS]], RhoXYPLOTS];
Print["The rho plots are done"]
```

Import Data [Changing Phi Data]

Boundary 'a' Data

```
PHI0 = dataa = Import["phi_outa.mx"];
PHI1 = a = dataa[[1]];
PHI2 = b = dataa[[2]];
PHI3 = p2 = dataa[[3]];
PHI4 = p1 = dataa[[4]];
PHI5 = EtempSa = dataa[[5]];
PHI6 = EstempSa = dataa[[6]];
PHI7 = ErhotempSa = dataa[[7]];
PHI8 = Erhotempia = dataa[[8]];
PHI9 = EphitempSa = dataa[[9]];
PHI10 = Ephitempia = dataa[[10]];
PHI11 = EeregcyITMSa = dataa[[11]];
PHI12 = EeregcyITMSa = dataa[[12]];
PHI13 = EeregcyITMSa = dataa[[13]];
PHI14 = EeregcyITMSa = dataa[[14]];
PHI15 = EeregcyITMSa = dataa[[15]];
PHI16 = EeregcyITMSa = dataa[[16]];
PHI17 = EeregcyITMSa = dataa[[17]];
PHI18 = EeregcyITMSa = dataa[[18]];
PHI19 = EeregcyITMSa = dataa[[19]];
PHI20 = EeregcyITMSa = dataa[[20]];

Printed by Wolfram Mathematica Student Edition
```

```
PHI21 = EphiRegCylTEIa = dataa[[21]];
PHI22 = EphiRegCylTMIa = dataa[[22]];
PHI23 = phiRange = dataa[[23]];
PHI24 = p = dataa[[24]];
PHI25 = lambda0 = dataa[[25]];
PHI26 = o1 = dataa[[26]];
PHI27 = phidelta = dataa[[27]];

Printed by Wolfram Mathematica Student Edition
```

Boundary 'b' Data

```
PHI28 = datab = Import["phi_outb.mx"];
PHI29 = a = datab[[1]];
PHI30 = b = datab[[2]];
PHI31 = p2 = datab[[3]];
PHI32 = p1 = datab[[4]];
PHI33 = EstempSb = datab[[5]];
PHI34 = EstempIb = datab[[6]];
PHI35 = ErhotempSb = datab[[7]];
PHI36 = ErhotempIb = datab[[8]];
PHI37 = EphitempSb = datab[[9]];
PHI38 = EphitempIb = datab[[10]];
PHI39 = EeregcyITMSb = datab[[11]];
PHI40 = EeregcyITMSb = datab[[12]];
PHI41 = EeregcyITMSb = datab[[13]];
PHI42 = EeregcyITMSb = datab[[14]];
PHI43 = EeregcyITMSb = datab[[15]];
PHI44 = EeregcyITMSb = datab[[16]];
PHI45 = EeregcyITMSb = datab[[17]];
PHI46 = EeregcyITMSb = datab[[18]];
PHI47 = EeregcyITMSb = datab[[19]];
PHI48 = EeregcyITMSb = datab[[20]];
PHI49 = EeregcyITMSb = datab[[21]];

Printed by Wolfram Mathematica Student Edition
```



```

SolEAllTMplusTESandI =
N[Abs[Sqrt[(EhoregcyITESandI + ErhoregcyITMSandI) * Cos[phiRange] -
(EphiregcyITESandI + EprhoregcyITMSandI) * Sin[phiRange]]^2 +
(EhoregcyITESandI + ErhoregcyITMSandI) * Sin[phiRange] +
(EphiregcyITESandI + EprhoregcyITMSandI) * Cos[phiRange]]^2 +
(EzregcyITESandI + EzregcyITMSandI)^2]];
dataEAllTMplusTESandI = Transpose[phiRange, SolEAllTMplusTESandI];

(*Scattered Only Solutions*)
SolEzregcyITMplusTES = N[Abs[EzregcyITES + EzregcyITMS]];
dataEzregcyITMplusTES = Transpose[phiRange, SolEzregcyITMplusTES];

SolEphiregcyITMplusTES = N[Abs[EphiregcyITES + ErhoregcyITMS]];
dataEphiregcyITMplusTES = Transpose[phiRange, SolEphiregcyITMplusTES];

SolEzregcyITMplusTES = N[Abs[EzregcyITES + ErhoregcyITMS]];
dataEzregcyITMplusTES = Transpose[phiRange, SolEzregcyITMplusTES];

SolEphiregcyITMplusTES = N[Abs[EphiregcyITES + ErhoregcyITMS]];
dataEphiregcyITMplusTES = Transpose[phiRange, SolEphiregcyITMplusTES];

SolEAllTMplusTES = N[Abs[Sqrt[(EhoregcyITES + ErhoregcyITMS) * Cos[phiRange] -
(EphiregcyITES + EprhoregcyITMS) * Sin[phiRange]]^2 +
(EhoregcyITES + ErhoregcyITMS) * Sin[phiRange] +
(EphiregcyITES + EprhoregcyITMS) * Cos[phiRange]]^2 +
(EzregcyITES + EzregcyITMS)^2]];
dataEAllTMplusTES = Transpose[phiRange, SolEAllTMplusTES];

(*RCS Solution*)
RCSolEzregcyITMplusTES = (4 * Pi * (rho^2)) *
((Abs[EzregcyITES + EzregcyITMS])^2) / ((Abs[EzregcyITES + EzregcyITMS])^2);
RCSdataEzregcyITMplusTES = Transpose[phiRange, RCSolEzregcyITMplusTES];

RCSolEphiregcyITMplusTES =
(4 * Pi * (rho^2)) * ((Abs[EphiregcyITES + ErhoregcyITMS])^2) /
((Abs[EphiregcyITES + ErhoregcyITMS])^2);
RCSdataEphiregcyITMplusTES = Transpose[phiRange, RCSolEphiregcyITMplusTES];

RCSolEzregcyITMplusTES =
(4 * Pi * (rho^2)) * ((Abs[EzregcyITES + ErhoregcyITMS])^2) /
((Abs[EzregcyITES + ErhoregcyITMS])^2);
RCSdataEzregcyITMplusTES = Transpose[phiRange, RCSolEzregcyITMplusTES];

RCSolEphiregcyITMplusTES = Sqrt[
(EhoregcyITES + ErhoregcyITMS) * Cos[phiRange] - (EphiregcyITES + EprhoregcyITMS) *
Sin[phiRange]]^2 + (EhoregcyITES + ErhoregcyITMS) * Sin[phiRange] +

```

```

(EphiregcyITES + EprhoregcyITMS) * Cos[phiRange]]^2 +
(EzregcyITES + EzregcyITMS)^2];
RCSolEzregcyITMplusTESallI = Sqrt[(EhoregcyITES + ErhoregcyITMS) * Cos[phiRange] -
(EphiregcyITES + EprhoregcyITMS) * Sin[phiRange]]^2 +
(EhoregcyITES + ErhoregcyITMS) * Sin[phiRange] +
(EphiregcyITES + EprhoregcyITMS) * Cos[phiRange]]^2 +
(EzregcyITES + EzregcyITMS)^2];
RCSdataEzregcyITMplusTESallI = (4 * Pi * (rho^2)) *
((Abs[RCSolEzregcyITMplusTESallI])^2) / ((Abs[RCSolEzregcyITMplusTESallI])^2);
RCSdataEzregcyITMplusTESallI = Transpose[phiRange, RCSolEzregcyITMplusTESallI];

(*RCS Solution - In dB*)
RCSdataEzregcyITMplusTESdB =
Transpose[phiRange, 10 * Log10[RCSolEzregcyITMplusTES]];
RCSdataEphiregcyITMplusTESdB =
Transpose[phiRange, 10 * Log10[RCSolEphiregcyITMplusTES]];
RCSdataEzregcyITMplusTESdB =
Transpose[phiRange, 10 * Log10[RCSolEzregcyITMplusTES]];
RCSdataEzregcyITMplusTESallIDB =
Transpose[phiRange, 10 * Log10[RCSolEzregcyITMplusTESallI]];

```

Changing Phi Polar Plots

Table of Parameters

```

14180. tableValues = {{N[E0] "V/m", "-", "-", "-", "-"},
{N[R0] "A/m", "-", "-", "-", "-"}, {f0 "Hz", "-", "-", "-", "-"},
{lambda0 "m", "-", "-", "-", "-"}, {a / lambda0 "λ", "-", "-", "-", "-"},
{b / lambda0 "λ", "-", "-", "-", "-"}, {c1 / lambda0 "λ", "-", "-", "-", "-"},
{c2 / lambda0 "λ", "-", "-", "-", "-"}, {"-", N[phiRange][[1]] + (180 / Pi)] "Deg",
N[phiRange][Length[phiRange]] + (180 / Pi)] "Deg",
N[phiDelta] + (180 / Pi)] "Deg", Length[phiRange], {d / lambda0 "λ", "-",
"-", "-", "-"}, {spotout / a "a" at apoint / lambda0 "λ", "-", "-", "-", "-"},
{"-", "-", "-", "-", "deg"}, {N[d1] + (180 / Pi)] "Deg", "-", "-", "-", "-"},
{N[d1] + (180 / Pi)] "Deg", "-", "-", "-", "-"},
{"-", "min", "max", "l", "eqty"}, {"-", "min", "max", "l", "eqty"},
{"-", "min", "max", "l", "eqty"}, {maxcheck, "-", "-", "-", "-"},
{maxcheck, "-", "-", "-", "-"}, {"Boundary a+b", "-", "-", "-", "-"},
{tableRowHeading = {"R0", "f0", "λ", "Frequency", "a", "b", "c1", "c2",
"φ range", "d (observed)", "z (observed)", "Matching Points", "d1",
"d1", "d1", "m", "max allowable m", "max allowable l", "Boundary"},
tableColHeading = {"value", "min", "max", "delta", "Qty of Points"}];
14181. ChangingPhiTable = Grid[ArrayFlatten[{{{"-", "-"}, {tableColHeading}},
{List[tableRowHeading, ArrayFlatten[tableValues]}]}],
ItemStyle -> {Bold, 10}, Frame -> All, Background -> {{LightGray}, {LightGray}}];
14182. Export[ToString[StringForm["", PhiTable]], ChangingPhiTable]

```

Corrugated Cylinder Plots

Plot Ez (Scattered)

```

14183. EzCorr = ListPolarPlot[dataEz, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Corrugated Cylinder (Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEz]}];

```

Plot Ez (Inc + Scattered)

```

14184. EzCorrInc = ListPolarPlot[dataEz, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Corrugated Cylinder (Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEz]}];

```

Plot Erho (Scattered)

```

14185. ErhoCorr = ListPolarPlot[dataErho, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Erho Corrugated Cylinder (Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErho]}];

```

Plot Erho (Inc + Scattered)

```

14186. ErhoCorrInc = ListPolarPlot[dataErho, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Erho Corrugated Cylinder (Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErho]}];

```

Plot Ephi (Scattered)

```

14187. EphiCorr = ListPolarPlot[dataEphi, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ephi Corrugated Cylinder (Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphi]}];

```

Plot Ephi (Inc + Scattered)

```

14188. EphiCorrInc = ListPolarPlot[dataEphi, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ephi Corrugated Cylinder (Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphi]}];

```

Plot EAll (Scattered)

```

%%EAll = ListPolarPlot[dataEAllS, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal: Corrugated Cylinder (Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllS]};
    
```

Plot EAll (Inc + Scattered)

```

%%EAllCorrSandI =
ListPolarPlot[dataEAllSandI, Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal: Corrugated Cylinder (Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllSandI]};
    
```

Summary Corrugated Cylinder Plots

```

%%EAllGraphicsGrid[
{{EAllCorr, EAllCorrSandI}, {ErhoCorr, ErhoCorrSandI}, {EphiCorr, EphiCorrSandI},
{EAllCorr, EAllCorrSandI}], Spacings -> {Scaled[0], Scaled[0]};
    
```

Smooth Cylinder Plots - TM Plots

Ez (TM Scattered)

```

%%EzRegCylTMSandI = ListPolarPlot[dataEzregcylTMS, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez: Smooth Cylinder (TM Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzregcylTMS]};
    
```

Ez (TM Inc + Scattered)

```

%%EzRegCylTMSandI = ListPolarPlot[dataEzregcylTMSandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez: Smooth Cylinder (TM Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzregcylTMSandI]};
    
```

Erho (TM Scattered)

```

%%ErhoRegCylTMS = ListPolarPlot[dataErhoRegcylTMS, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TM Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoRegcylTMS]};
    
```

Erho (TM Inc + Scattered)

```

%%ErhoRegCylTMSandI = ListPolarPlot[dataErhoRegcylTMSandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TM Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoRegcylTMSandI]};
    
```

Ephi (TM Scattered)

```

%%EphiRegCylTMS = ListPolarPlot[dataEphiRegcylTMS, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ: Smooth Cylinder (TM Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphiRegcylTMS]};
    
```

Ephi (TM Inc + Scattered)

```

%%EphiRegCylTMSandI = ListPolarPlot[dataEphiRegcylTMSandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ: Smooth Cylinder (TM Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEphiRegcylTMSandI]};
    
```

EAll(TM Scattered)

```

%%EAllRegCylTMS = ListPolarPlot[dataEAllTMS, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal: Smooth Cylinder (TM Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllTMS]};
    
```

EAll (TM Inc + Scattered)

```

%%EAllRegCylTMSandI = ListPolarPlot[dataEAllTMSandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal: Smooth Cylinder (TM Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllTMSandI]};
    
```

Summary TM Plots

```

%%EAllGraphicsGrid[{{EzRegCylTMS, EzRegCylTMSandI},
{ErhoRegCylTMS, ErhoRegCylTMSandI}, {EphiRegCylTMS, EphiRegCylTMSandI},
{EAllRegCylTMS, EAllRegCylTMSandI}], Spacings -> {Scaled[0], Scaled[0]};
    
```

Smooth Cylinder Plots - TE Plots

Ez (TE Scattered)

```

%%EzRegCylTES = ListPolarPlot[dataEzregcylTES, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez: Smooth Cylinder (TE Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzregcylTES]};
    
```

Ez (TE Inc + Scattered)

```

%%EzRegCylTESandI = ListPolarPlot[dataEzregcylTESandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez: Smooth Cylinder (TE Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEzregcylTESandI]};
    
```

Erho (TE Scattered)

```

%%ErhoRegCylTES = ListPolarPlot[dataErhoRegcylTES, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TE Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoRegcylTES]};
    
```

Erho (TE Inc + Scattered)

```

%%ErhoRegCylTESandI = ListPolarPlot[dataErhoRegcylTESandI, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TE Incident + Scattered Field)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolErhoRegcylTESandI]};
    
```



```

Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[SolEAllTMpluTES, SolEAllS]}],

{ListPolarPlot[{dataEAllTMSandI, dataEAllSandI},
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal TM Incident + Scattered (V/m) Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[SolEAllTMSandI, SolEAllSandI]}],
ListPolarPlot[{dataEAllTESandI, dataEAllSandI},
Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Etotal TE Incident + Scattered (V/m) Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[SolEAllTMpluTESandI, SolEAllSandI]}];
}
Export[ToString[StringForm["", .jpg], PhiPolarPlotName], PhiPolarPlots]

```

Changing Phi RCS Polar Plots

Corrugated Cylinder Plots

Plot Ez

```

%%1004 - RCSEzCorr = ListPolarPlot[RCSdataEz, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEz]}];

```

Plot Erho

```

%%1005 - RCSErhoCorr = ListPolarPlot[RCSdataErho, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErho]}];

```

Plot Ephi

```

%%1006 - RCSEphiCorr = ListPolarPlot[RCSdataEphi, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphi]}];

```

Plot EAll

```

%%1007 - RCSEAllCorr = ListPolarPlot[RCSdataEAll, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal Corrugated Cylinder (RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEAll]}];

```

Summary Corrugated Cylinder Plots

```

%%1008 - GraphicsGrid[{{RCSzCorr}, {RCSrhoCorr}, {RCSphiCorr}, {RCSAllCorr}},
Spacings -> {Scaled[0], Scaled[0]}];

```

Smooth Cylinder Plots - TM Plots

Ez (TM RCS)

```

%%1009 - RCSEzRegCylTM = ListPolarPlot[RCSdataEzregCylTM, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEzregCylTM]}];

```

Erho (TM RCS)

```

%%1010 - RCSErhoRegCylTM = ListPolarPlot[RCSdataErhoRegCylTM, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErhoRegCylTM]}];

```

Ephi (TM RCS)

```

%%1011 - RCSEphiRegCylTM = ListPolarPlot[RCSdataEphiRegCylTM, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphiRegCylTM]}];

```

EAll (TM RCS)

```

%%1012 - RCSEAllRegCylTM = ListPolarPlot[RCSdataEregCylTMAll, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal Smooth Cylinder (TM RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEregCylTMAll]}];

```

Summary TM Plots

```

%%1013 - GraphicsGrid[{{RCSzRegCylTM}, {RCSrhoRegCylTM}, {RCSphiRegCylTM},
{RCSAllRegCylTM}}, Spacings -> {Scaled[0], Scaled[0]}];

```

Smooth Cylinder Plots - TE Plots

Ez (TE RCS) - DOES NOT EXIST

Erho (TE RCS)

```

%%1014 - RCSErhoRegCylTE = ListPolarPlot[RCSdataErhoRegCylTE, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TE RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolErhoRegCylTE]}];

```

Ephi (TE RCS)

```

%%1015 - RCSEphiRegCylTE = ListPolarPlot[RCSdataEphiRegCylTE, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TE RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEphiRegCylTE]}];

```

EAll (TE RCS)

```

%%1016 - RCSEAllRegCylTE = ListPolarPlot[RCSdataEregCylTEAll, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Etotal Smooth Cylinder (TE RCS m2)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSzSolEregCylTEAll]}];

```

Summary TE Plots

```

%%1017 - GraphicsGrid[{{RCSrhoRegCylTE}, {RCSphiRegCylTE}, {RCSAllRegCylTE}},
Spacings -> {Scaled[0], Scaled[0]}];

```

Smooth Cylinder Plots - TM + TE Plots

Ez (TM + TE RCS)

```
RCSERegCylTMplusTE = ListPolarPlot[RCSdataEzregcylTMplusTE, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS m²)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEzregcylTMplusTE]}];
```

Erho (TM + TE RCS)

```
RCSERhoRegCylTMplusTE = ListPolarPlot[RCSdataErhoRegcylTMplusTE, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Erho Smooth Cylinder (TM + TE RCS m²)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataErhoRegcylTMplusTE]}];
```

Ephi (TM + TE RCS)

```
RCSERphiRegCylTMplusTE = ListPolarPlot[RCSdataEphiRegcylTMplusTE, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ephi Smooth Cylinder (TM + TE RCS m²)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEphiRegcylTMplusTE]}];
```

EAll (TM + TE RCS)

```
RCSERAllRegCylTMplusTE = ListPolarPlot[RCSdataEregcylTMplusTEAll, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eregcyl Smooth Cylinder (TM + TE RCS m²)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEregcylTMplusTEAll]}];
```

Summary TM + TE Plots

```
GraphicsGrid[
{{RCSERegCylTMplusTE, RCSERhoRegCylTMplusTE}, {RCSERphiRegCylTMplusTE,
RCSERAllRegCylTMplusTE}}, Spacings -> {Scaled[0], Scaled[0]}];
```

Compare (Regular vs Corrugated) Plots

TM, TE, and TM+TE Compare

```
PHRCSERPolarPlots =
GraphicsGrid[{{ListPolarPlot[RCSdataEzregcylTM, RCSdataErho],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"Ez, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEzregcylTM, RCSdataErho]}],
"Er TE Does Not Exist"},
{ListPolarPlot[RCSdataEphiRegcylTM, RCSdataEphi],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ephi, TM TE RCS (m²) Smooth Cylinder (Blue) vs
Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEphiRegcylTM, RCSdataEphi]}],
{ListPolarPlot[RCSdataEzregcylTM, RCSdataErho],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"Ez, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEzregcylTM, RCSdataErho]}],
{ListPolarPlot[RCSdataEzregcylTM, RCSdataErho],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
```

```
"Ez, TE RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEzregcylTE, RCSdataErho]}];
```

```
ListPolarPlot[RCSdataEzregcylTMplusTE, RCSdataErho],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez, TM-TE RCS (m²) Smooth Cylinder (Blue) vs
Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEzregcylTMplusTE, RCSdataErho]}],
},
{ListPolarPlot[RCSdataEphiRegcylTM, RCSdataEphi],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"Ez, TM RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEphiRegcylTM, RCSdataEphi]}];
```

```
ListPolarPlot[RCSdataEphiRegcylTE, RCSdataEphi],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"Ez, TE RCS (m²) Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[RCSdataEphiRegcylTE, RCSdataEphi]}];
```

```
ListPolarPlot[RCSdataEzregcylTMplusTE, RCSdataEphi],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
"Ez, TM-TE RCS (m²) Smooth Cylinder (Blue) vs
Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEzregcylTMplusTE, RCSdataEphi]}],
},
{ListPolarPlot[RCSdataEregcylTMAll, RCSdataEAll],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None, PlotLabel ->
```

```
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eregcyl TM RCS (m²) Smooth Cylinder (Blue) vs
Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEregcylTMAll, RCSdataEAll]}];
```

```
ListPolarPlot[RCSdataEregcylTEAll, RCSdataEAll],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eregcyl TE RCS (m²) Smooth Cylinder (Blue) vs
Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEregcylTEAll, RCSdataEAll]}];
```

```
ListPolarPlot[RCSdataEregcylTMplusTEAll, RCSdataEAll],
Joined -> True, PolarGridLines -> Automatic,
PolarTicks -> {"Degrees", Automatic}, PlotStyle -> {Blue, {Red, Dashed}},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eregcyl TM-TE RCS (m²) Smooth Cylinder (Blue)
vs Corrugated Cylinder (Red, --)", ImageSize -> 700,
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes -> True,
PolarAxesOrigin -> {0, Max[RCSdataEregcylTMplusTEAll, RCSdataEAll]}];
```

```
Export[ToString[StringForm["*", "jpg", PHRCSERPolarPlotsName]], PHRCSERPolarPlots];
```

Changing Phi RCS dB Polar Plots

Corrugated Cylinder Plots

Plot Ez

```
RCSERCorrDB = ListPolarPlot[RCSdataErhoDB, Joined -> True,
PolarGridLines -> Automatic, PolarTicks -> {"Degrees", Automatic},
PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
PlotMarkers -> None, PlotLabel -> "Ez, Corrugated Cylinder (RCS dBsm)",
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
PolarAxes -> True, PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSdataErho]]]}];
```

Plot Erho

```

%%1030 RCSrhoCorrDB = ListPolarPlot[RCSdataRrhoDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes = True, PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRho]]]};
    
```

Plot Ephi

```

%%1030 RCSphiCorrDB = ListPolarPlot[RCSdataEphiDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes = True, PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSphiRho]]]};
    
```

Plot EAll

```

%%1030 RCSAllCorrDB = ListPolarPlot[RCSdataEAllDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> {Red, Dashed}, BaseStyle -> AbsoluteThickness[2],
  PlotMarkers -> None, PlotLabel -> "Ez Corrugated Cylinder (RCS dBsm)",
  ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
  PolarAxes = True, PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSAllRho]]]};
    
```

Summary Corrugated Cylinder Plots

```

%%1030 GraphicsGrid[{{RCSrhoCorrDB}, {RCSphiCorrDB}, {RCSrhoRhoDB}, {RCSphiRhoDB}},
  Spacings -> {Scaled[0], Scaled[0]};
    
```

Smooth Cylinder Plots - TM Plots

Ez (TM RCS)

```

%%1030 RCSrhoRegCylTMDB = ListPolarPlot[RCSdataEregCylTMDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRegCylTM]]]};
    
```

Erho (TM RCS)

```

%%1030 RCSrhoRegCylTMDB = ListPolarPlot[RCSdataEregCylTMDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRegCylTM]]]};
    
```

Ephi (TM RCS)

```

%%1030 RCSphiRegCylTMDB = ListPolarPlot[RCSdataEphiRegCylTMDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSphiRegCylTM]]]};
    
```

EAll (TM RCS)

```

%%1030 RCSAllRegCylTMDB = ListPolarPlot[RCSdataEregCylTMAllDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSAllRegCylTM]]]};
    
```

Summary TM Plots

```

%%1030 GraphicsGrid[{{RCSrhoRegCylTMDB}, {RCSphiRegCylTMDB}, {RCSrhoRegCylTMDB},
  {RCSphiRegCylTMDB}}, Spacings -> {Scaled[0], Scaled[0]};
    
```

Smooth Cylinder Plots - TE Plots

Ez (TE RCS) - DOES NOT EXIST

Erho (TE RCS)

```

%%1030 RCSrhoRegCylTEDB = ListPolarPlot[RCSdataEregCylTEDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRegCylTE]]]};
    
```

Ephi (TE RCS)

```

%%1030 RCSphiRegCylTEDB = ListPolarPlot[RCSdataEphiRegCylTEDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSphiRegCylTE]]]};
    
```

EAll (TE RCS)

```

%%1030 RCSAllRegCylTEDB = ListPolarPlot[RCSdataEregCylTEAllDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSAllRegCylTEAll]]]};
    
```

Summary TE Plots

```

%%1030 GraphicsGrid[{{RCSrhoRegCylTEDB}, {RCSphiRegCylTEDB}, {RCSAllRegCylTEDB}},
  Spacings -> {Scaled[0], Scaled[0]};
    
```

Smooth Cylinder Plots - TM + TE Plots

Ez (TM + TE RCS)

```

RCSrhoRegCylTMplusTEDB = ListPolarPlot[RCSdataEregCylTMplusTEDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRegCylTMplusTE]]]};
    
```

Erho (TM + TE RCS)

```

RCSrhoRegCylTMplusTEDB = ListPolarPlot[RCSdataEregCylTMplusTEDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSrhoRegCylTMplusTE]]]};
    
```

Ephi (TM + TE RCS)

```

RCSphiRegCylTMplusTEDB = ListPolarPlot[RCSdataEphiRegCylTMplusTEDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSphiRegCylTMplusTE]]]};
    
```

EAll (TM + TE RCS)

```

RCSAllRegCylTMplusTEDB = ListPolarPlot[RCSdataEregCylTMplusTEAllDB, Joined = True,
  PolarGridLines = Automatic, PolarTicks = {"Degrees", Automatic},
  PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
  PlotLabel -> "Ez Smooth Cylinder (TM + TE RCS dBsm)", ImageSize -> 700,
  BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, PolarAxes = True,
  PolarAxesOrigin -> {0, Max[Abs[10 * Log10[RCSAllRegCylTMplusTEAll]]]};
    
```


Plot EAll (Inc + Scattered)

```

10198: EAllCorrSandI = ListLinePlot[dataEAllSandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEAllSandI]}}, PlotStyle -> {Red, Dashed},
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Esol: Corrugated Cylinder (Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM Plots

```

10199: GraphicsGrid[{{EzCorrS, EzCorrSandI}, {ErhoCorrS, ErhoCorrSandI},
{EphiCorrS, EphiCorrSandI}, {EAllCorrS, EAllCorrSandI}},
Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TM Plots

Ez (TM Scattered)

```

10198: EzRegCylTMS = ListLinePlot[dataEzregcylTMS,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEzregcylTMS]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es: Smooth Cylinder (TM Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TM Inc + Scattered)

```

10199: EzRegCylTMSandI = ListLinePlot[dataEzregcylTMSandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEzregcylTMSandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es: Smooth Cylinder (TM Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM Scattered)

```

10198: ErhoRegCylTMS = ListLinePlot[dataErhoRegcylTMS,
PlotRange -> {{0, 2*Pi}, {0, Max[SolErhoRegcylTMS]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TM Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM Inc + Scattered)

```

10199: ErhoRegCylTMSandI = ListLinePlot[dataErhoRegcylTMSandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolErhoRegcylTMSandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TM Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM Scattered)

```

10198: EphiRegCylTMS = ListLinePlot[dataEphiRegcylTMS,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEphiRegcylTMS]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ: Smooth Cylinder (TM Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM Inc + Scattered)

```

10199: EphiRegCylTMSandI = ListLinePlot[dataEphiRegcylTMSandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEphiRegcylTMSandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ: Smooth Cylinder (TM Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TE Scattered)

```

10198: EAllRegCylTMS =
ListLinePlot[dataEAllTMS, PlotRange -> {{0, 2*Pi}, {0, Max[SolEAllTMS]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Esol: Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM Inc + Scattered)

```

10199: EAllRegCylTMSandI = ListLinePlot[dataEAllTMSandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEAllTMSandI]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Esol: Smooth Cylinder (TM Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM Plots

```

GraphicsGrid[{{EzRegCylTMS, EzRegCylTMSandI}, {ErhoRegCylTMS, ErhoRegCylTMSandI},
{EphiRegCylTMS, EphiRegCylTMSandI}, {EAllRegCylTMS, EAllRegCylTMSandI}},
Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TE Plots

Ez (TE Scattered)

```

10198: EzRegCylTES = ListLinePlot[dataEzregcylTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEzregcylTES]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es: Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TE Inc + Scattered)

```

10199: EzRegCylTESandI = ListLinePlot[dataEzregcylTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEzregcylTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Es: Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TE Scattered)

```

10198: ErhoRegCylTES = ListLinePlot[dataErhoRegcylTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SolErhoRegcylTES]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TE Inc + Scattered)

```

10199: ErhoRegCylTESandI = ListLinePlot[dataErhoRegcylTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SolErhoRegcylTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Er: Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TE Scattered)

```

10198: EphiRegCylTES = ListLinePlot[dataEphiRegcylTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SolEphiRegcylTES]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Eφ: Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TE Inc + Scattered)

```

%%1000 ErRegCylTESandI = ListLinePlot[dataErRegCylTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErRegCylTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TE Scattered)

```

%%1001 EAllRegCylTES =
ListLinePlot[dataEAllTES, PlotRange -> {{0, 2*Pi}, {0, Max[SoLEAllTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez,all Smooth Cylinder (TE Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TE Inc + Scattered)

```

%%1002 EAllRegCylTESandI = ListLinePlot[dataEAllTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLEAllTESandI]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez,all Smooth Cylinder (TE Incident + Scattered Field)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TE Plots

```

%%1003 GraphicsGrid[{{ErRegCylTES, ErRegCylTESandI},
{ErhoRegCylTES, ErhoRegCylTESandI}}, {EphiRegCylTES, EphiRegCylTESandI},
{EAllRegCylTES, EAllRegCylTESandI}], Spacings -> {Scaled[0], Scaled[0]}];
    
```

Smooth Cylinder Plots - TM + TE Plots

Ez (TM+TE Scattered)

```

%%1004 ErRegCylTMplusTES = ListLinePlot[dataErRegCylTMplusTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ez (TM+TE Inc + Scattered)

```

%%1005 ErRegCylTMplusTESandI = ListLinePlot[dataErRegCylTMplusTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM+TE Scattered)

```

%%1006 ErhoRegCylTMplusTES = ListLinePlot[dataErhoRegCylTMplusTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErhoRegCylTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Erho (TM+TE Inc + Scattered)

```

%%1007 ErhoRegCylTMplusTESandI = ListLinePlot[dataErhoRegCylTMplusTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErhoRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM+TE Scattered)

```

%%1008 EphiRegCylTMplusTES = ListLinePlot[dataEphiRegCylTMplusTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLEphiRegCylTMplusTES]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Ephi (TM+TE Inc + Scattered)

```

%%1009 EphiRegCylTMplusTESandI = ListLinePlot[dataEphiRegCylTMplusTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLEphiRegCylTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM+TE Scattered)

```

%%1010 EAllRegCylTMplusTES = ListLinePlot[dataEAllTMplusTES,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLEAllTMplusTES]}}, PlotStyle -> Blue,
BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez,all Smooth Cylinder (TM + TE Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

EAll (TM+TE Inc + Scattered)

```

%%1011 EAllRegCylTMplusTESandI = ListLinePlot[dataEAllTMplusTESandI,
PlotRange -> {{0, 2*Pi}, {0, Max[SoLEAllTMplusTESandI]}},
PlotStyle -> Blue, BaseStyle -> AbsoluteThickness[2], PlotMarkers -> None,
PlotLabel -> "Ez,all Smooth Cylinder (TM + TE Inc and Scattered)",
Frame -> True, FrameLabel -> {"φ", "V/m"},
GridLines -> {{Pi}, {Thick, Gray, Dashed}}, Automatic, Background -> White,
ImageSize -> 700, BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}];
    
```

Summary TM+TE Plots

```

GraphicsGrid[{{ErRegCylTMplusTES, ErRegCylTMplusTESandI},
{ErhoRegCylTMplusTES, ErhoRegCylTMplusTESandI},
{EphiRegCylTMplusTES, EphiRegCylTMplusTESandI},
{EAllRegCylTMplusTES, EAllRegCylTMplusTESandI}], Spacings -> {Scaled[0], Scaled[0]}];
    
```

Compare (Smooth vs Corrugated) Plots

TM Compare

```

%%1012 GraphicsGrid[{{Show[ErRegCylTMS, ErCorrS],
PlotRange -> {{0, 2*Pi}, {0, Max[SoLErRegCylTMS, SoLErCorrS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"φ/A", "V/m"}, PlotLabel ->
"Ez TM Scattered Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)"},
Show[ErRegCylTMSandI, ErCorrSandI, PlotRange ->
{{0, 2*Pi}, {0, Max[SoLErRegCylTMSandI, SoLErCorrS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"φ/A", "V/m"},
PlotLabel -> "Ez TM Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"},
>Show[ErhoRegCylTMS, ErhoCorrS, PlotRange -> {{0, 2*Pi},
{0, Max[SoLErhoRegCylTMS, SoLErhoS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, Frame -> True,
FrameLabel -> {"φ/A", "W/m"}, PlotLabel ->
"Ez TM Scattered Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)"},
>Show[ErhoRegCylTMSandI, ErhoCorrSandI, PlotRange ->
{{0, 2*Pi}, {0, Max[SoLErhoRegCylTMSandI, SoLErhoS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"},
Frame -> True, FrameLabel -> {"φ/A", "W/m"},
PlotLabel -> "Ez TM Inc + Scattered Smooth Cylinder
(Blue) vs Corrugated Cylinder (Red, --)"},
>Show[EphiRegCylTMS, EphiCorrS, PlotRange -> {{0, 2*Pi},
{0, Max[SoLEphiRegCylTMS, SoLEphiS]}},
BaseStyle -> {FontSize -> 14, FontWeight -> "Bold"}, Frame -> True,
FrameLabel -> {"φ/A", "V/m"}, PlotLabel ->
"Ez TM Scattered Smooth Cylinder (Blue) vs Corrugated Cylinder (Red, --)"},
>Show[EphiRegCylTMSandI, EphiCorrSandI, PlotRange ->
{{0, 2*Pi}, {0, Max[SoLEphiRegCylTMSandI, SoLEphiS]}},
    
```


APPENDIX B

Derivation for Fundamental Equations of Guided Waves from Maxwell's Equations

Start with Maxwell's equations in differential form, $\nabla \times \vec{E}$ and $\nabla \times \vec{H}$ [12, p. 2], and expand into cylindrical coordinates [12, p. 925]

$$\begin{aligned} \nabla \times \vec{E} &= -j\omega\mu\vec{H} = \hat{\rho} \left(\frac{1}{\rho} \frac{\partial E_z}{\partial \phi} - \frac{\partial E_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial E_\rho}{\partial z} - \frac{\partial E_z}{\partial \rho} \right) + \hat{z} \left(\frac{1}{\rho} \frac{\partial(\rho E_\phi)}{\partial \rho} - \frac{1}{\rho} \frac{\partial E_\rho}{\partial \phi} \right) \\ \nabla \times \vec{H} &= j\omega\varepsilon\vec{E} = \hat{\rho} \left(\frac{1}{\rho} \frac{\partial H_z}{\partial \phi} - \frac{\partial H_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial H_\rho}{\partial z} - \frac{\partial H_z}{\partial \rho} \right) + \hat{z} \left(\frac{1}{\rho} \frac{\partial(\rho H_\phi)}{\partial \rho} - \frac{1}{\rho} \frac{\partial H_\rho}{\partial \phi} \right) \end{aligned}$$

Replace, $\frac{\partial}{\partial z} = -j\beta$ based on the relationship the relationship $\frac{\partial}{\partial z}(e^{-j\beta z}) = -j\beta e^{-j\beta z}$

and separate into cylindrical components

$$-j\omega\mu H_\rho = \frac{1}{\rho} \frac{\partial E_z}{\partial \phi} - \frac{\partial E_\phi}{\partial z} = \frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + j\beta E_\phi$$

$$j\omega\varepsilon E_\rho = \frac{1}{\rho} \frac{\partial H_z}{\partial \phi} - \frac{\partial H_\phi}{\partial z} = \frac{1}{\rho} \frac{\partial H_z}{\partial \phi} + j\beta H_\phi$$

$$-j\omega\mu H_\phi = \frac{\partial E_\rho}{\partial z} - \frac{\partial E_z}{\partial \rho} = -j\beta E_\rho - \frac{\partial E_z}{\partial \rho}$$

$$j\omega\varepsilon E_\phi = \frac{\partial H_\rho}{\partial z} - \frac{\partial H_z}{\partial \rho} = -j\beta H_\rho - \frac{\partial H_z}{\partial \rho}$$

$$-j\omega\mu H_z = \frac{1}{\rho} \frac{\partial(\rho E_\phi)}{\partial \rho} - \frac{1}{\rho} \frac{\partial E_\rho}{\partial \phi}$$

$$j\omega\varepsilon E_z = \frac{1}{\rho} \frac{\partial(\rho H_\phi)}{\partial \rho} - \frac{1}{\rho} \frac{\partial H_\rho}{\partial \phi}$$

Also,

$$k = \frac{2\pi}{\lambda} = \omega\sqrt{\mu\varepsilon}$$

$$k_c^2 = k^2 - \beta^2 = \omega^2\mu\varepsilon - \beta^2$$

Solving for E_ρ

$$E_\rho = \frac{1}{j\omega\varepsilon} \left(\frac{1}{\rho} \frac{\partial H_z}{\partial \phi} + j\beta H_\phi \right)$$

Substitute

$$H_\phi = \frac{1}{j\omega\mu} \left(j\beta E_\rho + \frac{\partial E_z}{\partial \rho} \right)$$

$$E_\rho = \frac{1}{j\omega\varepsilon} \left(\frac{1}{\rho} \frac{\partial H_z}{\partial \phi} + \frac{j\beta}{j\omega\mu} \left(j\beta E_\rho + \frac{\partial E_z}{\partial \rho} \right) \right) = \frac{1}{j\omega\varepsilon} \left(\frac{1}{\rho} \frac{\partial H_z}{\partial \phi} - \frac{\beta^2 E_\rho}{j\omega\mu} + \frac{j\beta}{j\omega\mu} \frac{\partial E_z}{\partial \rho} \right)$$

$$E_\rho = \frac{1}{j\omega\varepsilon\rho} \frac{\partial H_z}{\partial \phi} + \frac{\beta^2 E_\rho}{\omega^2 \mu \varepsilon} - \frac{j\beta}{\omega^2 \mu \varepsilon} \frac{\partial E_z}{\partial \rho}$$

$$E_\rho - \frac{\beta^2 E_\rho}{\omega^2 \mu \varepsilon} = \frac{1}{j\omega\varepsilon\rho} \frac{\partial H_z}{\partial \phi} - \frac{j\beta}{\omega^2 \mu \varepsilon} \frac{\partial E_z}{\partial \rho}$$

$$E_\rho \left(1 - \frac{\beta^2}{\omega^2 \mu \varepsilon} \right) = \frac{1}{j\omega\varepsilon\rho} \frac{\partial H_z}{\partial \phi} - \frac{j\beta}{\omega^2 \mu \varepsilon} \frac{\partial E_z}{\partial \rho}$$

Multiply both sides by $\omega^2 \mu \varepsilon$

$$E_\rho (\omega^2 \mu \varepsilon - \beta^2) = \frac{\omega\mu}{j\rho} \frac{\partial H_z}{\partial \phi} - j\beta \frac{\partial E_z}{\partial \rho}$$

Replace $k_c^2 = \omega^2 \mu \varepsilon - \beta^2$ and solve for E_ρ

$$E_\rho = \frac{-j}{k_c^2} \left(\frac{\omega\mu}{\rho} \frac{\partial H_z}{\partial \phi} + \beta \frac{\partial E_z}{\partial \rho} \right)$$

Solving for H_ϕ

$$H_\phi = \frac{1}{j\omega\mu} \left(j\beta E_\rho + \frac{\partial E_z}{\partial \rho} \right) = \frac{1}{j\omega\mu} \left(j\beta \left(\frac{1}{j\omega\varepsilon} \left(\frac{1}{\rho} \frac{\partial H_z}{\partial \phi} + j\beta H_\phi \right) \right) + \frac{\partial E_z}{\partial \rho} \right)$$

$$H_\phi = \frac{1}{j\omega\mu} \left(\frac{j\beta}{j\omega\varepsilon\rho} \frac{\partial H_z}{\partial \phi} - \frac{\beta^2}{j\omega\varepsilon} H_\phi + \frac{\partial E_z}{\partial \rho} \right) = -\frac{j\beta}{\omega^2 \mu \varepsilon \rho} \frac{\partial H_z}{\partial \phi} + \frac{\beta^2}{\omega^2 \mu \varepsilon} H_\phi + \frac{1}{j\omega\mu} \frac{\partial E_z}{\partial \rho}$$

$$H_\phi \left(1 - \frac{\beta^2}{\omega^2 \mu \varepsilon} \right) = -\frac{j\beta}{\omega^2 \mu \varepsilon \rho} \frac{\partial H_z}{\partial \phi} + \frac{1}{j\omega\mu} \frac{\partial E_z}{\partial \rho}$$

Multiply both sides by $\omega^2 \mu \varepsilon$

$$H_\phi (\omega^2 \mu \varepsilon - \beta^2) = -\frac{j\beta}{\rho} \frac{\partial H_z}{\partial \phi} + \frac{\omega\varepsilon}{j} \frac{\partial E_z}{\partial \rho} = -j \left(\frac{\beta}{\rho} \frac{\partial H_z}{\partial \phi} + \omega\varepsilon \frac{\partial E_z}{\partial \rho} \right)$$

$$H_\phi = \frac{-j}{k_c^2} \left(\frac{\beta}{\rho} \frac{\partial H_z}{\partial \phi} + \omega \varepsilon \frac{\partial E_z}{\partial \rho} \right)$$

Solving for E_ϕ

$$E_\phi = \frac{1}{j\omega\varepsilon} \left(-j\beta H_\rho - \frac{\partial H_z}{\partial \rho} \right)$$

Substitute,

$$H_\rho = -\frac{1}{j\omega\mu} \left(\frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + j\beta E_\phi \right)$$

$$E_\phi = \frac{1}{j\omega\varepsilon} \left(\frac{j\beta}{j\omega\mu\rho} \frac{\partial E_z}{\partial \phi} - \frac{\beta^2}{j\omega\mu} E_\phi - \frac{\partial H_z}{\partial \rho} \right) = \frac{-j\beta}{\omega^2\mu\varepsilon\rho} \frac{\partial E_z}{\partial \phi} + \frac{\beta^2}{\omega^2\mu\varepsilon} E_\phi - \frac{1}{j\omega\varepsilon} \frac{\partial H_z}{\partial \rho}$$

$$E_\phi \left(1 - \frac{\beta^2}{\omega^2\mu\varepsilon} \right) = \frac{-j\beta}{\omega^2\mu\varepsilon\rho} \frac{\partial E_z}{\partial \phi} - \frac{1}{j\omega\varepsilon} \frac{\partial H_z}{\partial \rho}$$

Multiply both sides by $\omega^2\mu\varepsilon$

$$E_\phi(\omega^2\mu\varepsilon - \beta^2) = \frac{-j\beta}{\rho} \frac{\partial E_z}{\partial \phi} - \frac{\omega\mu}{j} \frac{\partial H_z}{\partial \rho} = -j \left(\frac{\beta}{\rho} \frac{\partial E_z}{\partial \phi} - \omega\mu \frac{\partial H_z}{\partial \rho} \right)$$

$$E_\phi = \frac{-j}{k_c^2} \left(\frac{\beta}{\rho} \frac{\partial E_z}{\partial \phi} - \omega\mu \frac{\partial H_z}{\partial \rho} \right)$$

Solving for H_ρ

$$H_\rho = \frac{-1}{j\omega\mu} \left(\frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + j\beta E_\phi \right)$$

Substitute,

$$E_\phi = \frac{1}{j\omega\varepsilon} \left(j\beta H_\rho - \frac{\partial H_z}{\partial \rho} \right)$$

$$H_\rho = \frac{-1}{j\omega\mu} \left(\frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + j\beta \left(\frac{1}{j\omega\varepsilon} \left(j\beta H_\rho - \frac{\partial H_z}{\partial \rho} \right) \right) \right) = \frac{-1}{j\omega\mu} \left(\frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + \frac{\beta^2}{j\omega\varepsilon} H_\rho - \frac{j\beta}{j\omega\varepsilon} \frac{\partial H_z}{\partial \rho} \right)$$

$$H_\rho = \frac{-1}{j\omega\mu\rho} \frac{\partial E_z}{\partial \phi} + \frac{\beta^2}{\omega^2\mu\varepsilon} H_\rho - \frac{j\beta}{\omega^2\mu\varepsilon} \frac{\partial H_z}{\partial \rho}$$

$$H_\rho \left(1 - \frac{\beta^2}{\omega^2\mu\varepsilon} \right) = \frac{-1}{j\omega\mu\rho} \frac{\partial E_z}{\partial \phi} - \frac{j\beta}{\omega^2\mu\varepsilon} \frac{\partial H_z}{\partial \rho}$$

Multiply both sides by $\omega^2\mu\varepsilon$

$$H_\rho(\omega^2 \mu \varepsilon - \beta^2) = \frac{-\omega \varepsilon}{j\rho} \frac{\partial E_z}{\partial \phi} - j\beta \frac{\partial H_z}{\partial \rho} = -j \left(\frac{-\omega \varepsilon}{\rho} \frac{\partial E_z}{\partial \phi} + \beta \frac{\partial H_z}{\partial \rho} \right)$$

$$H_\rho = \frac{-j}{\kappa_c^2} \left(\frac{-\omega \varepsilon}{\rho} \frac{\partial E_z}{\partial \phi} + \beta \frac{\partial H_z}{\partial \rho} \right)$$

Note that in paper k_c is substituted with k_ρ and β is substituted with k_z .

REFERENCES

- [1] G. Manara, G. Pelosi, A. Monorchio and R. Coccioli, "Plane-wave scattering from cylinders with transverse corrugations," *Electronics Letters*, vol. 316, pp. 437-438, 16 March 1995.
- [2] G. Manara, A. Monorchio, G. Pelosi and R. Coccioli, "Electromagnetic Scattering From Corrugated Cylinders," in *Antennas and Propagation Society International Symposium*, 1995.
- [3] A. A. Kishk and P.-S. Kildal, "An asymptotic boundary condition for corrugated surfaces and its application to calculate scattering from circular cylinders with dielectric filled corrugations," in *Antennas and Propagation Society International Symposium*, 1996.
- [4] A. A. Kishk, K. S. P., A. Monorchio and G. Manara, "Asymptotic boundary condition for corrugated surfaces, and its application to scattering from circular cylinders with dielectric filled corrugations," *IEE Proceedings - Microwaves, Antennas and Propagation*, vol. 145, no. 1, pp. 116-122, 1998.
- [5] A. Freni, "Plane wave scattering from a cylinder loaded periodically with groups of metallic rings," *Electronics Letters*, vol. 32, no. 10, pp. 874-875, 9 May 1996.

- [6] T. C. Rao, "Plane Wave Scattering by a Corrugated Conducting Cylinder at Oblique Incidence," *IEEE Transactions on Antennas and Propagation*, vol. 36, no. 8, pp. 1184-1188, 1988.
- [7] P. Hillion, "Scattering of T_e and T_m ," *Journal of Electromagnetic Waves and Applications*, vol. 14, no. 5, pp. 655-662, 2000.
- [8] R. E. Collins, *Field Theory of Guided Waves*, Second ed., New York: John Wiley & Sons, Inc., 1991.
- [9] A. F. Peterson, S. L. Ray and R. Mittra, *Computational Methods for Electromagnetics*, New York: IEEE Press, 1998.
- [10] J. F. G. Farrell and D. H. Kuhn, "Mutual coupling in infinite planar arrays of rectangular waveguide horns," *IEEE Transactions on Antennas and Propagation*, Vols. AP-16, pp. 405-414, 1968.
- [11] T. Bohning, *Electromagnetic scattering from a periodic array of open-ended*, PhD Dissertation, Florida Atlantic University, 1992.
- [12] C. A. Balanis, *Advanced Engineering Electromagnetics*, Hoboken: John Wiley & Sons, 1989.
- [13] D. M. Pozar, *Microwave Engineering*, 3rd ed., Hoboken, NJ: John Wiley & Sons, 2005.
- [14] R. F. Harrington, *Time-Harmonic Electromagnetic Fields*, New York: IEEE Press, 2001.
- [15] Wikipedia, "Bloch wave," Wikipedia, 23 September 2016. [Online]. Available: https://en.wikipedia.org/wiki/Bloch_wave. [Accessed 5 November 2016].

- [16] F. T. Ulaby, *Fundamentals of Applied Electromagnetics*, 5th ed., Upper Saddle River: Pearson Prentice Hall, 2007.
- [17] Wolfram Research, Inc., *Mathematica*, Version 10.3 ed., Champaign, Illinois: Wolfram Research, Inc., 2016.
- [18] J. W. Helton and R. L. Miller, "NCAIgebra," February 2016. [Online]. Available: <http://math.ucsd.edu/~ncalg/>.
- [19] M. T. Heath, "The Numerical Solution of Ill-Conditioned Systems of Linear Equations," National Technical Information Service U.S. Department of Commerce, Springfield, 1974.
- [20] E. W. Weisstein, "Moore-Penrose Matrix Inverse," From MathWorld--A Wolfram Web Resource, [Online]. Available: <http://mathworld.wolfram.com/Moore-PenroseMatrixInverse.html>. [Accessed 4 November 2016].
- [21] Wolfram Research, "LeastSquares," Wolfram Research, 2007. [Online]. Available: <https://reference.wolfram.com/language/ref/LeastSquares.html>. [Accessed 4 November 2016].
- [22] C. Wolff, "Radar Basics," Christian Wolff, [Online]. Available: <http://www.radartutorial.eu/01.basics/Rayleigh-%20versus%20Mie-Scattering.en.html>. [Accessed 4 November 2016].
- [23] A. E. Fuhs, "Radar Cross Section Lectures," Naval Postgraduate School, Monterey, 1982.
- [24] Catslash, "File:Radar cross section of metal sphere from Mie theory.svg," Wikipedia, 27 June 2009. [Online]. Available:

https://commons.wikimedia.org/wiki/File:Radar_cross_section_of_metal_sphere_from_Mie_theory.svg. [Accessed 4 November 2016].

- [25] A. A. Kishk, P. -S. Kildal, A. Monorchio, G. Manara and Z. Sipus, "Validation of the Asymptotic Cormgation Boundary Condition for Circular Cylinders with Dielectric Filled Corrugations," *IEEE Conference Publications*, vol. 3, pp. 2080-2083, 1997.
- [26] K. A. Ahmed and P.-S. Kildal, "Asymptotic Boundary Conditions for Strip-Loaded Scatterers Applied to Circular Dielectric Cylinders Under Oblique Incidence," *IEEE Transactions on Antennas and Propagation*, vol. 45, no. 1, pp. 51-55, 1997.
- [27] A. Freni, C. Mias and F. L. Ronald, "Hybrid Finite-Element Analysis of Electromagnetic Plane Wave Scattering from Axially Periodic Cylindrical Structures," *IEEE Transactions on Antennas and Propagation*, vol. 46, no. 12, pp. 1859 - 1866, 1998.
- [28] A. Freni, "Scattering from a dielectric cylinder axially loaded with periodic metallic rings," *IEE Proc.-Microw. Antennas Propug.*, vol. 143, no. 3, pp. 233-237, 1996.
- [29] C. A. Balanis, *Antenna Theory: Analysis and Design*, 3rd ed., Hoboken: John Wiley & Sons, 2005.
- [30] A. Rohatgi, "<http://arohatgi.info/WebPlotDigitizer/>," May 2016. [Online]. Available: <http://arohatgi.info/WebPlotDigitizer>. [Accessed 12 November 2016].
- [31] S. Garcia, J. Bagby and I. Morazzani, "Plane-Wave Scattering of a Periodic Corrugated Cylinder," in *Proc. of the International Microwave Symposium (IMS)*, Honolulu, 2017.

- [32] M. T. Włodarczyk and S. R. Seshadri, "Excitation and scattering of guided modes on a dielectric cylinder with a periodically varying radius," *Journal of Applied Physics*, vol. 57, no. 3, pp. 943-955, 1984.
- [33] G. Zheng, X. Yin, J. Wang, M. Guo and X. Wang, "Complex permittivity and microwave absorbing property," *J. Mater. Sci. Technol.*, vol. 28(8), p. 745–50, 2012.
- [34] J. Bagby and S. Garcia, "Electromagnetic Scattering from a Loaded Corrugated Cylinder," in *Proc. of the Progress In Electromagnetics Research Symposium (PIERS)*, St Petersburg, 2017.
- [35] B. A. Munk, *Frequency Selective Surfaces: Theory and Design*, New York: John Wiley & Sons, 2000.